

AD-A100 730

GRUMMAN AEROSPACE CORP BETHPAGE NY
HYDRAULIC DIAGNOSTIC MONITORING SYSTEM.(U)
MAR 81 J J DUZICH

F/G 14/2

N62269-78-C-0041

UNCLASSIFIED

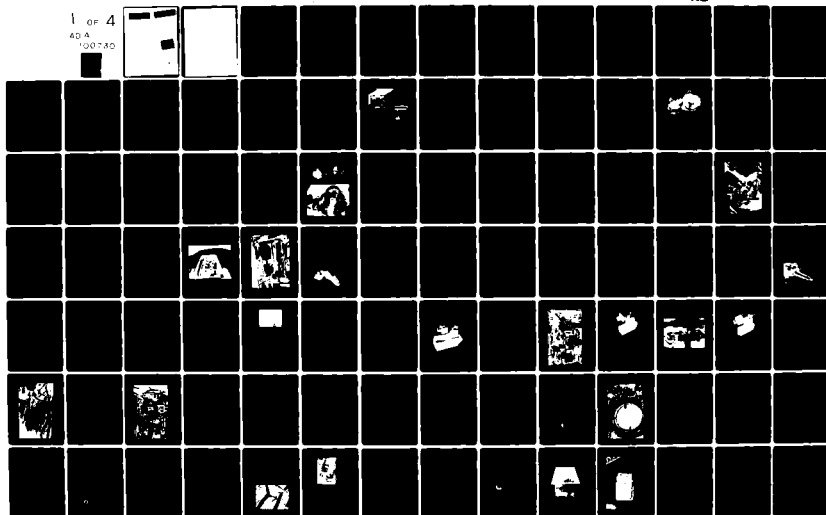
NADC-TR-81073-60

NL

1 OF 4

AD A

100730



AD 1000 30

III

(12)



UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

11/77R 81073-60

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM																									
1. REPORT NUMBER (18) NADC 81073-60	2. GOVT ACCESSION NO. AD-A100730	3. RECIPIENT'S CATALOG NUMBER																									
4. TITLE (and Subtitle) (6) Hydraulic Diagnostic Monitoring System • FINAL REPORT		5. TYPE OF REPORT & PERIOD COVERED (9) Final Rpt. Jan 79-Oct 80																									
7. AUTHOR(s) (11) John J./Duzich		8. CONTRACT OR GRANT NUMBER(s) N62269-78-C-0041																									
9. PERFORMING ORGANIZATION NAME AND ADDRESS Grumman Aerospace Corporation Bethpage N.Y. 11714		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS																									
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Air Systems Command Washington D.C. Code 340		12. REPORT DATE (11) 2 March 1981																									
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Naval Air Development Center Warminster Pennsylvania 18974		13. NUMBER OF PAGES 316																									
16. DISTRIBUTION STATEMENT (of this Report) Approved for Public Release Distribution Unlimited.		15. SECURITY CLASS. (of this report) Unclassified																									
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)																											
18. SUPPLEMENTARY NOTES																											
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) <table border="0"> <tr> <td>Hydraulic</td> <td>Pressure</td> <td>Pumps</td> <td>Display Panel</td> </tr> <tr> <td>Monitoring</td> <td>Temperature</td> <td>Displacement</td> <td>Analog</td> </tr> <tr> <td>Flow</td> <td>Fiber Optics</td> <td>Accumulators</td> <td>Discrete</td> </tr> <tr> <td>Level</td> <td>Reservoir</td> <td>Microprocessor</td> <td></td> </tr> <tr> <td></td> <td>Desiccant</td> <td></td> <td></td> </tr> <tr> <td></td> <td>Filters</td> <td></td> <td></td> </tr> </table>				Hydraulic	Pressure	Pumps	Display Panel	Monitoring	Temperature	Displacement	Analog	Flow	Fiber Optics	Accumulators	Discrete	Level	Reservoir	Microprocessor			Desiccant				Filters		
Hydraulic	Pressure	Pumps	Display Panel																								
Monitoring	Temperature	Displacement	Analog																								
Flow	Fiber Optics	Accumulators	Discrete																								
Level	Reservoir	Microprocessor																									
	Desiccant																										
	Filters																										
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <p>This report presents a second twelve month summary of a two year effort of a HYCOS hydraulic diagnostic monitoring system. The program was broken down into three tasks:</p> <p>(See Over)</p>																											

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 68 IS OBSOLETE
S/N 0102-014-6601

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

388847

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

Task III Integrated the Diagnostic System into A6E B/N 155628
Debugged the system and ran a 12 month flight test schedule.
This report covers Task III.

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524
--

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

SUMMARY

This program was based on the feasibility study of a hydraulic monitoring system described in NADC report number TR75168-30 published in July 1976. The interim report, NADC TR76389-30, was published in May 1979 and covered Tasks I and II.

The purpose of the Hydraulic Diagnostic Monitoring System (HYCOS) is to warn of impending failure of hydraulic system components by onboard sensors continuously monitoring failure-indicating parameters.

The monitoring system consists of three basic types of sensors: analog, discrete, and fiber-optic. These sensors feed information to a self-contained, centrally located display panel through interface circuits that are easily accessible to ground maintenance personnel. The panel has circuit and system test capability which detects malfunctions of electronic equipment, sensor circuits, and display indicators.

The Sensor List includes the following types:

- Displacement: (a) Potentiometer - rotary and linear (analog)
 (b) Photo-optic (reflective)
 (c) Hall Effect (magnetic)
- Temperature: (a) Pressurized gas (discrete)
 (b) Bimetallic (discrete)
 (c) I/C transducer (analog)
- Differential Pressure, Filter: Spring biased piston (discrete)
- Pressure: (a) Gas and spring biased switch (discrete)
 (b) Semiconductor strain gage (analog)
- Liquid Detection: Fiber-optic probe using refractive index coupling (discrete)
- Flow: Orifice with bypass shunt for higher flows (discrete)
- Desiccant Color Detection: Fiber-optic color transmission using reflected light. Optical properties of irregular granules (analog - color spectrum)

Displacement sensors of the variable-resistance type were used to measure reservoir piston, accumulator, rudder, and rudder pedal displacements. Two other concepts evolved in the accumulator application, a reflective photo-optic type and a magnetic Hall Effect type. Since they are experimental in nature and require development, they were not used in the prototype system.

Three types of temperature sensors (one analog and two discrete) were chosen and utilized in the pneumatic, fluid, and surface temperature circuits. Their performance was satisfactory during simulator testing. Filter differential pressure indicators were of the spring biased magnetically latching type. Their performance was satisfactory.

Two types of pressure-sensor devices were utilized. In one pneumatic circuit, a temperature-compensated pressure switch performed as predicted over a broad temperature range. In another pneumatic hydraulic circuit, a semiconductor strain-gage type also performed according to specification.

Liquid detection circuits in high-pressure pneumatic bottles proved to be a challenge in the area of pressure sealing and liquid detection using the optical properties of liquids, solids, and gases. All major problems were overcome after extensive development effort.

The use of shunt orifice flow measuring devices proved satisfactory in three hydraulic subcircuits. In two of the three cases, the indicator was immobilized during normal system operation.

Desiccant color detection utilizing color transmission proved difficult due to the irregular desiccant particles. A high-intensity light source was required to achieve sufficient color transmission. An improved sensor was developed for the A-6E installation.

The diagnostic system monitors the hydraulic system during flight as well as on the ground. Any flight discrete failures are displayed when the aircraft is interrogated on the ground. Discrete sensors are manually resettable.

An onboard preprogrammed microprocessor handles all the analog inputs through A/D converters and determines the condition of components with multiple sensors.

Task I defined and procured hardware sensors for two diagnostic monitoring systems. After individual component acceptance testing, the system was interfaced with a F-14A hydraulic simulator.

Task II consisted of installing the system on the F-14A hydraulic simulator in order to demonstrate system/component reliability under simulated conditions. A baseline was established and various failure modes and diagnostic system reactions determined.

The scope of the Interim Report covered only the development and integration of the F-14 hydraulic monitoring system.

Task III of the hydraulic monitoring system contract consisted of procuring, building, installing, and testing in a bailed A-6E flight test vehicle for a duration of at least 6 months.

To accomplish these objectives:

- Bracketry was designed and fabricated to support the system components. The combined hydraulic fluid distribution system was modified to accept pressure, flow, and temperature sensors
- Electrical and fiber-optic cable runs were designed, fabricated, and installed between the HYCOS display panel and sensors
- The HYCOS system was installed only in the combined hydraulic system and did not affect system operation
- Representative system components and parameters were monitored. These included
 - Hydraulic reservoir
 - Filters
 - Accumulator
 - Pneumatic bottles
 - Hydraulic pump
 - Rudder actuator
 - Relief valve
 - System operational hours
- The microprocessor program was written to apply specifically to the A-6E requirements

- The vehicle received normal ground tests prior to being cleared for its normally scheduled flight program
- During the flight program (installed January 1979, removed November 15, 1980) the system accumulated over 160 flight hours. First flight occurred on October 31, 1979.

A Navy A-6E bailed aircraft was designated as the official test vehicle in January 1979. By May 1979, the modified hydraulic system was initially pressurized to check for system compatibility. During the latter part of the year, the system was modified to improve reliability and maintainability.

Improvements were made to both the display panel and sensors. In the area of light sensing, transmission of colored light proved difficult since, during installation of the fiber-optic cables, excessive bends were made creating unacceptable light losses. However, the concept was verified.

During the test program, the system continuously detected low pneumatic bottle pressures and low reservoir level during calibration and system operation. No other system abnormalities or malfunctions were detected.

The total time for interrogating the system is 1-1/2 minutes. This significantly reduces turnaround time and increases aircraft availability.

PREFACE

This report was prepared by the Grumman Aerospace Corporation under a Naval Air Development Center, Contract Number N62269-78-C-0041, entitled "Hydraulic Diagnostic Monitoring System".

The program was based on a previous feasibility study conducted by Grumman Aerospace Corporation and reported in NADC TR 75168-30.

Task I of this program covered procured hardware, sensors, and microprocessors for two monitoring systems. One system was installed in a F-14 Flight Simulator and the other scheduled for an A-6 aircraft. The work reported in the report covers the November 1977 to December 1978 timeframe.

Task II covered the results of installing the system in an F-14A hydraulic simulator, integrating and debugging the system, and finally simulating various failure modes in order to demonstrate diagnostic system reaction.

Interim Report NADC TR 76389-30 Hydraulic Diagnostic Monitoring System was published 31 May 1979, covered Tasks I and II.

Task III encompassed the basic integration, debugging, and flight test of the A-6 System.

The sponsoring agency is the Naval Air Systems Command, Washington, D.C. Mr. Steve Hurst, AIR 340C, was the Program Manager

The work was administered under the technical direction of:

Mr. Douglas O. Bagwell

Naval Air Development Center, Warminster, PA 18974

Program Manager for this effort was Mr. Edwin A. Anderson

Project Engineer for this contract was Mr. John J. Duzich

The author wishes to acknowledge the significant support and contributions made by the following Grumman disciplines:

- Aircraft Programs
- Aircraft Project Office
- Controls and Mechanisms
- Electronic Design and Development
- Equipment Lines
- Flight Development Group
- Fluid Power
- Mechanical Design
- Mechanical/Fluid Systems Test
- Quality Control
- Structural Design.

Daily HYCOS System recording, performed by Mr. Frank Martella, Plane Captain, was invaluable in assessing this phase of the program.

CONTENTS

<u>Section</u>	<u>Page</u>
1 HYDRAULIC DIAGNOSTIC MONITORING SYSTEM	13
1.1 Vehicle Designation	13
1.2 Vehicle Modification	13
1.3 Vehicle Component Installation	15
1.3.1 Hydraulic Reservoir	16
1.3.2 Pneumatic Bottles	37
1.3.3 Hydraulic Pump/System	55
1.3.4 Hydraulic Accumulators	68
1.3.5 Rudder	81
1.3.6 Display Panel	86
1.3.7 Hydraulic Filters	100
1.3.8 Flight Control Hydraulic Backup Package	103
2 GROUND AND FLIGHT TESTS	107
2.1 System Debugging	107
2.2 Developmental Modifications and Improvements	107
2.2.1 HYCOS Display Panel	107
2.2.2 Panel Support Structure	108
2.2.3 Sensor Light Sources	109
2.2.4 Flow Sensor Indicators	109
2.2.5 Desiccant Color Detector	109
3 PERFORMANCE AND EVALUATION/ASSESSMENT	111
3.1 Procedures and Methods	111
3.1.1 Objective	111
3.1.2 Procedure	111
3.1.3 Log Sheet Description	112
3.1.4 HYCOS Interrogation Procedure	112
3.1.5 HYCOS Display Criteria	113
3.2 Overall Evaluation of HYCOS System	115

CONTENTS (Cont)

<u>Section</u>		<u>Page</u>
4	RESTORATION OF THE AIRCRAFT	117
5	CONCLUSIONS	119
6	RECOMMENDATIONS	121
7	REFERENCES	122

Appendices

A	HYCOS Log Sheet Format and Typical Flight Log Sheet	A-1
B	Flight-Hour Accumulated Log	B-1
C	Abbreviated Chronological Log	C-1
D	HYCOS Wiring Diagram	D-1
E	Participating Firms	E-1
F	Estimated Weight of Prototype Full-Blown System	F-1
G	Drawing Index and Installation Engineering Orders	G-1
H	HYCOS Program Flow Diagram	H-1
I	HYCOS Battery Analysis and Charger Wiring Diagram	I-1
J	System Installation and Vehicle Photos	J-1
K	Microprocessor Program	K-1

ILLUSTRATIONS

<u>Fig. No.</u>		<u>Page</u>
1	A-6E HYCOS block diagram	14
2	Access panel before modification	15
3	A-6 reservoir typical construction (before modification)	16
4	A-6E reservoir sensing logic	18
5	Modified reservoir (level sensing)	19
6	Modified reservoir subassembly and details	20
7	Hydraulic reservoir (laboratory calibration curve)	21
8	Reservoir calibration curve considering fluid temperature variation	22
9	Calibration curve considering entrained air and temperature variation	23
10	Combined reservoir depletion rate vs time	25
11	Flight reservoir depletion rate vs time	26
12	Voltage-current plot for an IC transducer	27
13	Calibration curve for an IC transducer	27
14	Temperature transducer assembly	28
15	Reservoir temperature sensor installation	28
16	Optical desiccant sensor (early approach)	29
17	Sensor assembly	30
18	Grain-of-wheat bulb characteristic	32
19	Halogen bulb characteristic	33
20	Grain-of-wheat bulb/halogen bulb comparison	34
21	Interim desiccant sensor installation	35
22	Plano-convex lens	36
23	Moisture detector fiber-optic circuit	37
24	No. 1491901-304-21 optical desiccant fitting	38
25	Typical service card	39
26	Emergency canopy dump bottle installation	40
27	Landing gear door dump bottle installation	41

ILLUSTRATIONS (Cont)

<u>Fig. No.</u>		<u>Page</u>
28	Temperature-compensated pressure switch	42
29	Plot of pressure vs temperature for nitrogen	43
30	Temperature-compensated pressure switch: diagrammatic circuit	43
31	Switch actuation points vs temperature (Specification 204-1)	44
32	Switch actuation points vs temperature (Specification 204-2)	46
33	Liquid sensor assembly (early version)	49
34	Liquid sensor assembly (improved version)	50
35	Crofon light guide properties	53
36	Transmissivity of Crofon light guides	53
37	Effect of bend radius on light transmissivity	54
38	Assembled fiber-optic connector	55
39	Display panel fiber-optic terminal	56
40	Pressure seal	57
41	Quiescent flow sensor	58
42	Calibration: flow sensor, bypass type, quiescent flow	59
43	System quiescent flow sensor installation	60
44	Pump case drain flow sensor	61
45	Calibration: pump case drain flow sensor, bypass type	61
46	Pump case drain flow sensor installation	62
47	Rudder actuator flow sensor	63
48	Calibration: rudder actuator quiescent flow sensor, bypass type	64
49	Rudder actuator quiescent flow sensor installation	65
50	System pressure switch	66
51	Relief valve temperature and system pressure switch installation	67
52	Pressure versus temperature of n-propyl alcohol at constant volume	69
53	Manual reset temperature switch	70
54	Accumulator piston displacement versus precharge and system pressures at constant (70°F) temperature	72

ILLUSTRATIONS (Cont)

<u>Fig. No.</u>		<u>Page</u>
55	Accumulator piston displacement versus precharge pressure versus temperature at constant (3000 psi) system pressure	73
56	Precharge pressure nomograph	74
57	Ram air turbine accumulator installation	75
58	Photo-optic accumulator piston displacement sensor	77
59	Photo-optic accumulator piston sensor test results	77
60	Photo-optic displacement sensor wiring diagram	78
61	Entran transducer: output voltage versus pressure	79
62	ESP-1032 pressure transducer wiring diagram	79
63	Pressure transducer envelope	80
64	Potentiometer transducers	82
65	Turtle-deck bell crank potentiometer installation	83
66	Rudder position potentiometer installation	84
67	Rudder differential displacement potentiometer calibration	84
68	DC-DC displacement transducer	85
69	HYCOS panel location on typical aircraft	87
70	HYCOS panel showing bottom connectors	88
71	HYCOS installation in flight test vehicle	89
72	Types of display indicators	92
73	Spectral output of various displays compared to response of human eye	93
74	Intel 8748 block diagram	94
75	Intel 8748 pin configuration	95
76	Nickel-cadmium battery charge characteristics	96
77	Removable display cards	98
78	HYCOS panel with cover removed	99
79	Filter differential pressure indicator	101
80	Filter differential pressure indicator with sampling valve	101
81	Multicator indicator installation in pump case drain filter	102
82	Linear output Hall Effect differential pressure indicator	103
83	Resettable temperature switch characteristics	104
84	Flight control backup module installation	105

TABLES

<u>No.</u>		<u>Page</u>
1	IC Temperature Transducer Data	24
2	Desiccant Components	36
3	Temperature - Compensated Pressure Switches (Specification 204-2)	45
4	Refractive Indices of Various Elements	47
5	Properties of Crofon Fibers with Polyethylene Jackets	52
6	Entran ESP-1032 Transducer Data	80
7	A-6E Rudder Potentiometer Transducers	83
8	HYCOS Display Indicator Considerations	91

Section 1

HYDRAULIC DIAGNOSTIC MONITORING SYSTEM

1.1 VEHICLE DESIGNATION

On 31 January 1979, Naval Air Systems Command Selected A-6 Bureau Number 155628 as the vehicle to be used as a flight test bed for the hydraulic monitoring system. The vehicle, which was being modified/updated, arrived at the Grumman facility during the preceding year and started through the modification line in February as MOD 229.

1.2 VEHICLE MODIFICATION

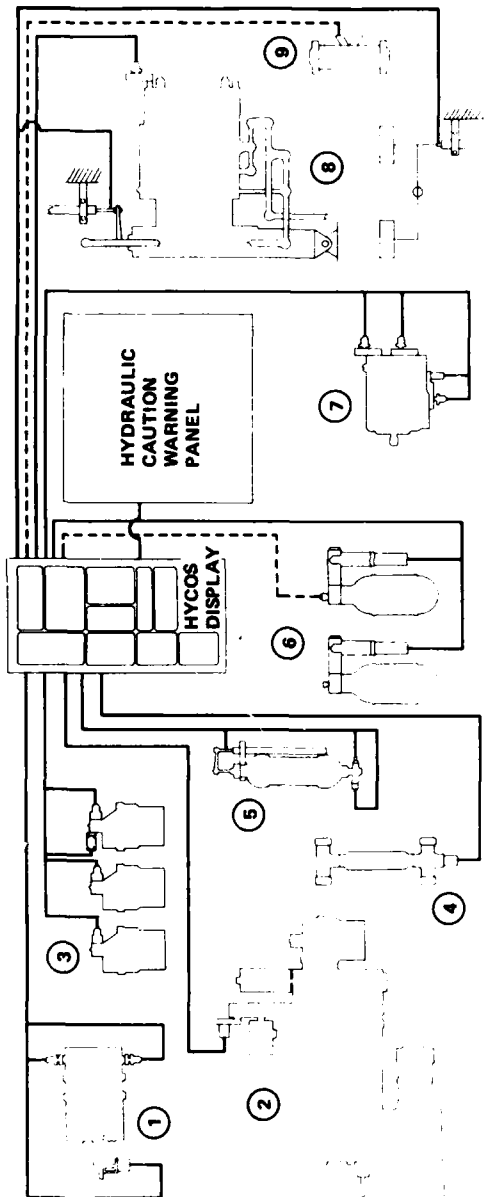
During the time the vehicle was being upgraded to an A-6E configuration, the HYCOS system was installed since all necessary areas were accessible. The HYCOS A-6E block diagram is shown in Figure 1.

Installation was accomplished through the issuance of both Record and Flight Test Engineering Orders (EO) to minimize the impact of the normal buildup. This approach led to an efficient and expeditious system installation. All EOs are listed in Appendix G.

Vehicle modifications included provisions for mounting the HYCOS panel in a ground-accessible area on the port side of the engine duct. Mounting brackets and an access panel door were fabricated and installed. Since the selected surface area is a load-bearing member, Calfax fasteners were used for easy access.

Both wire and fiberoptic line runs were installed in the vehicle at this time in conjunction with the other wiring circuits. New lines were fabricated as required for sensors installed in the pressure system.

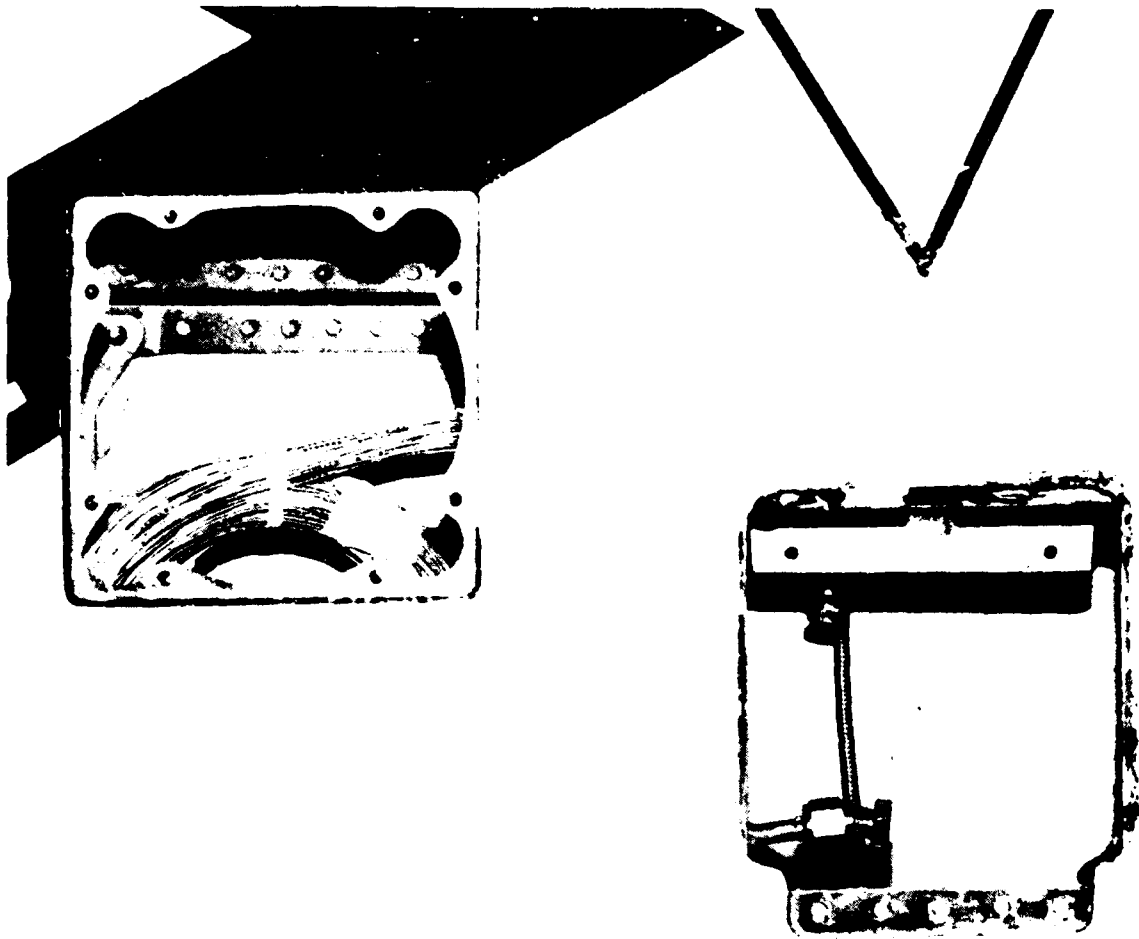
All HYCOS sensor line runs terminated at the test panel through the use of three electrical connectors and two fiberoptic connectors. Figure 2 shows the access area with the wire bundles before modification.



ITEM	DESCRIPTION	SENSOR	TYPE	ITEM	DESCRIPTION	SENSOR	TYPE
1.	RESERVOIR	LEVEL TEMP. PRESS. TEMP.	POTENTIOMETER IC	6.	PNEUMATIC BOTTLE	PRESS. LIQUID	SWITCH OPTICAL PROBE
2.	BACK UP PACKAGE			7.	PUMP	PRESS. FLOW TEMP QUIESCENT	SWITCH SWITCH SWITCH SWITCH
3.	FILTERS			8.	OUTLET CASE FLOW		
4.	RELIEF VALVE	DELTA P DELTA P DELTA P (SAMPLING VALVE)	SWITCH SWITCH SWITCH SWITCH		RUDDER ACTUATOR FLOW PEDALS DESICCANT CONDITION	DIFF DISPL QUIESCENT DIFF DISPL COLOR	POTENTIOMETER SWITCH POTENTIOMETER OPTICAL
5.	ACCUMULATOR	TEMP PRESS TEMP DISPL	SWITCH TRANSDUCER TRANSDUCER TRANSDUCER	9.			

R80-2038-001(T)

Figure 1. A-6E HYCOS block diagram.



R80-2038-002(T)

Figure 2. Access panel before modification.

1.3 VEHICLE COMPONENT INSTALLATION

As specified in the statement of work, various components were modified to sense variables as determined during the previous program. The parameters included:

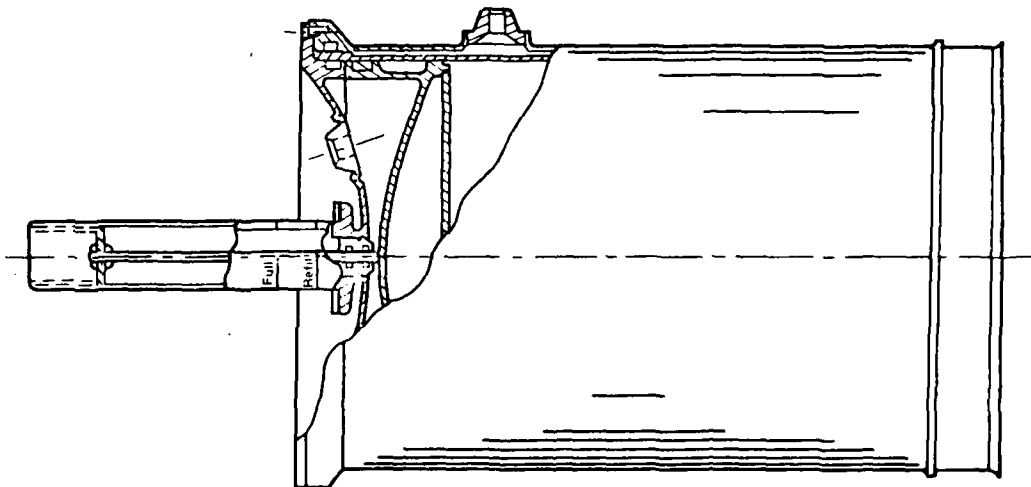
- Level
- Temperature
- Air Content

- Differential Pressure
- Liquid Detection
- Flow
- Desiccant Saturation
- Total System Operating Hours

1.3.1 Hydraulic Reservoir

1.3.1.1 Description

The combined system reservoir was designed to meet the requirements of Specification MIL-R-5520A-1 for a "Class II" separated air and oil reservoir. A "Type B" reservoir pressurized with air to a nominal operating value of 40 psi was used. The detail design configuration is that of a welded and machined outer casing with concave hemispherical ends enclosing a cantilevered, pressure-balanced sleeve. This configuration is not subjected to distortions produced by pressure surges and structural deflection. A free-floating piston separates system oil from pressurizing air. Both return and suction ports are located in the side of the outer shell. Returning oil impinging on the outer surface of the piston sleeve provides natural air separation characteristics. The concave ends minimize weight by reducing the volume of non-usable oil. Figure 3 shows the typical construction.



R80-2038-003(T)

Figure 3. A-6 reservoir typical construction (before modification).

1.3.1.2 Reservoir Sensing Logic

The purpose of the reservoir sensing logic is to:

- Detect the presence of entrained air
- Detect low oil level
- Detect extensive leakage during the previous flight.

Figure 4 shows the A-6E hydraulic reservoir sensing logic. The logic employs variables of fluid temperature and piston displacement. Piston placement during the nonpressurized to pressurized condition gives an indication of entrained air. Fluid thermal expansion is automatically taken into account during microprocessor programming.

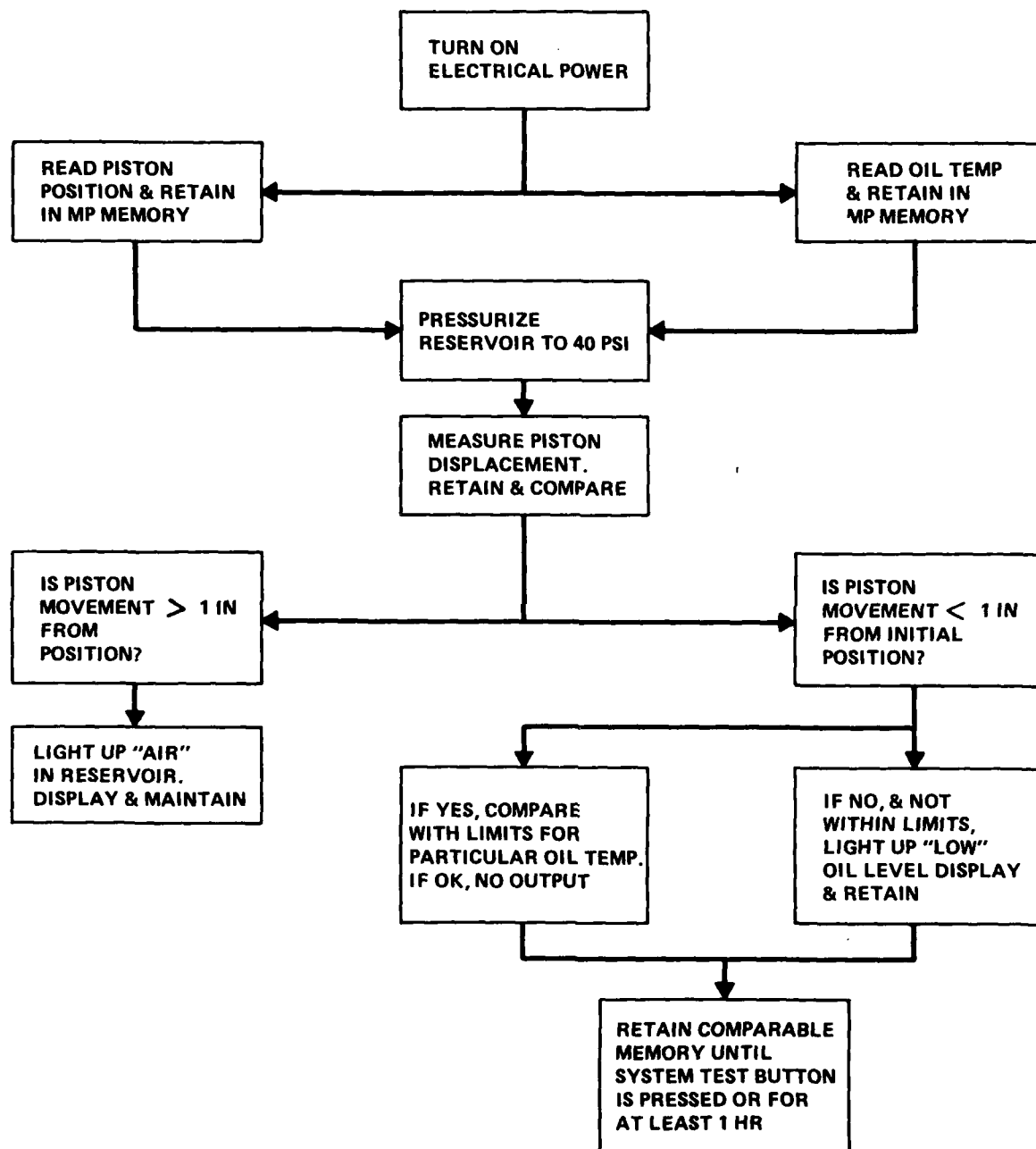
1.3.1.3 Displacement Sensor

An external 10-turn potentiometer was driven via a cable attached to the modified piston. Tensioning of the cable was accomplished by a negator spring motor contained in a pressure housing. One pulley on the motor drove an externally mounted potentiometer through a lip type seal. Reservoir pressurization was accomplished through the normal pressure housing port.

This configuration minimized the rework modification required for providing remote reservoir level sensing capability. Figure 5 shows a cross-section of the modification and the adapter ring added to the reservoir piston. Figure 6 shows details and subassembly of the modified reservoir.

The negator motor model number ML-2918, manufactured by the Hunter Spring Division of Ametek, was selected because of its constant-torque characteristics. Pertinent motor assembly details are listed below:

- Physical Dimensions 2-1/2 x 3-3/4 x 1-3/16 in.
- Materials:
 - Base Zinc-plated steel
 - Drums Delrin or nylon
 - Spring 301 stainless steel
 - Cable 0.024 in. dia stainless steel



R80-2038-004(T)

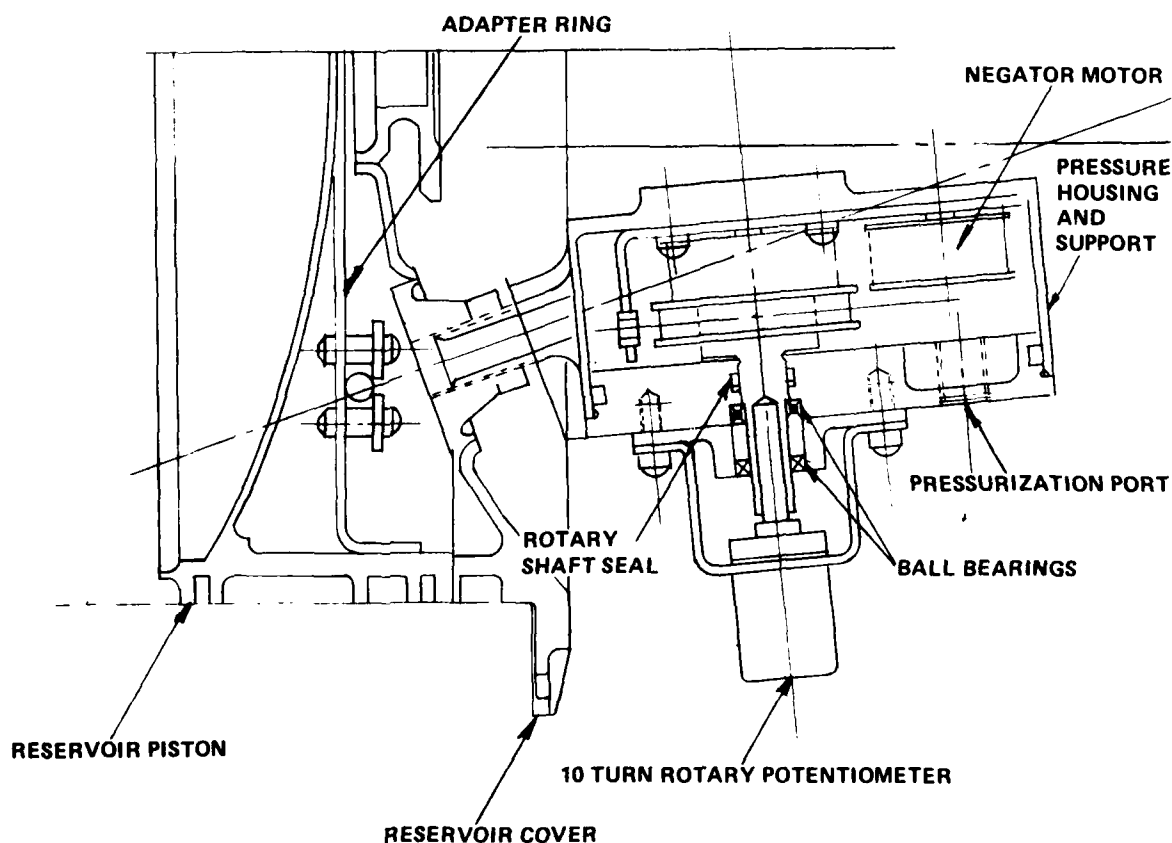
Figure 4. A-6E reservoir sensing logic.

- Spring Torque 1.56 lb-in.
- Cable Tension 2 lb
- Cable Length 72 in.
- Number of Revolutions 15
- Min Endurance Cycles 2500

The motor assembly was mounted in the 1491-901-306 remote sensor housing with the cable terminal modified from a coil to a bead. This cable bead was free to float in the modified piston adapter ring.

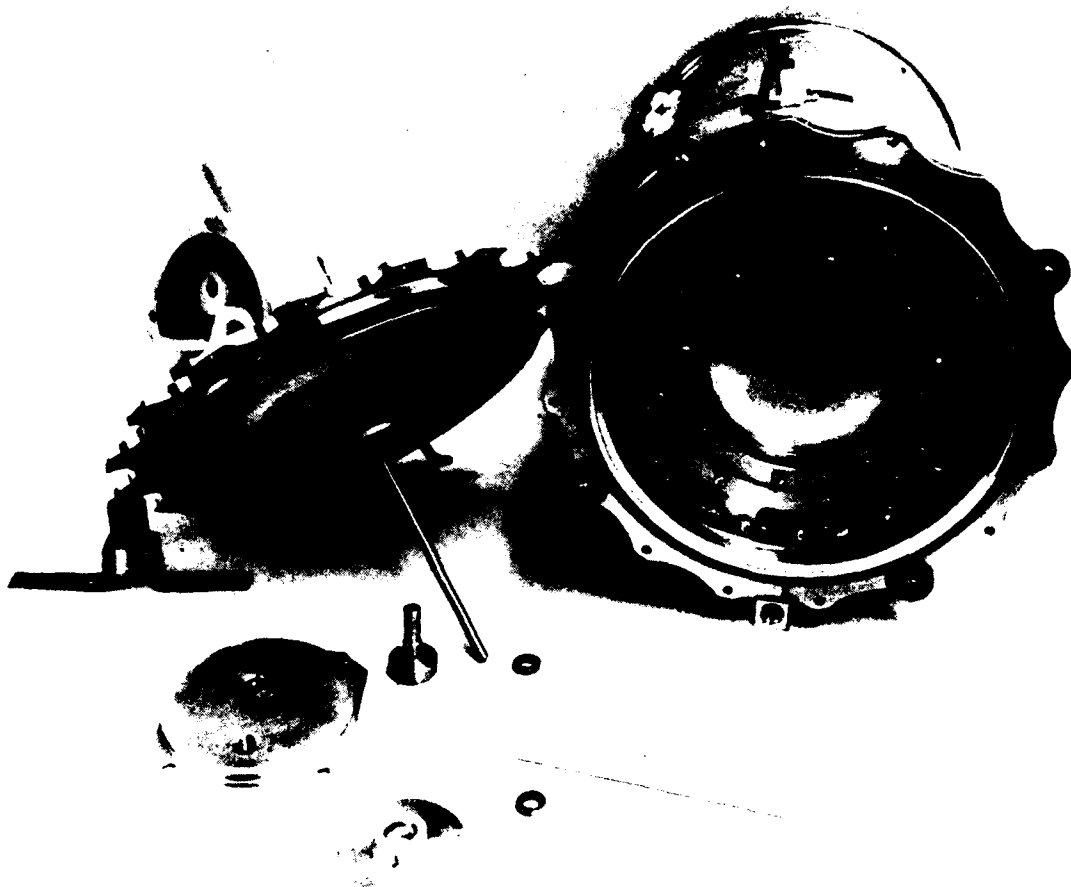
A rotary potentiometer was attached to the driving end of the motor assembly as specified in Grumman Specification 209. Some pertinent data includes:

- Type: 10-Turn



R80-2038-005(T)

Figure 5. Modified reservoir (level sensing).

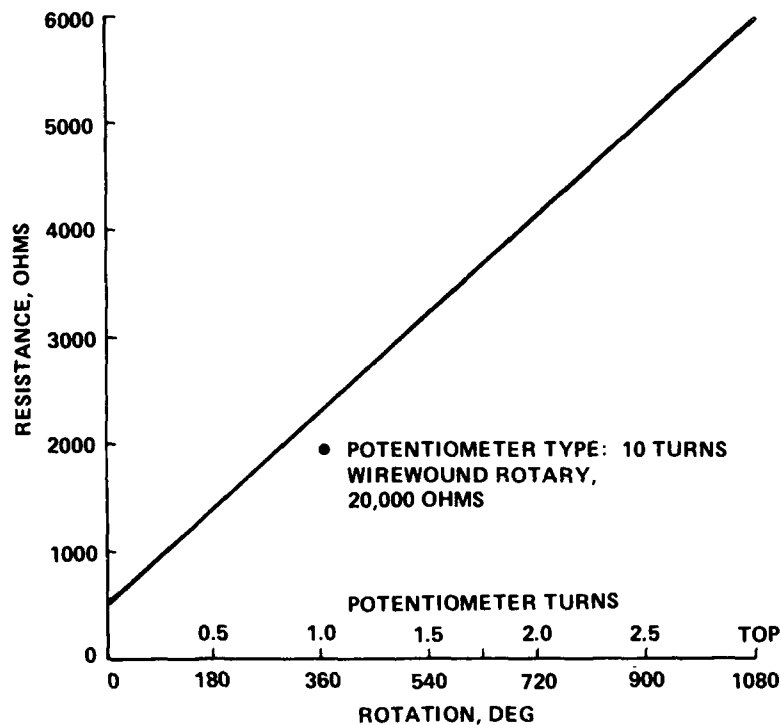


R80-2038-006(T)

Figure 6. Modified reservoir subassembly and details.

- Element: Wirewound
- Dimensions: 0.875 in. OD
1.00 in. long
- Resistance: 20,000 Ohms
- Power Rating: 2 W
- Temperature Range: -65 to 255°F
- Torque: 0.60 oz-in. maximum
- Weight: 1 oz
- Resolution: 0.014%

Full travel of the hydraulic reservoir piston is 13.31 in. This piston movement relates to approximately three turns of the potentiometer, which is approximately 6000 Ohms. Figure 7 shows a calibration curve prepared in the Plant 14 Laboratory.

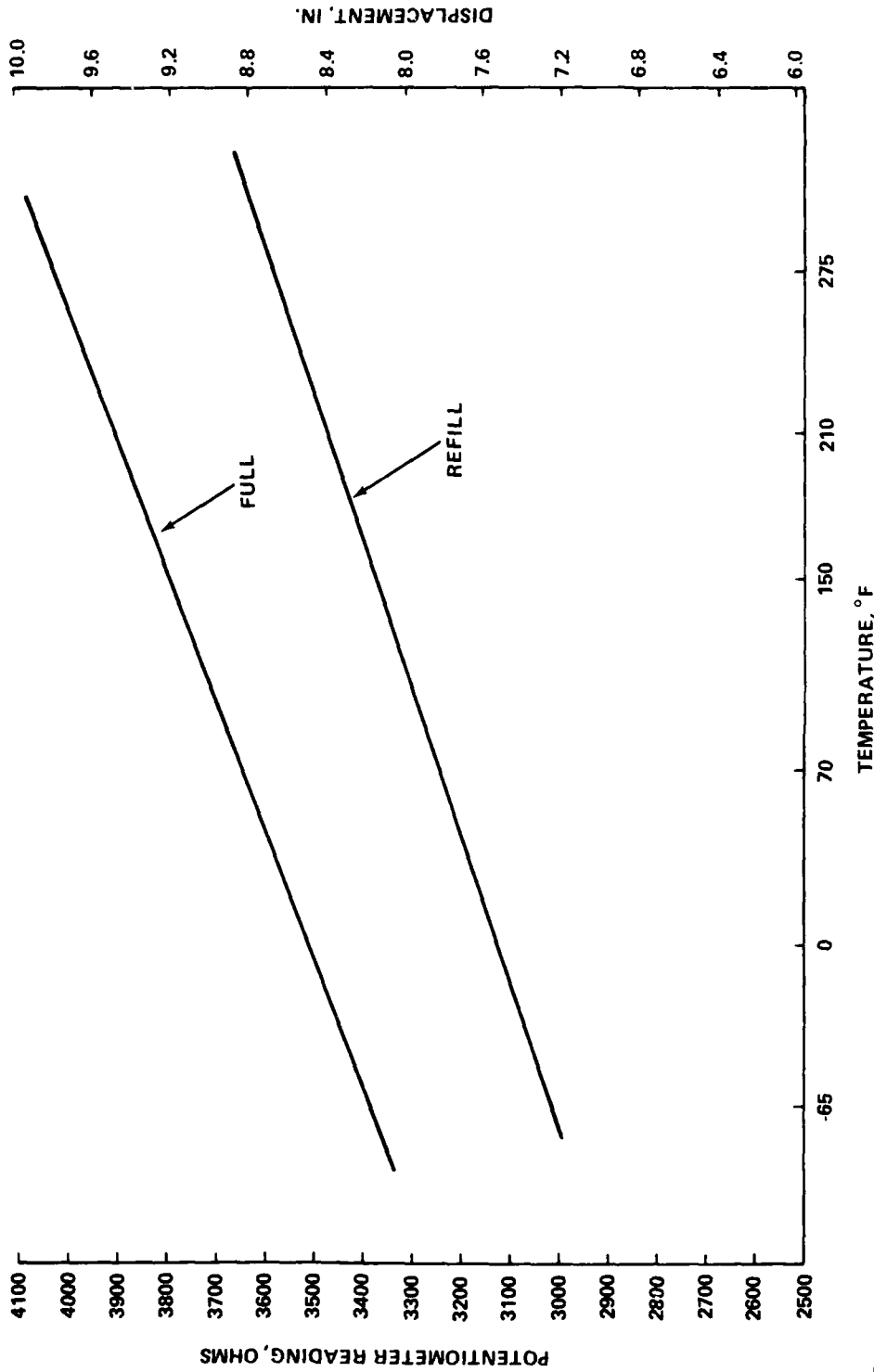


R80-2038-007(T)

Figure 7. Hydraulic reservoir (laboratory calibration curve).

Considerations of temperature and entrained air variations provide the curves shown in Figures 8 and 9. Since the reservoir pressurization is only 40 psi, significant volumes of entrained air are required to cause measurable piston displacements between the pressurized and nonpressurized state. Hysteresis is limited to 2 psi in either direction.

Another factor considered but not applied in reservoir level sensing is piston movement/depletion time versus leak rate for both the combined and flight system. These curves (Figures 10 and 11) give an indication of reservoir depletion time in minutes versus varying leak rates. The initial datum point is taken at the refill mark of each reservoir. If each respective reservoir is full, the time to depletion is proportionately longer.



R80-2038-008(T)

Figure 8. Reservoir calibration curve considering fluid temperature variation.

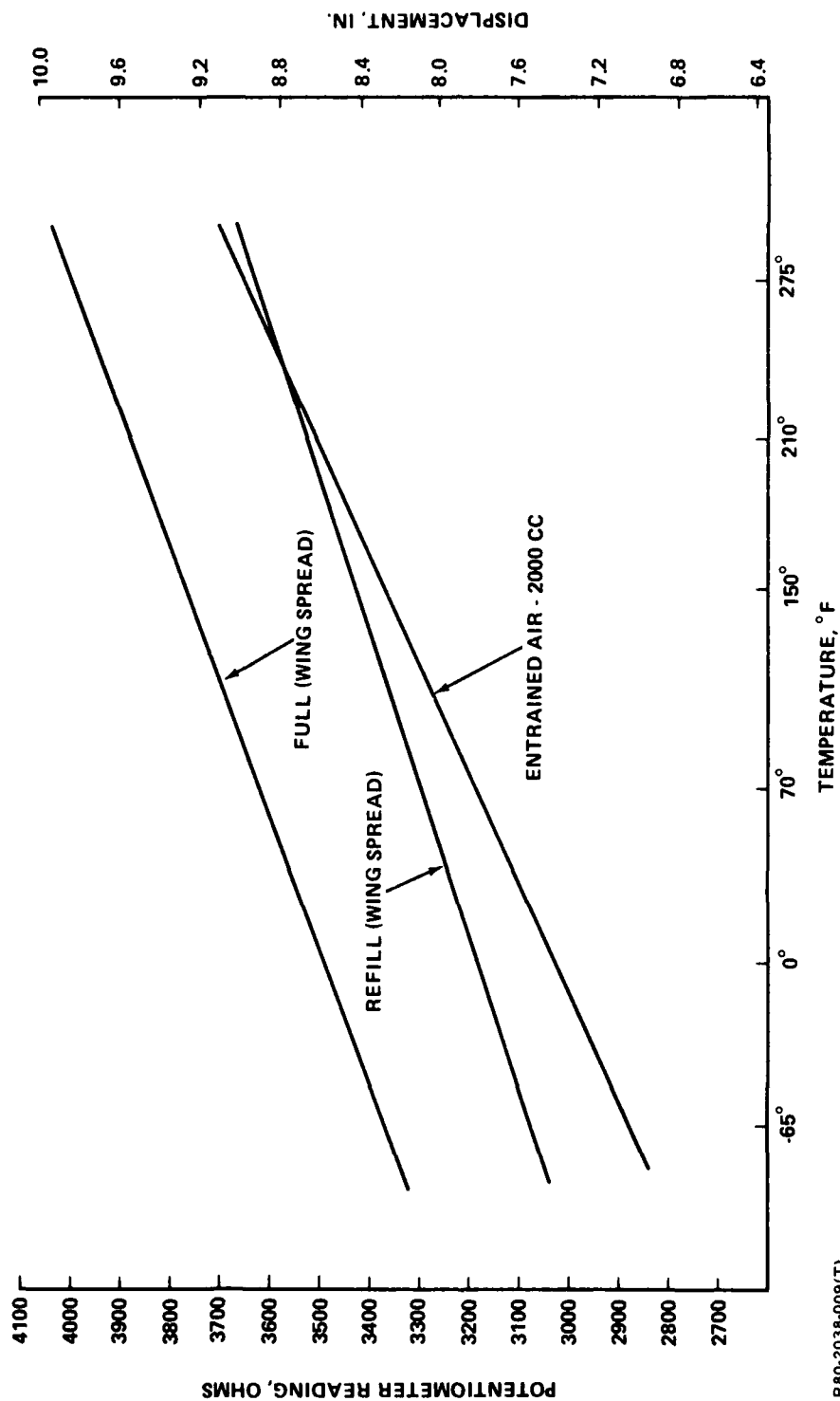


Figure 9. Calibration curve considering entrained air and temperature variation.

R80-2038-009(T)

1.3.1.4 Temperature Transducer

The temperature sensor utilized a two-terminal I/C temperature transducer manufactured by Analog Devices of Norwood, Massachusetts.

The transducer, part no. AD590.C, produces an output current proportional to absolute temperature. With a supply voltage of 5 VDC, the device acts as a high-impedance, constant-current regulator passing $1\mu\text{A}/^\circ\text{K}$. Table 1 (extracted from Ref. 1) shows pertinent technical data.

TABLE 1. IC TEMPERATURE TRANSDUCER DATA.

- TYPE: ANALOG DEVICES AD 590.C
- OUTPUT: $1\mu\text{A}/^\circ\text{K}$
- OPERATING TEMP RANGE: -55°C TO 150°C (-67°F TO 302°F)
- TWO-TERMINAL DEVICE: VOLTAGE IN/CURRENT OUT
- CALIBRATION ACCURACY: $\pm 1^\circ\text{C}$
- LINEARITY: $\pm 0.5^\circ\text{C}$ OVER FULL RANGE
- POWER SUPPLY RANGE: +4 VDC TO +30 VDC
- SIZE: TO -52 PACKAGE

R80-2038-012(T)

Figure 12 (extracted from Ref. 1) shows a voltage-current plot for a typical transducer. Note that the current is essentially flat with an input voltage of 3 to 30 VDC.

The transducer was selected for its small size, performance, and compatability. Figure 13 shows the actual calibration for the unit.

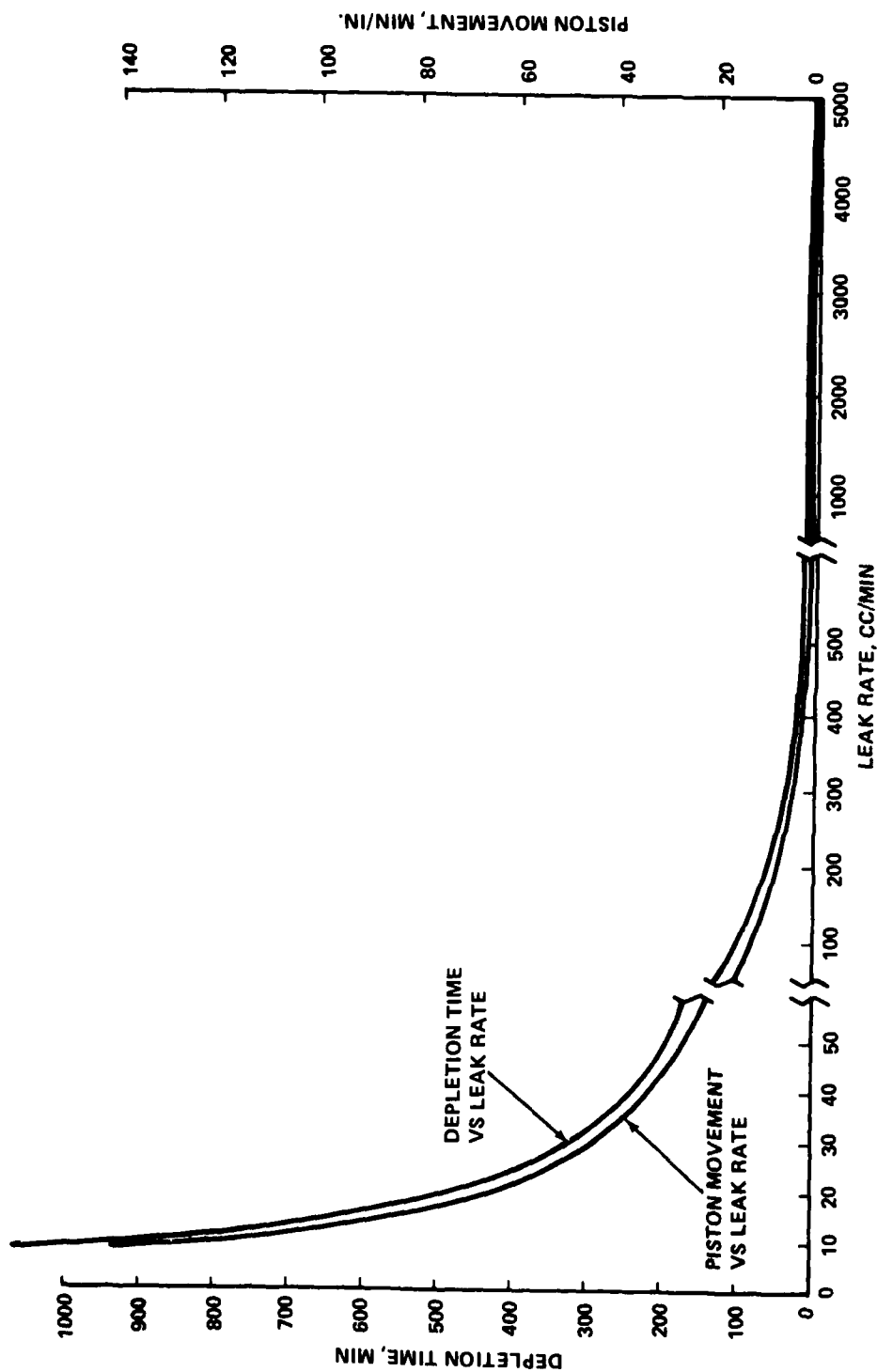
The final subassembly is shown in Figure 14 before potting and assembly. This sensor is used both in the reservoir-level sensing circuit (Figure 15) and in the accumulator circuit discussed in a later section.

1.3.1.5 Optical Desiccant Sensor

Some hydraulic systems (such as the A-6E) are pneumatically pressurized, utilizing regulated engine compressor bleed air.

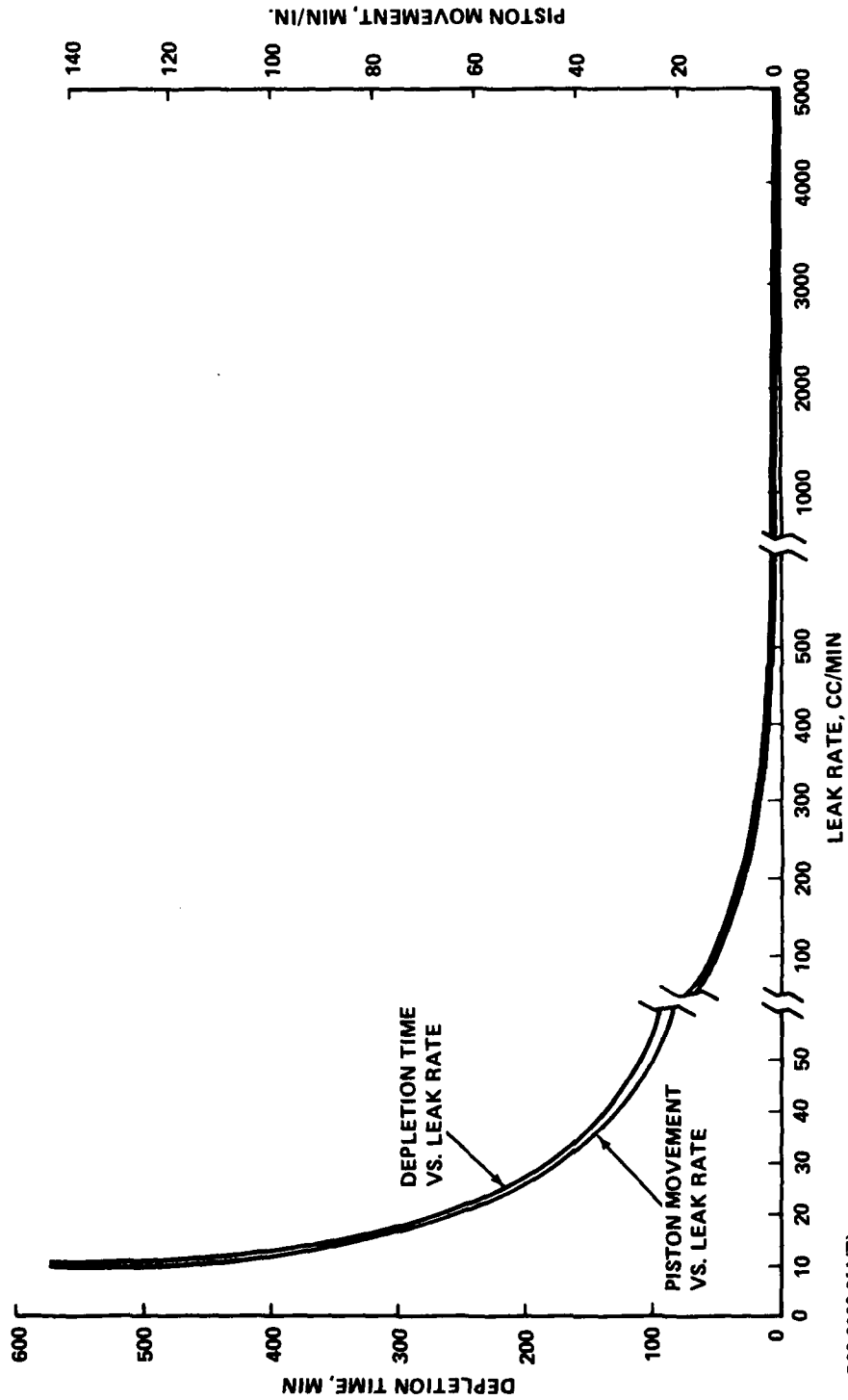
A desiccant is used to dry the makeup air used to pressurize the reservoir. The cartridges are replaced on periodic intervals predicated on vehicle system usage. In order to remotely detect a saturated condition, a colored desiccant cartridge is placed in series with the existing unit since the latter could not be readily modified.

The selected sensor was made by Delaval Special Products Division and conforms to Grumman Specification Number 205. The sensor measures approximately 5 in. x 3 in. long, has a transparent housing, and is rated for 100 psi operating pressure. The unit



R80-2038-010(T)

Figure 10. Combined reservoir depletion rate vs time.



R80-2038-011(7)

Figure 11. Flight reservoir depletion rate vs time.

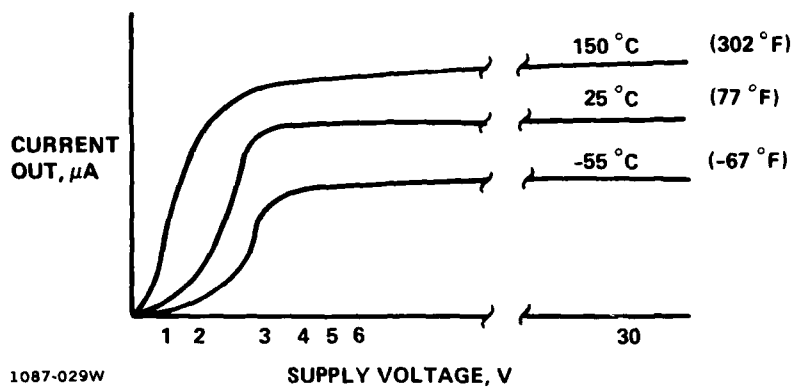


Figure 12. Voltage-current plot for an IC transducer.

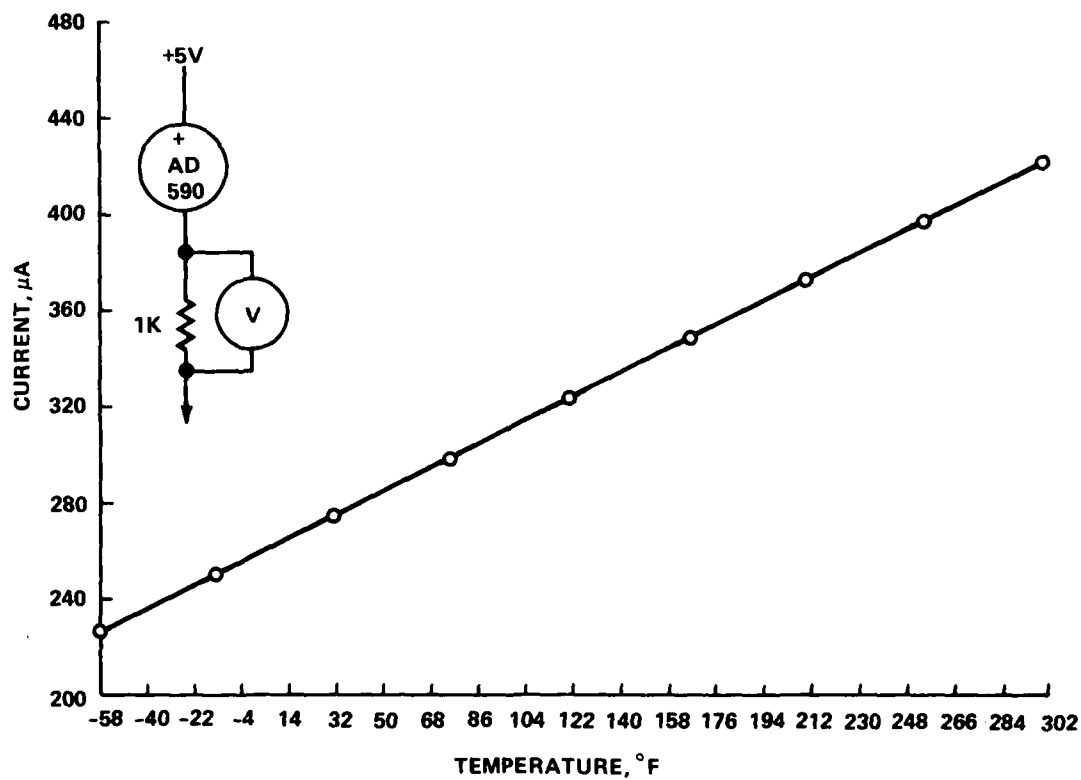
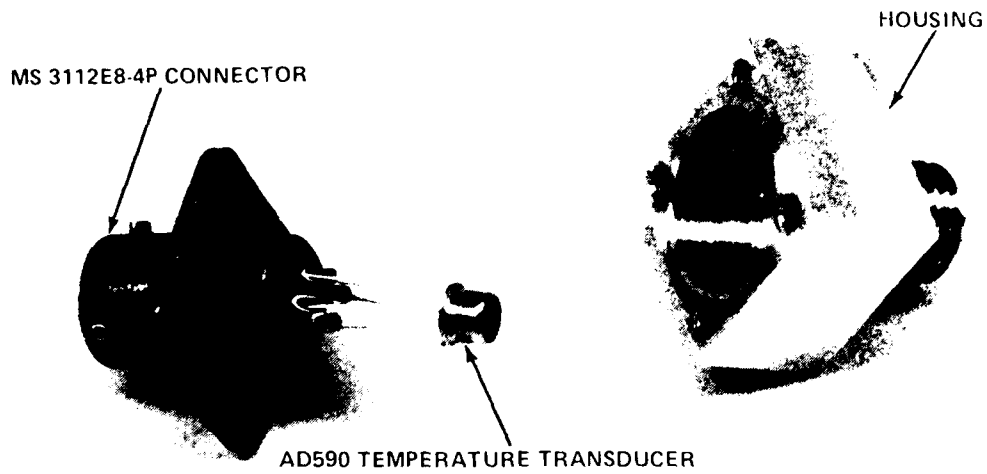


Figure 13. Calibration curve for an IC transducer.



R80-2038-015(T)

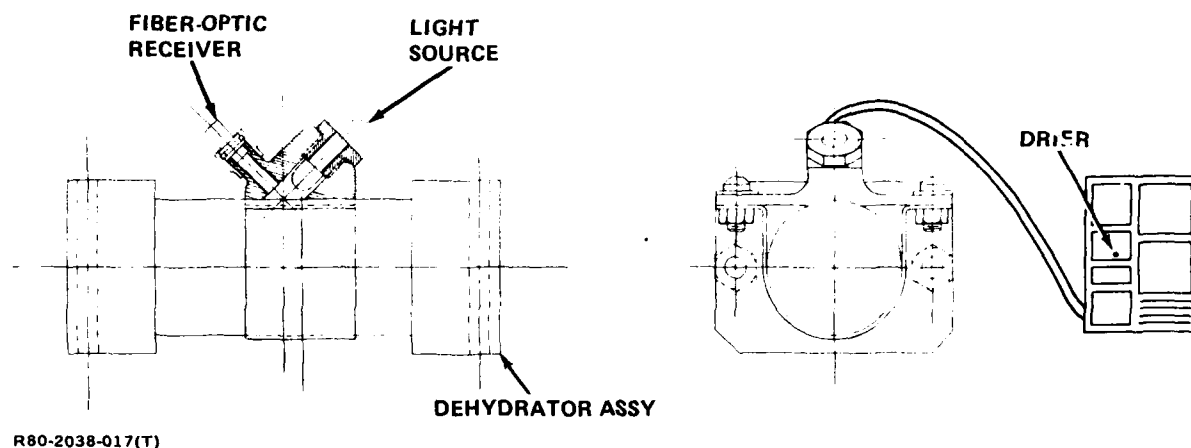
Figure 14. Temperature transducer assembly.



Figure 15. Reservoir temperature sensor installation.

contains approximately 2.6 in.³ of dyed silica gel conforming to Military Specification MIL-D-3716, Type IV. The initial color of the desiccant is deep to pale blue, depending on the desiccant condition. The color changes from pale blue to pink as the unit becomes saturated.

Reading desiccant condition remotely is accomplished by using reflected colored light from the irregular desiccant granules through the transparent housing. Figure 16 shows the concept employed to accomplish this objective.



R80-2038-017(T)

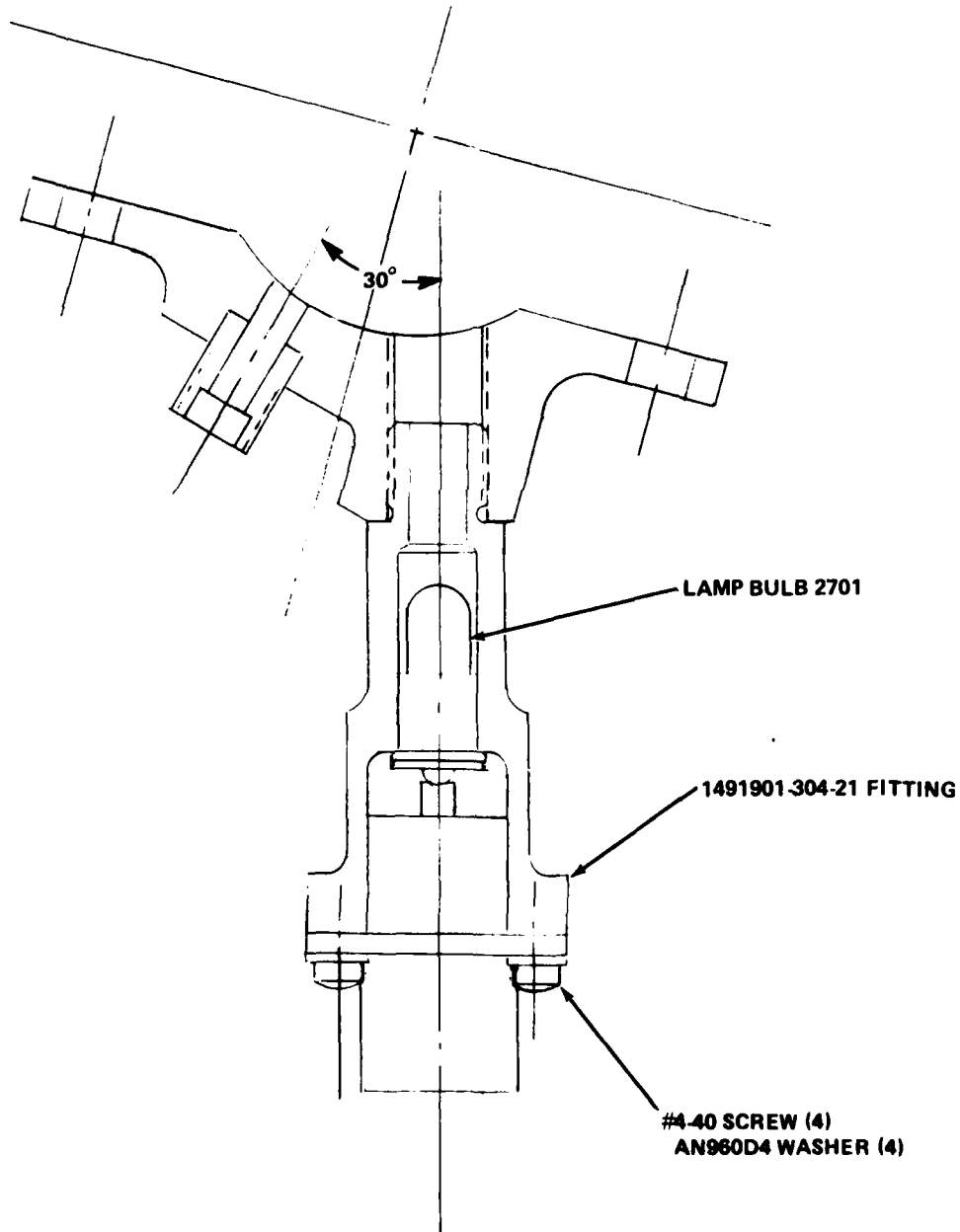
Figure 16. Optical desiccant sensor (early approach).

Initial test results revealed that a major portion of the light was being reflected by the transparent housing since the light transmitter and receiver were on the same axis. The light source transmitter-receiver angle was changed from 13° to 30°. No substantial improvements were noted. Various reflected angles were tested with the transmitter and receiver perpendicular to the desiccant housing axis in order to determine the maximum reflected light. This condition occurred with an included angle of 30 degrees between the transmitter and receiver. A second sensor housing (Figure 17) was originally made to support the grain of wheat light source and the fiber-optic terminal receiver. Subsequent testing revealed that color transmission became apparent but the intensity was not discernable to the viewer at the display panel.

Additional development effort dictated that the light source be brought closer to the transparent housing in order to increase the intensity of reflected light. A light source with a condensing lens was obtained to focus the light rays to one point. This change improved the reflective properties but, due to the irregular shape of the desiccant, the reflected light scatters in many directions and makes reflected colored light

difficult. As a final attempt a condensing lens was used on the reflected light source to intensify the reflected color.

The light source for the sensor was originally a grain-of-wheat bulb, but its intensity after passing through the desiccant was not strong enough to be seen at the display panel. The grain-of-wheat bulb was then replaced by a General Electric No. 2701



R80-2038-018(T)

Figure 17. Sensor assembly.

halogen lamp requiring an operating voltage of 3.5 VDC and developing a maximum of 3.5 W, increasing the intensity by a factor of 20. Figure 18 shows plots of voltage, current, and power versus light intensity of the grain-of-wheat bulb; similar plots for the halogen bulb are shown in Figure 19. A comparison of the power versus light intensity of the grain-of-wheat and halogen bulbs is given in Figure 20.

ven with the halogen lamp, the reflected color properties were affected by the irregular angles of the desiccant crystals. Figure 21 shows the interim desiccant sensor installation. A decision was made to eliminate the desiccant and develop a moisture sensor. After several laboratory attempts, a disc was developed.

The desiccant sensor is a mixture of potassium bromide and cobaltous chloride, in a two-to-one ratio by weight, respectively. A description of the two components used in the desiccant is given in Table 2 (extracted from Ref. 2). The mixture is compressed into a half-inch diameter disc under a pressure of 22,000 psi and a vacuum of 25 in. mercury for 2 min. In order to focus the translucent disc color to a narrow point, a condensing lens was used adjacent to the disc support.

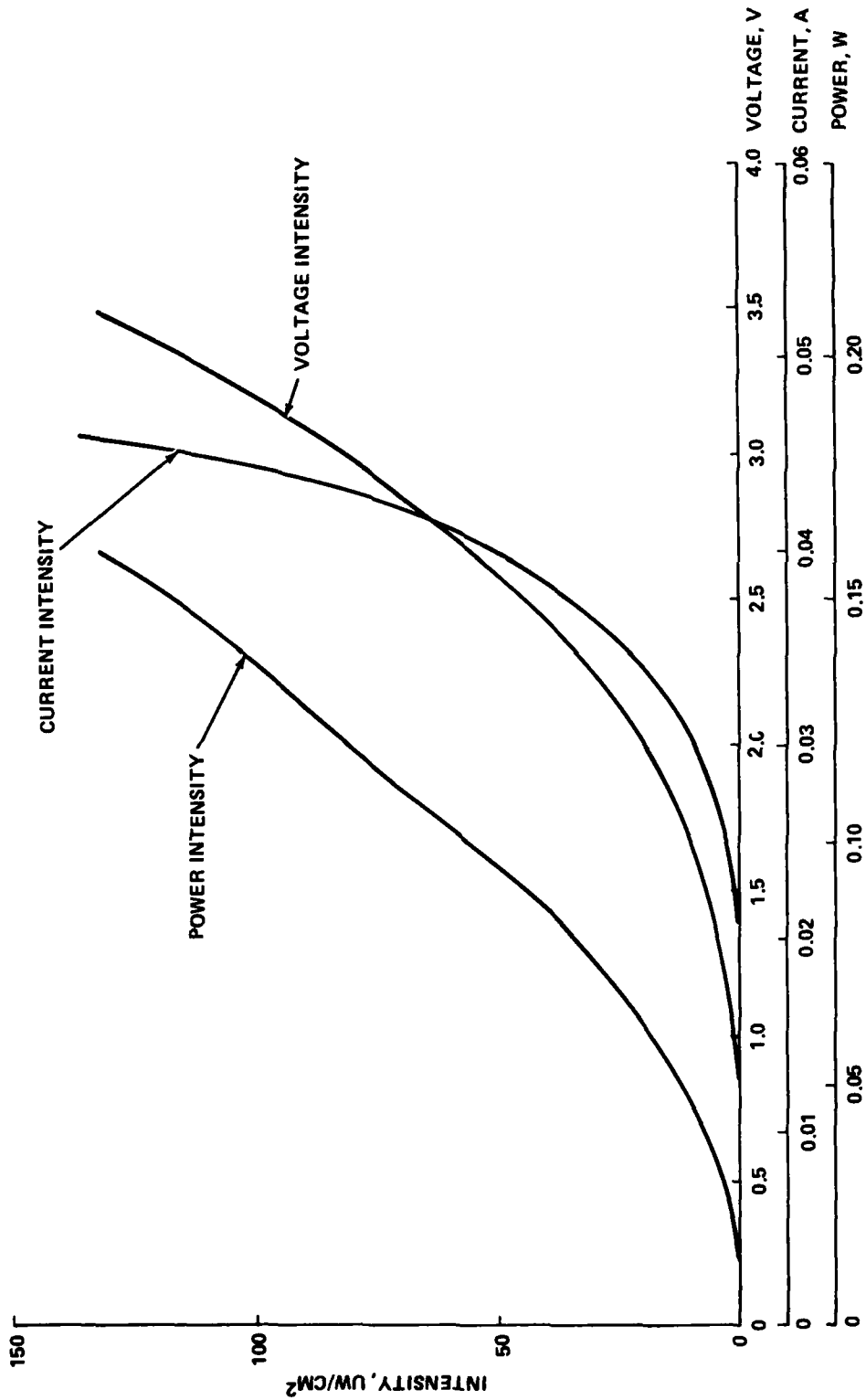
The lens is a condensing plano-convex lens Stock No. 10.0015 made by Rolyn Optics Company, Arcadia, California. The lens is made of spectacle crown glass (B-270) having a diameter of $0.295 \pm .02$ in. and a focal length of 0.512 in. $\pm 5\%$, as shown in Figure 22. The power of this lens is the reciprocal of the focal length, which gives a power of approximately 2 in.^{-1} or 76.9 diopters.

The lens and desiccant disc are mounted inside the cartridge by a slide type assembly, shown in Figure 23. The slide is secured in position by the gasket, screen filter, and felt rings in the end covers. The complete assembly is coupled with two through bolts.

Since no suitable halogen bulb lamp holders were available, one had to be designed and fabricated to support the bulb and provide the proper mechanical/electrical interface. The resultant design was the 1491-304-21 optical desiccant fitting shown in Figure 24. A modified MS connector supplied power to the lamp. In order to reduce the voltage from 5 VDC to approximately 3.5 V, a 20-Ohm, 5-W resistor was used in the mating connector.

Specifications for the light source are as follows:

- GE Lamp Number 2701
- Voltage 3.5 V



R80-2038-019(T)

Figure 18. Grain-of-wheat bulb characteristic.

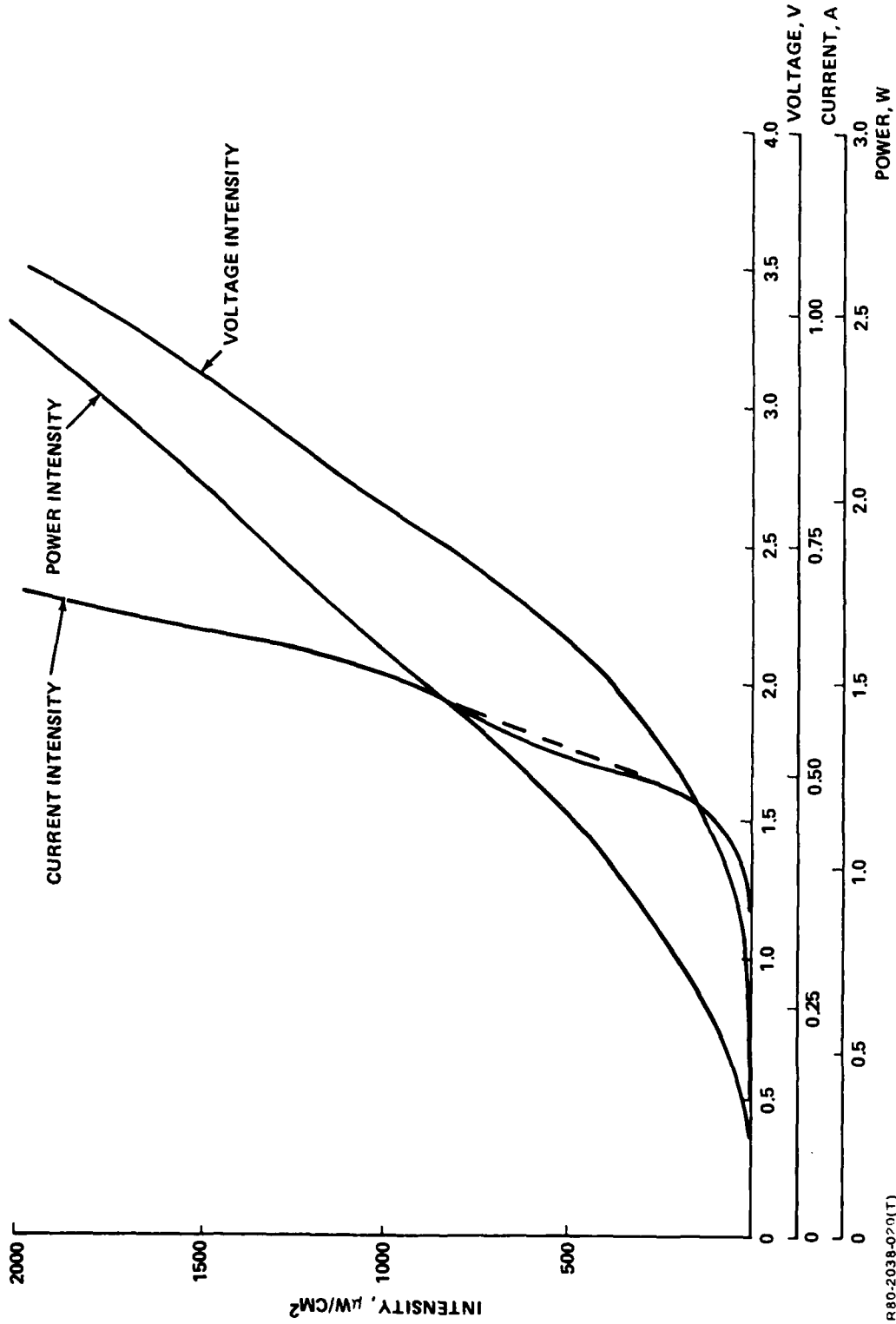
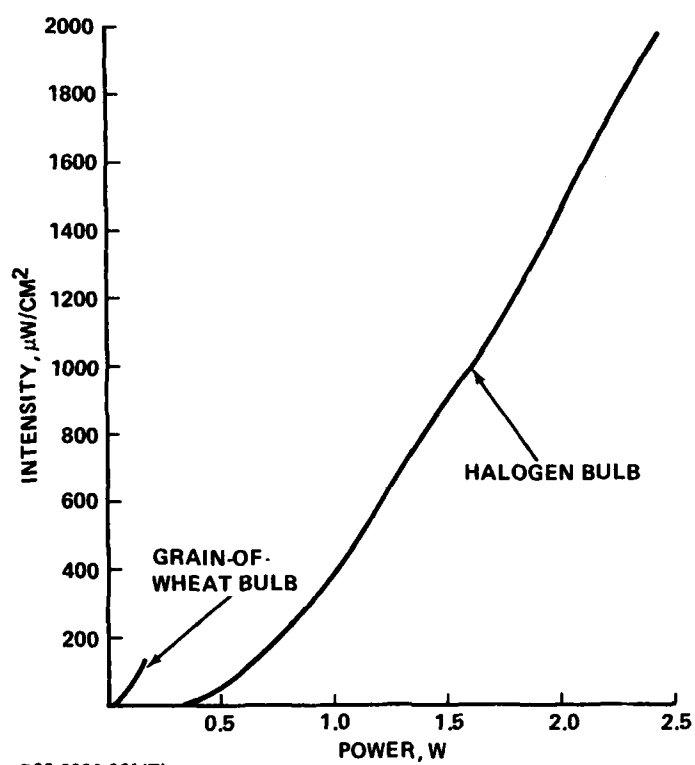
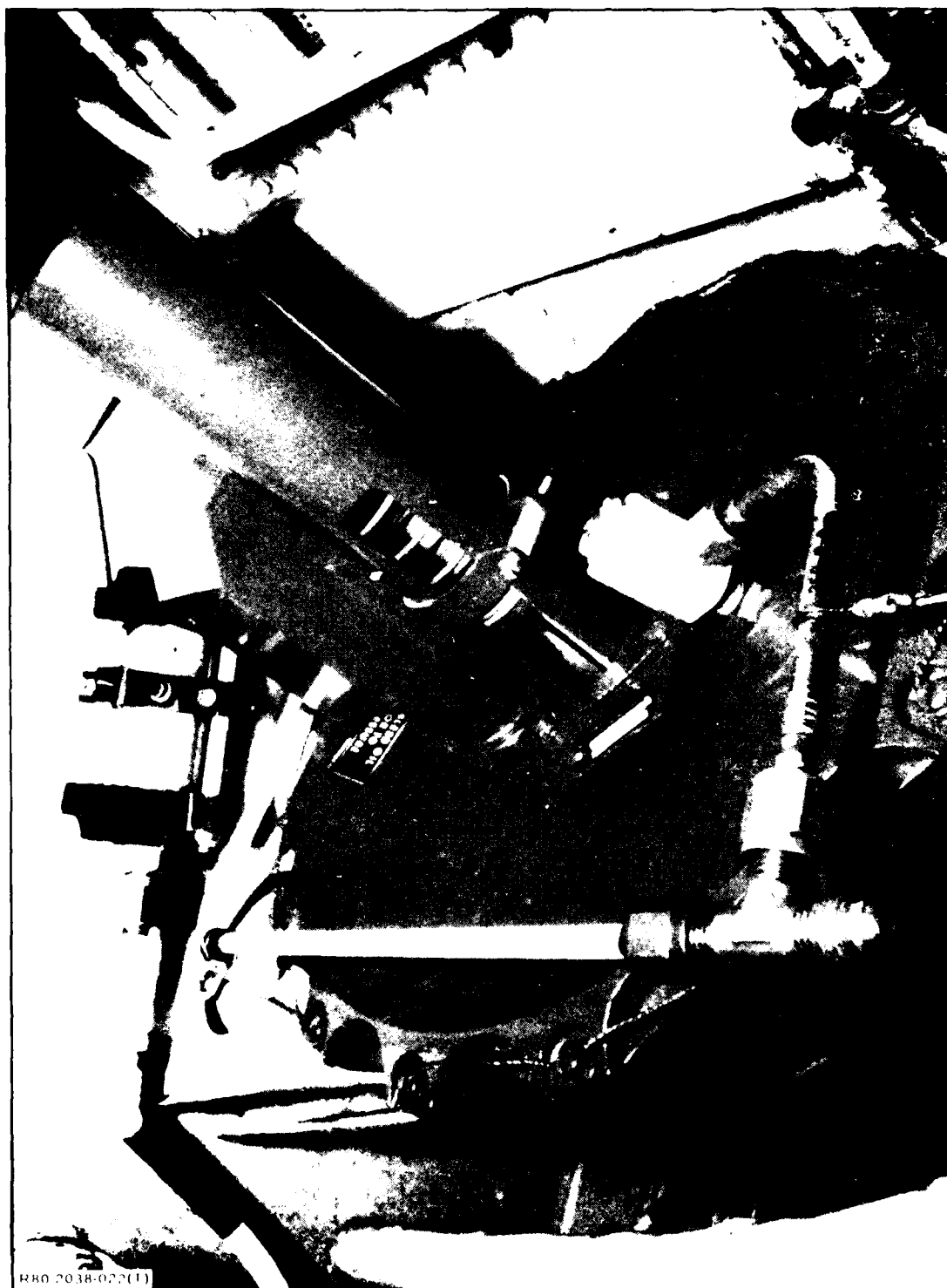


Figure 19. Halogen bulb characteristic.



R80-2038-021(T)

Figure 20. Grain-of-wheat bulb/halogen bulb comparison.



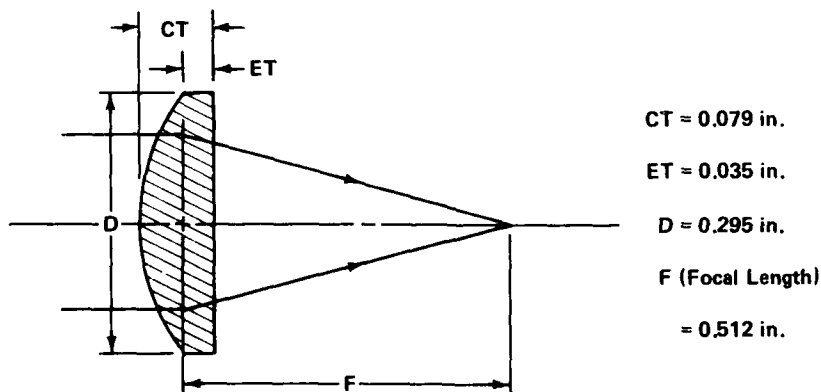
R80 2038-027(1)

Figure 21. Interim desiccant sensor installation.

TABLE 2. DESICCANT COMPONENTS.

POTASSIUM BROMIDE, KBr	COBALTOUS CHLORIDE (COBALT CHLORIDE (A) CoCl_2 (B) $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$)
<p>PROPERTIES: WHITE, CRYSTALLINE GRANULES OR POWDER; PUNGENT, STRONG, BITTER SALINE TASTE; SOMEWHAT HYGROSCOPIC. SOLUBLE IN WATER AND GLYCERIN; SLIGHTLY SOLUBLE IN ALCOHOL AND ETHER; SP GR 2.749; M.P. 730°C; H.P. 1435°C.</p> <p>DERIVATION: SOLUTIONS OF IRON BROMIDE AND POTASSIUM CARBONATE ARE MIXED AND HEATED THE SOLUTION FILTERED AND CONCENTRATED AND THE BROMIDE CRYSTALLIZED OUT.</p> <p>GRADES: TECHNICAL, C. P. N.F.; REAGENT; SINGLE CRYSTALS.</p> <p>HAZARD: MODERATELY TOXIC BY INGESTION AND INHALATION.</p> <p>USES: MEDICINE; PHOTOGRAPHY (GELATIN BROMIDE PAPERS AND PLATES); PROCESS ENGRAVING AND LITHOGRAPHY; SPECIAL SOAPS, LABORATORY REAGENT.</p>	<p>PROPERTIES: (A) BLUE (B) RUBY-RED CRYSTAL. SOLUBLE IN WATER AND ALCOHOL; ALSO SOLUBLE IN ACETONE. SP GR (A) 3.348 (B) 1.924; M.P. (A) SUBLIMES (B) 86.75°C.</p> <p>DERIVATION: BY THE ACTION OF HYDROCHLORIC ACID ON COBALT, ITS OXIDE, HYDROXIDE OR NATE. CONCENTRATION GIVES (B) AND DEHYDRATION (A).</p> <p>USES: ABSORBENT FOR AMMONIA; GAS-MASKS; ELECTROPLATING, SYMPATHETIC INKS, HYGROMETER IN SOILS AND ANIMAL FEEDS; VITAMIN B_{12}; FOR MAGNESIUM REFINING; SOLID LUBRICANT; MORDANT; CATALYST; BAROMETERS.</p>

R80-2038-023(T)



R80-2038-024(T)

Figure 22. Plano-convex lens.

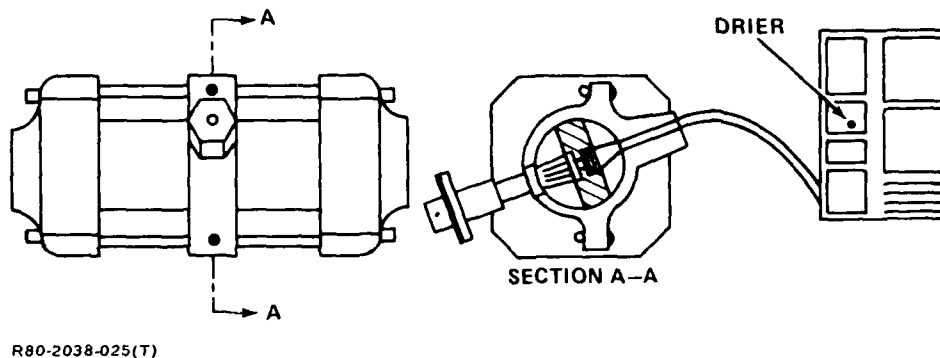


Figure 23. Moisture detector fiber-optic circuit.

- Power 2.5 W
- Life 20 hr
- Bulb Type TL 1/2
- Dimensions 0.625 x 0.285 in.

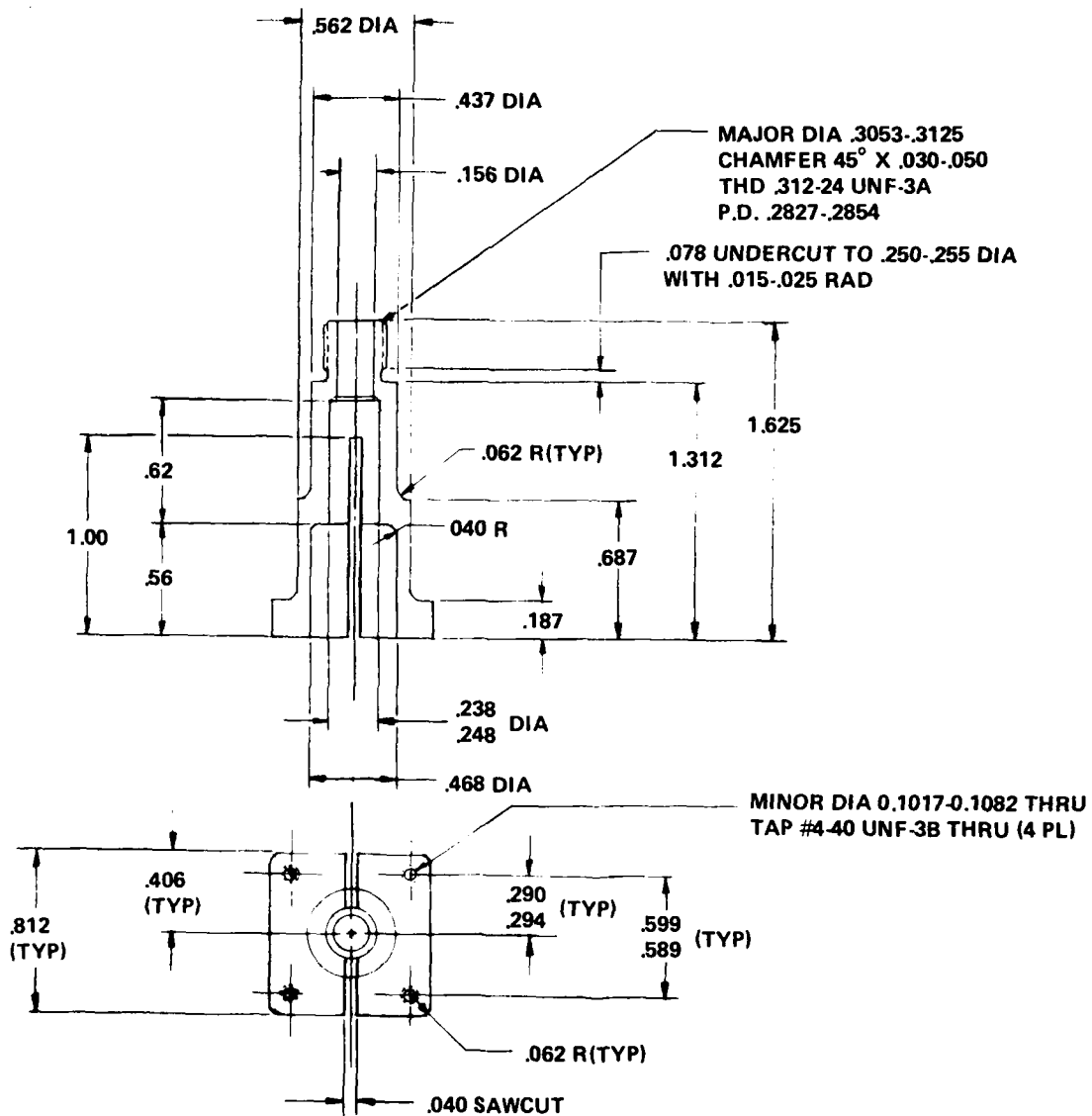
Desiccant Fiber-Optic Link. In an effort to improve visibility at the display, power optical measurements were taken using a recently purchased Photodyne Model 22XL optical multimeter. The results indicated that the cable running from the optical sensor to the display unit had an unsatisfactory 32 db/m optical loss instead of 10 db/m, which would normally be expected with a properly installed line run. The fact that the cable run was installed during vehicle buildup precluded improvements in this area.

1.3.2 Pneumatic Bottles

1.3.2.1 Description

Pneumatic bottles are energy storage devices which are used as an emergency backup to a principal system. Servicing these bottles requires that the maintenance technician compensate for topping pressure as a function of ambient temperature. A typical nitrogen bottle service card is shown in Figure 25 (Ref. 3).

In this flight test program, two of the eight stored energy sources were modified to accept HYCOS sensors. One landing gear door dump bottle (Figure 27) was modified to accept a temperature-compensated pressure switch and a fiber-optic liquid detection circuit. The second emergency canopy dump bottle (Figure 26) was modified to accept another temperature-compensated pressure switch. Special fittings were manufactured to provide sensor bosses.



-21 FITTING
 MATERIAL: AL ALLOY 7075-T73
 FINISH: BLACK ANODIZE PER MIL-A-8625 TYPE II

R80-2038-026(T)

Figure 24. No. 1491901-304-21 optical desiccant fitting.

NADC 81073-60

REQ A-13	NAVAIR 01-85ADA-6-4 Date: 1 December 1977	CHANGE NO.	PHASE A	TEST PAR ON
TEST AREA	WORK UNIT CODE	TIME 01:30	RIS AMH NO. 1	MOD. 6053 NO. 1
			LANDING GEAR EMERGENCY OPERATIONAL CHECK	
			Assisted by AMH-2 (90.0 Min) AMH-3 (90.0 Min) AMH-4 (90.0 Min)	
			GROUND SUPPORT EQUIPMENT REQUIRED	
			Adapter, External Hyd Power 128GT10154	
			Power Source, Electric	
			Power Source, Hydraulic	
			Trailer, Nitrogen 515R100	
			Wrench, Torque (0-150 in-lb)	
			CONSUMABLES/REPLACEMENT PARTS	
			Fluid, Hydraulic MIL-H-83282	
			<u>WARNING:</u> Insure wheel well areas are clear of personnel and equipment.	
			Do not turn off elec power source, elec power shall remain on during entire operational check.	
2,4/5			1. Operation Check Emergency Landing Gear system IAW NA 01-85ADA-2-2.2, SECT 3.	
			NOTE: QA (Card A-23) witness task 2 (bottle servicing, swivel nut torque, for pressure loss).	
1,4/9			2. Service landing gear emergency extension bottles IAW NA 01-85ADA-2-1, SECT 6.	
			End of Card (Card A-13.1 Blank)	
R80-2038-027(T)				

Figure 25. Typical service card.

1.3.2.2 Temperature-Compensated Pressure Switch

At the onset of the program, it became evident that temperature-compensated pressure switches were not off-the-shelf hardware. NeoDyn Incorporated of Chatsworth, California, was contracted to develop and build temperature-compensated pressure switches for the hydraulic monitoring system program. An initial Grumman sensor specification (Number 204) was prepared.

Switch Description. The switch is an all-welded, hermetically sealed unit which physically conforms to Figure 28. The switch senses applied pressure and compares it to an internal sealed self-contained reference pressure within the probe, which is at the same temperature as the sensed media. A proprietary, welded stainless-steel sensing diaphragm is exposed to the probe reference pressure on one side and to the sensed pressure on the other side. Pressure settings, which vary as a function of sensed and reference pressure, are accomplished through a force balance interaction between a sensing diaphragm and a Belleville spring reference load. Since the reference pressure varies directly with sensed temperature, pressure settings are a function of temperature. Variation of reference pressure with temperature is shown graphically in Figure 29.

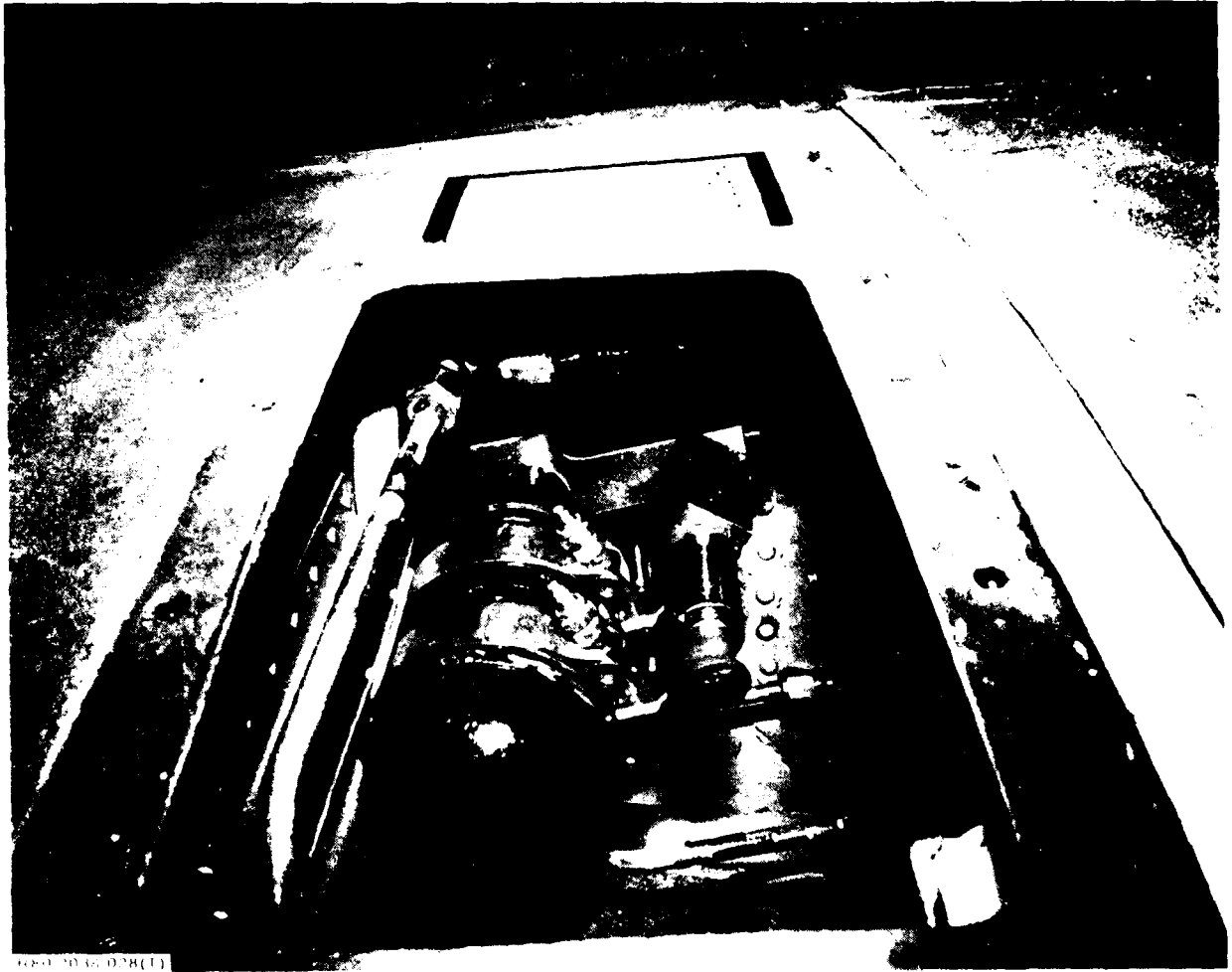


Figure 26. Emergency canopy dump bottle installation.

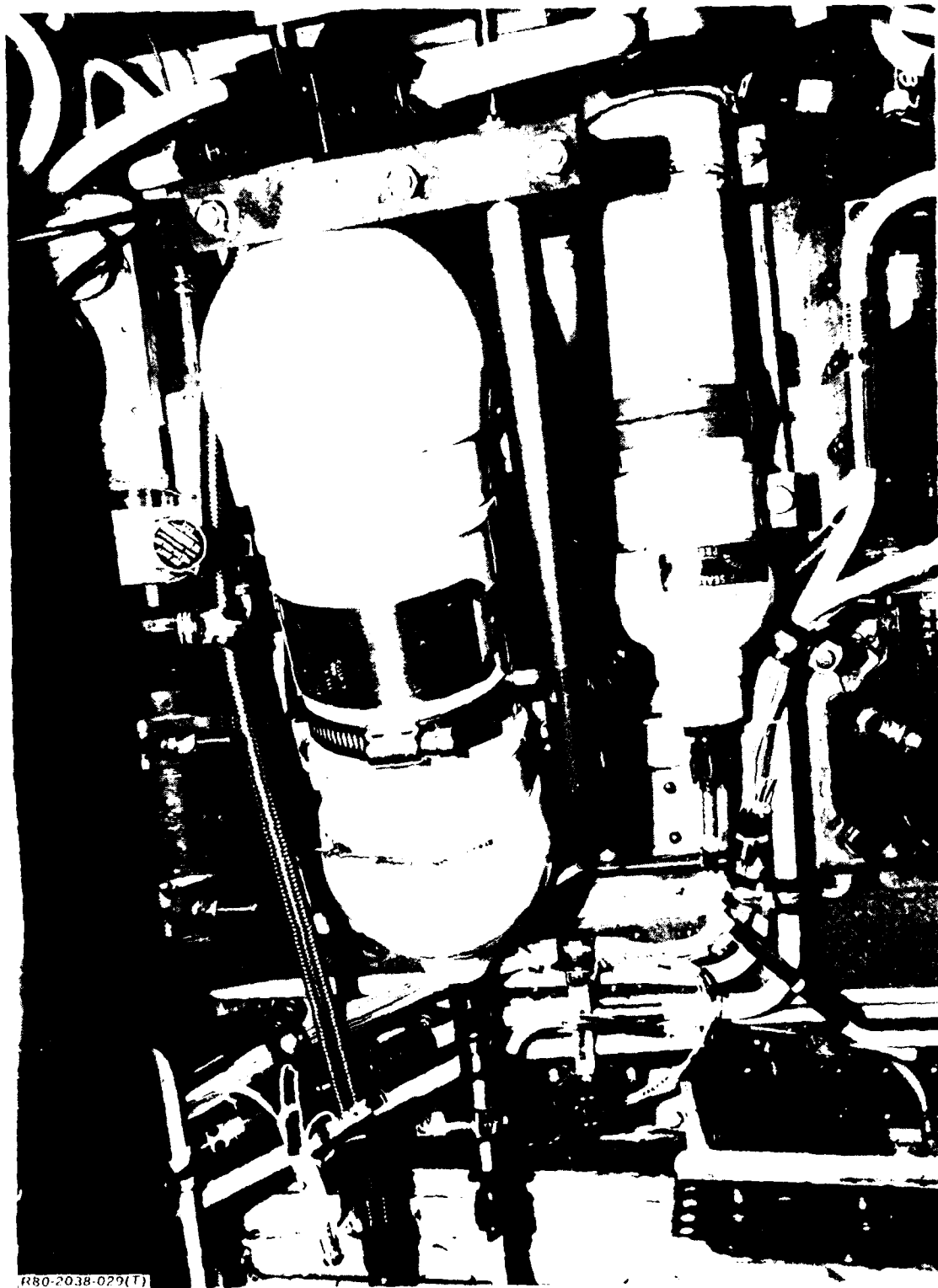
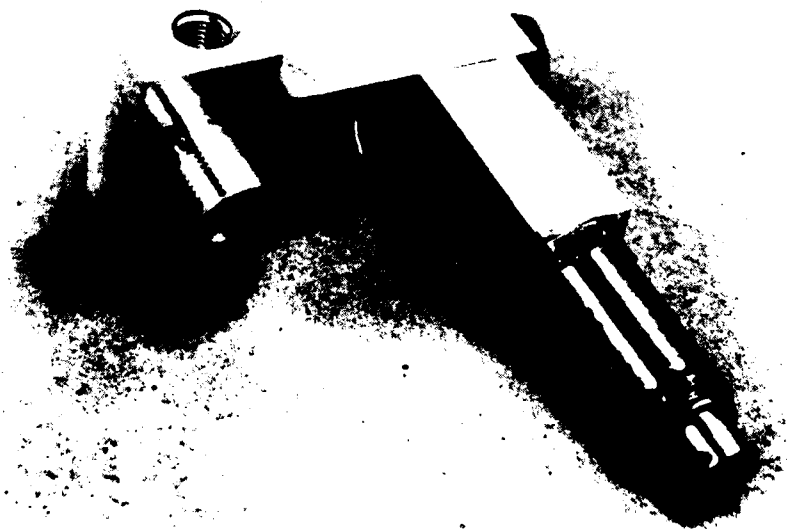
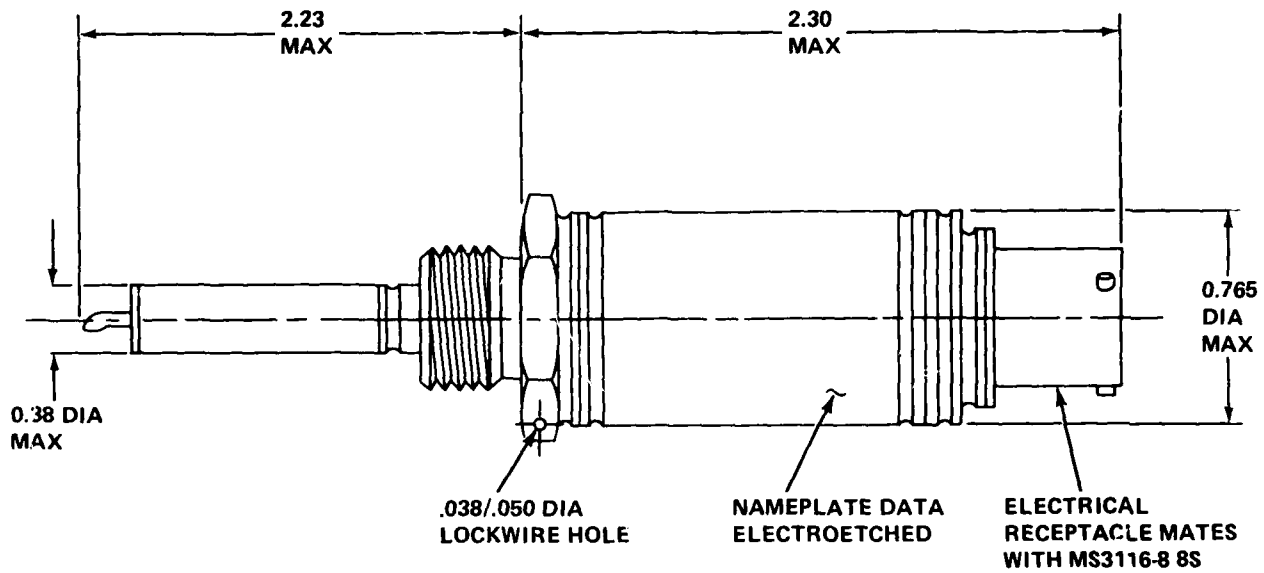
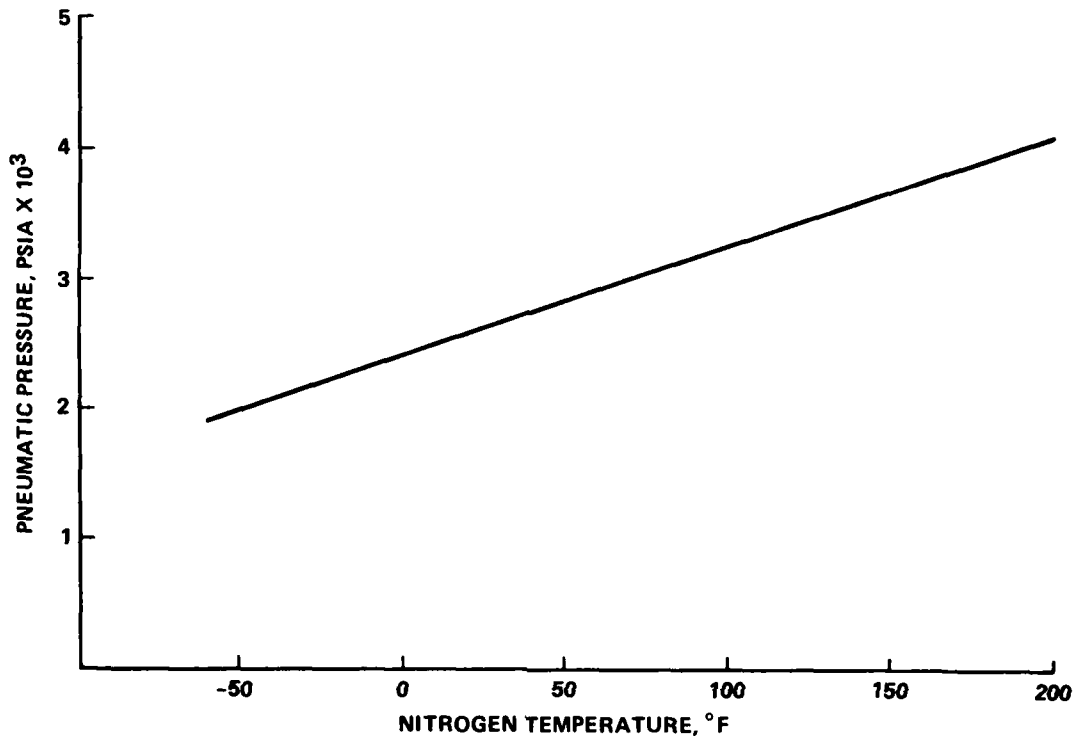


Figure 27. Landing gear door dump bottle installation.



R80-2038-030(T)

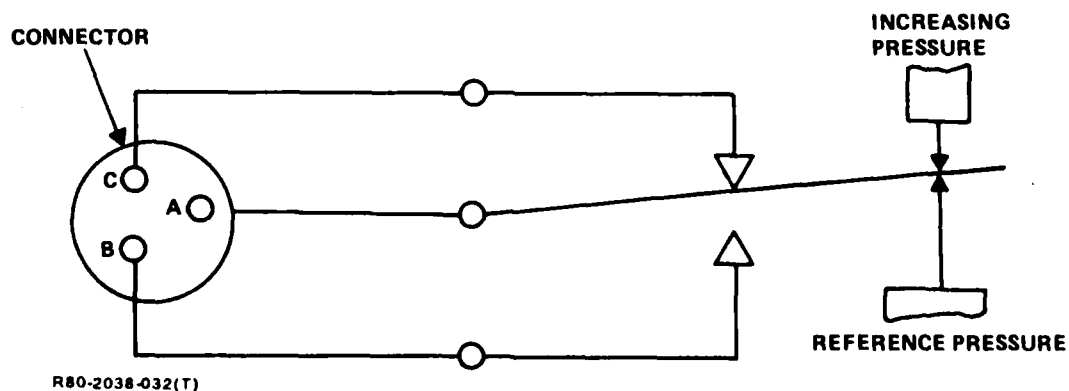
Figure 26. Temperature-compensated pressure switch.



R80-023-031(T)

Figure 29. Plot of pressure vs temperature for nitrogen.

A precision snap-action electrical switch exposed to sensed pressure is positioned within the mechanism stroke limits to provide electrical circuit control at predetermined differences between sensed and reference pressure. The complete assembly is housed within an all-welded, high-pressure hermetically sealing housing. Figure 30 shows the diagrammatic circuit.



R80-2038-032(T)

Figure 30. Temperature-compensated pressure switch: diagrammatic circuit.

Laboratory testing of a penumatic charge at variable temperatures verified the pressure switch temperature concept. Data for this switch (Grumman specification 204-1) is shown in Figure 31.

The reference temperature compensating gas is dry nitrogen that is hermetically sealed within the unit.

Switch Testing. Switch testing was conducted and found to fall within acceptable limits as defined by source control specification 204-2. The test results are listed in Table 3 and plotted in Figure 32.

1.3.2.3 Fiber-Optic Liquid Detection Circuit

The fiber-optic fluid detection circuit employs the properties of refractive index. If a diagonal gap exists between two fibers, light transmission will not jump the gap and will be absorbed by the core. In the presence of suitable fluid, the light will pass through the fluid and appear at the display panel. Water will be indicated by a white light and hydraulic oil will appear as a red light.

The liquid detector concept uses the optical properties of the light-conducting media. It is necessary to determine not only the properties of the light-conducting cables but also those of the fluids.

One of the important parameters of any fluid or light-conducting medium is its refractive index, defined as the ratio of the velocity of light in air to that in a given

- ACTUATION POINTS (SEE GRAPH)
- INCREASING PRESSURE: BY "A" MAX
- DECREASING PRESSURE: WITHIN BAND "B-C"

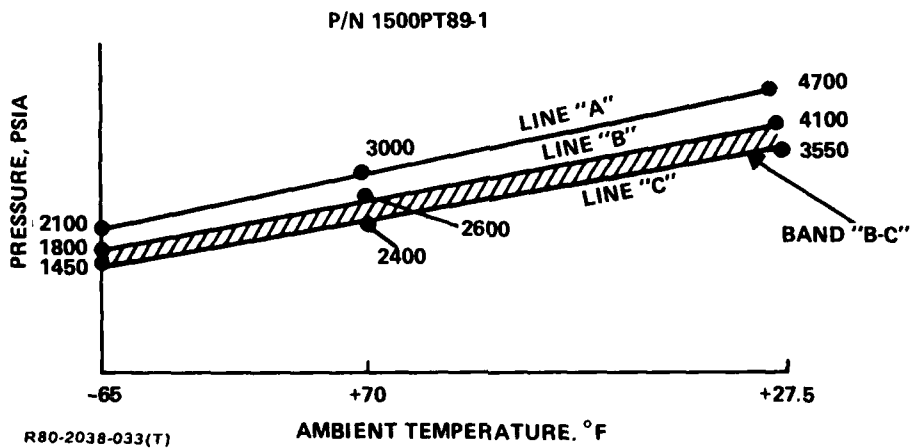


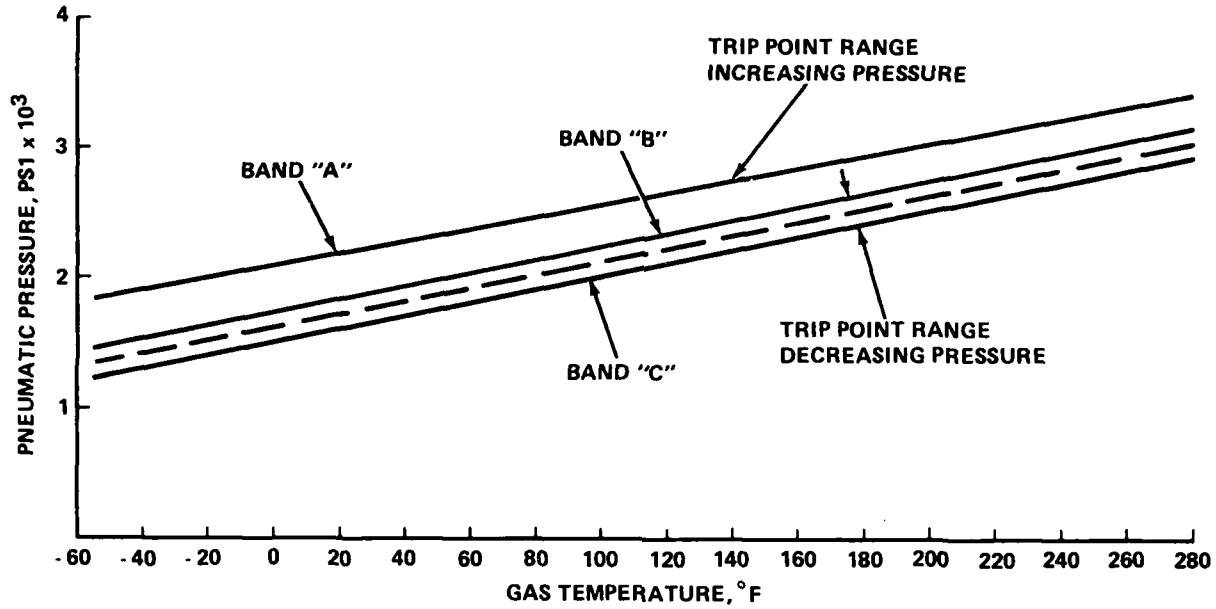
Figure 31. Switch actuation points vs temperature (Specification 204-1)

TABLE 3. TEMPERATURE-COMPENSATED PRESSURE SWITCHES
(GRUMMAN SPECIFICATION 204-2).

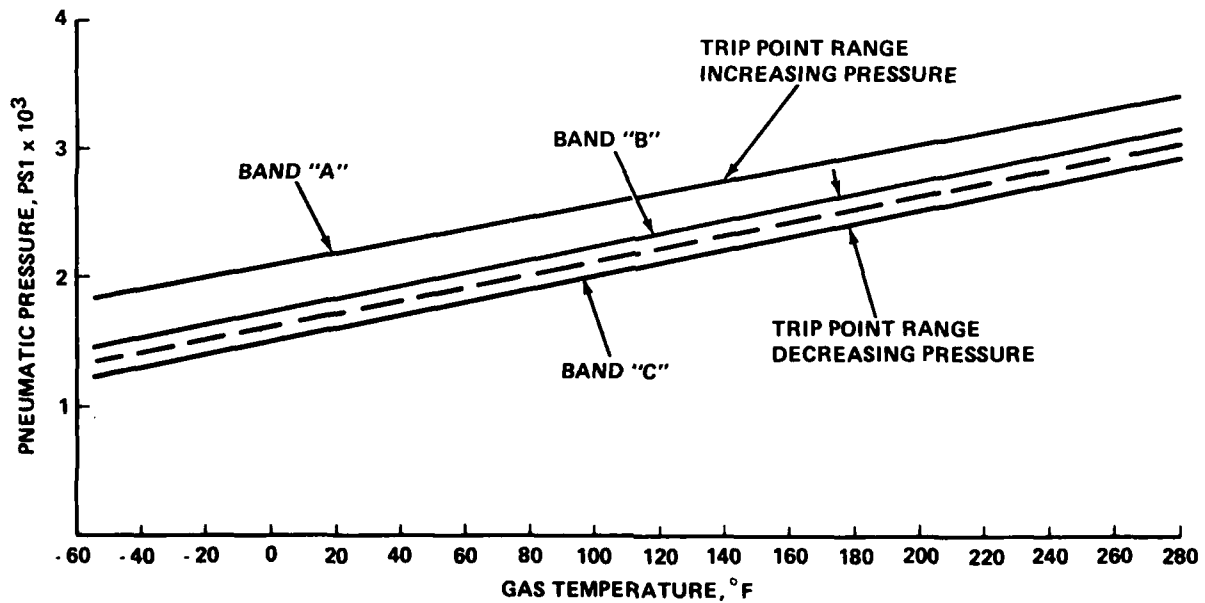
P/N 1500 PT89-2, S/N 001			
● AMBIENT	+69°F	1950 PSIG	
	69°F	2000 PSIG	
● HOT	273°F	3000 PSIG	
	275°F	3000 PSIG	
● COLD	−48°F	1525 PSIG	
	−55°F	1325 PSIG	
P/N 1500 PT89-2, S/N 002			
● AMBIENT	69°F TO 73.5°F	INCREASING PRESS. TRIP	2025 PSIG
		DECREASING PRESS. TRIP	1975 PSIG
● COLD	−64.5°F TO −68°F	INCREASING PRESS. TRIP	1450 PSIG
		DECREASING PRESS. TRIP	1175 PSIG
● HOT	+274.5°F TO +272°F	INCREASING PRESS. TRIP	3020 PSIG
		DECREASING PRESS. TRIP	2960 PSIG

R80-2038-035(T)

R80-2038-035(T)



A. P/N 1500 PT 89-2, S/N 001



B. P/N 1500 PT 89-2, S/N 002

R80-2038-034(T)

Figure 32. Switch actuation points vs temperature (Grumman Specification 204-2).

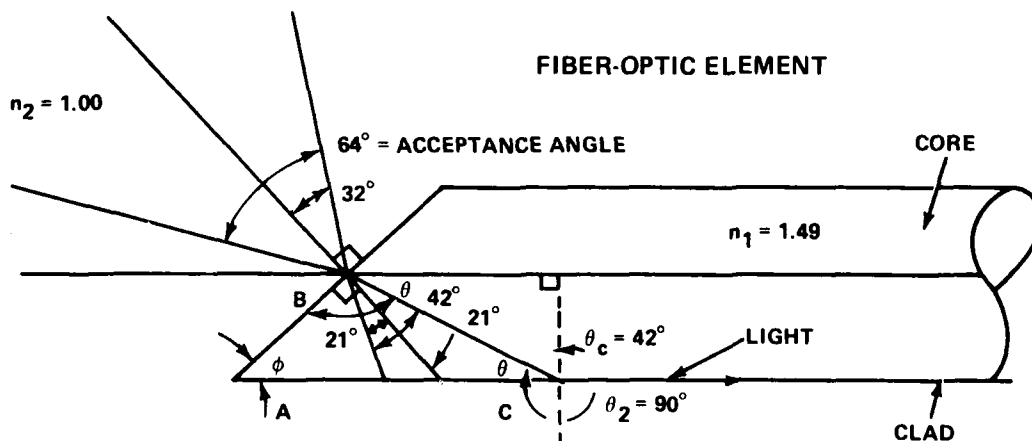
solid or fluid taking into account the angle at which the light beam travels. Willebrord Snell's Law of Sines states that the index of refraction is a constant, equal to the sine of the angle of incidence divided by the sine of the angle of refraction. Table 4 lists the refractive indices of various materials.

TABLE 4. REFRACTIVE INDICES OF VARIOUS ELEMENTS.

• WATER: 1.330	• MIL-H-83282 - 1.456
• AIR: 1.003	• MIL-H-6083 - 1.468
• MIL-H-5606: 1.463	
• CROFON (DUPONT)	• CABLE, FIBER-OPTIC TRANSMISSION
- CORE: 1.490	- CORE: 1.62
- CLAD: 1.392	- CLAD: 1.52
• LUCITE/PLEXIGLASS: 1.51	

R80-2038-036(T)

During the course of development, it became apparent that a single large-diameter fiber would be placed within the pneumatic bottle to detect the presence of a liquid, using the properties of the liquid for light coupling. The fiber angle in which a light ray would be lost when traveling through the conduit, unless the presence of water and/or hydraulic oil were available to permit optical coupling, was then derived mathematically. An analysis of the derivation follows:



$$\frac{\sin \theta_c}{\sin \theta_2} = \frac{n_2}{n_1}$$

$$\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_c$$

$$\sin 90^\circ = \frac{n_1}{n_2} \sin \theta_c$$

$$\frac{\sin 90^\circ}{\sin \theta_c} = \frac{n_1}{n_2}$$

$$\frac{1}{\sin \theta_c} = \frac{1.49}{1.00}$$

$$\sin \theta_c = \frac{1.00}{1.49} \quad (1)$$

$$\theta_c = \sin^{-1} \frac{1.00}{1.49} = 42^\circ$$

$$\theta = 90^\circ - \theta_c$$

$$\angle A = \phi$$

$$\angle B = 90^\circ + 21^\circ$$

$$\theta = 90^\circ - 42^\circ$$

$$\angle C = \theta$$

$$\theta = 48^\circ$$

$$\Delta ABC = \theta + (90^\circ + 21^\circ) + \phi$$

$$180 = \theta + (90^\circ + 21^\circ) + \phi$$

$$180 = 48 + 90 + 21 + \phi$$

$$\phi = 21^\circ$$

Any beveled cut less than 21° will result in having light absorbed by the core.

Definitions

θ_c = critical angle

ϕ = angle required (beveled cut angle)

n = refractive index

θ = angle used in solving ϕ

Assume $n_2 = 1.33$ (index of refraction for water)

$$\sin \theta_c = \frac{1.33}{1.49}$$

(1)

$$\theta_c = \sin^{-1} \frac{1.33}{1.49} = 63^\circ$$

Since θ_c (63°) exceeds the critical angle (42°), light will be transmitted through the light guide.

$$\theta = 90^\circ - \theta_c$$

$$\theta = 90^\circ - 63^\circ$$

$$\theta = 27^\circ$$

$$180^\circ = \theta + (90^\circ + 21^\circ) + \phi$$

$$180^\circ = 27^\circ + 90^\circ + 21^\circ + \phi$$

$\phi = 42^\circ$; beveled angle is increased, resulting in light being transmitted.

$$\sin \theta_c = \frac{1.4635}{1.49}$$

(2)

$$\theta_c = \sin^{-1} \frac{1.46}{1.49} = 79.2^\circ$$

Since θ_c (79.2°) exceeds the critical angle (42°), light will be transmitted through light guide with a MIL-H-5606 coupling.

It has been shown in the laboratory that this approach works in the presence of either fluid. However, instead of using one multistrand fiber-optic cable it became necessary to employ two single-fiber cables with an external light source, with the flexible sensing probe at the bottom of the bottle. Figure 33 shows the concept of an early liquid sensor (Ref. dwg 1491901-307). This approach had screw-on terminals attached to the fiber-optic cables at both the sensing probe and a lucite conductor. The lucite conductor provided an optical means of passing light out of the pneumatic bottle while still retaining the pressure seal. This method proved unacceptable as losses through the fittings and connectors were so drastic that no detectable amount of light could be found at the output fiber. Modifications were made and all unnecessary connectors removed. The result was a design which had one continuous fiber carrying inputted light, a gap allowing fluid detection, and another continuous fiber carrying outputted light. This design (Figure 34) combined the sensor with the fiber-optic cables and greatly reduced transmission losses.

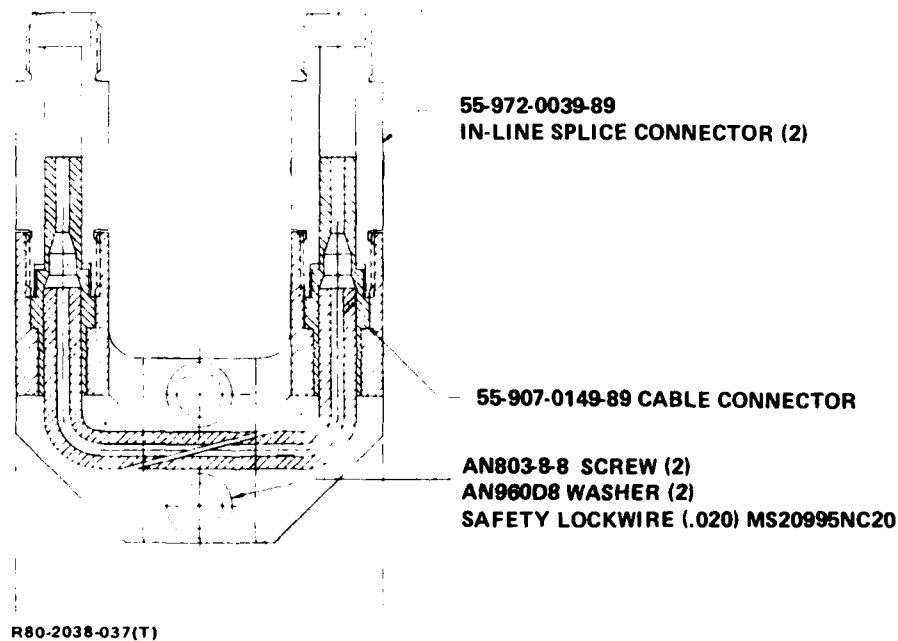


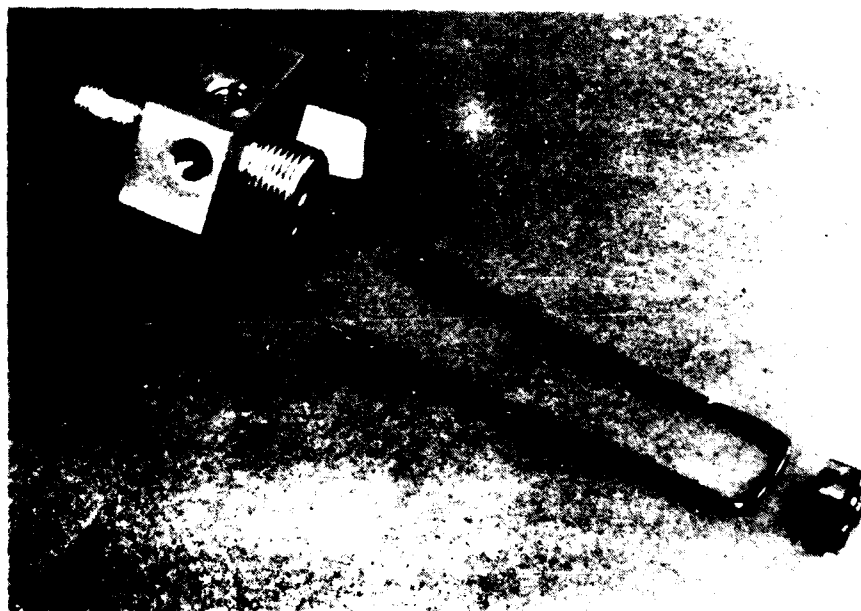
Figure 33. Liquid sensor assembly (early version).

128SCH161-1
AIR BOTTLE (30 IN.)

4.75

AN503-6-6 SCREW (4)
AN960D6L WASHER (4)
MS20995NC20 LOCKWIRE

1491901-308-11
1491901-308-13



R80-7038-038(T)

Figure 34. Liquid sensor assembly (improved version).

Two types of fiber-optic cables were purchased from Valtec Corporation, West Boylston, Massachusetts. The transmission cables were of the bifurcated and the single cable types. The bifurcated cabled type is used on the pneumatic bottle detection loop, whereas the single cable is used on the desiccant color-detection circuit.

Some of the parameters include:

- Number of fibers: 222-234
- Fiber diameter: 0.0031
- Bundle diameter: 0.045
- Acceptance cone angle: 68°
- Cone index of refraction: 1.62.

Additional cable information is provided in Appendix B, Specification No. 206. All cables use fiber-optic connectors in accordance with MIL-L-85044/1, developed by the Naval Ocean Systems Laboratory in San Diego, California. MIL-L-85044/1 covers pressurized bulkhead connectors, Type 1, for relatively low-pressure systems. These stainless steel connectors were manufactured and supplied by the Sealectro Corporation in Mamaroneck, New York.

The cable terminal ends were installed in accordance with the procedure specified on Page 6 of MIL-C-85044 using an epoxy bonding agent to fasten the assembly together.

Properties of Crofon Light Guides. Crofon is a Dupont registered trade name for plastic fiber light guides. The data in Table 5 were taken from a Dupont publication on Crofon Fiber Optics (Ref. 4) and a Machine Design article (Ref. 5). Table 5 shows some properties of the Crofon Fibers and their polyethylene jackets. Figure 35 shows a light ray entering the light guide.

Transmission of light through Crofon varies as a function of length. It is also dependent on input light intensity, output light interfaces, and any gap through the optic circuit. Figure 36 shows the transmission efficiency of white light through fully polished light guides.

Single bends are employed in the liquid detection circuit at the sensor end. It is desirable to ascertain the minimum bend radius for the single 1056 light guide. Too severe a bend will cause a significant light loss due to degradation of the cladding fiber itself. Figure 37 shows typical light transmission for several grads of Crofon light

TABLE 5. PROPERTIES OF CROFON FIBERS WITH POLYETHYLENE JACKETS.

A. IDENTIFICATION: CROFON 1056

• NUMBER OF FIBERS:	1	• CRITICAL ANGLE: 69°
• OD:	0.111 ± .005 IN.	• INDEX OF REFRACTION:
• FIBER DIAMETER:	0.056 IN.	– CORE $N_D = 1.490$
• JACKET MATERIAL:	POLYETHYLENE	– CLAD $N_D = 1.392$
• FIBER:	POLYMETHYL METHACRYLATE	• OPERATING TEMPERATURE LIMITS:
• ACCEPTANCE ANGLE:	64°	–40 °F TO 175 °F

B. TYPICAL PROPERTIES OF POLYETHYLENE

ASTM TEST	PROPERTY	LOW DENSITY	MEDIUM DENSITY	HIGH DENSITY	ULTRAHIGH MOLECULAR WEIGHT
PHYSICAL					
D792	SPECIFIC GRAVITY	0.910-0.925	0.926-0.940	0.941-0.965	0.928-0.941
–	SPECIFIC VOLUME (IN. ³ /LB)	30.4-29.9	29.9-29.4	29.4-28.7	29.4
D570	WATER ABSORPTION, 24 HR, 1/8-IN. THK (%)	<0.01	<0.01	<0.01	<0.01
MECHANICAL					
D638	TENSILE STRENGTH (PSI)	600-2,300	1,200-3,500	3,100-5,500	4,000-6,000
D638	ELONGATION (%)	90-800	50-600	20-1,000	200-500
D638	TENSILE MODULUS (10 ⁵ PSI)	0.14-0.38	0.25-0.55	0.6 - 1.8	0.20-1.10
D785	HARDNESS, ROCKWELL R	10	15	65	55
D790	FLEXURAL MODULUS (10 ⁵ PSI)	0.08-0.60	0.60-1.15	1.0-2.0	1.0-1.7
D256	IMPACT STRENGTH, IZOD (FT-LB/IN. OF NOTCH)	NO BREAK	0.5-16	0.5-20	NO BREAK
THERMAL					
C177	THERMAL CONDUCTIVITY (10 ⁻⁴ CAL/CM/SEC-CM ² .°C)	8.0	8.0-10.0	11.0-12.4	11.0
D696	COEF OF THERMAL EXPANSION (10 ⁻⁵ IN./IN. - °C)	10-22	14-16	11-13	14
D648	DEFLECTION TEMPERATURE (°F)				
–	AT 264 PSI	90-105	105-120	110-130	118
–	AT 66 PSI	100-121	120-165	140-190	170
–	CONTINUOUS, NO-LOAD SERVICE TEMP (°F)	180-212	220-250	250	–
ELECTRICAL					
D149	DIELECTRIC STRENGTH (V/MIL) SHORT TIME, 1/8-IN. THK	460-700	460-650	450-500	900*
D150	DIELECTRIC CONSTANT				
–	AT 60 Hz	2.25-2.35	2.25-2.35	2.25-2.35	–
–	AT 10 ³ Hz	2.25-2.35	2.25-2.35	2.30-2.35	2.30-2.35
D150	DISSIPATION FACTOR				
–	AT 10 ³ Hz	0.0002	0.0002	0.0003	0.0002
D257	VOLUME RESISTIVITY (OHM-CM)				
–	AT 73°F, 50% RH	10 ¹⁵	10 ¹⁵	10 ¹⁵	10 ¹⁵
D495	ARC RESISTANCE (SEC)	135-160	200-235	–	–
OPTICAL					
D542	REFRACTIVE INDEX	1.51	1.52	1.54	–
D1003	TRANSMITTANCE (%)	4-50	4-50	10-50	–
*kV/CM					
1087-052W					

guides. It becomes evident that bend radius should be as large as possible to minimize transmission loss.

Fiber-Optic Connectors. Numerous types of fiber-optic connectors were considered for use in HYCOS. The major concern was the availability of a high-pressure bulkhead fitting capable of sealing 3000 psi pneumatic pressure. As of February 1978, no bulk-head connectors on the market were capable of withstanding this high pneumatic pressure differential without leakage.

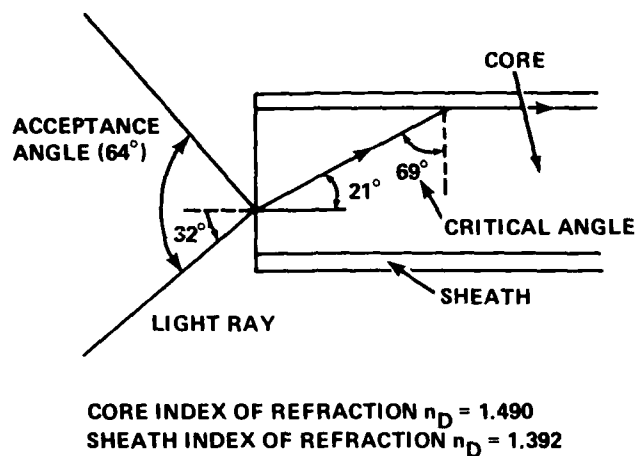
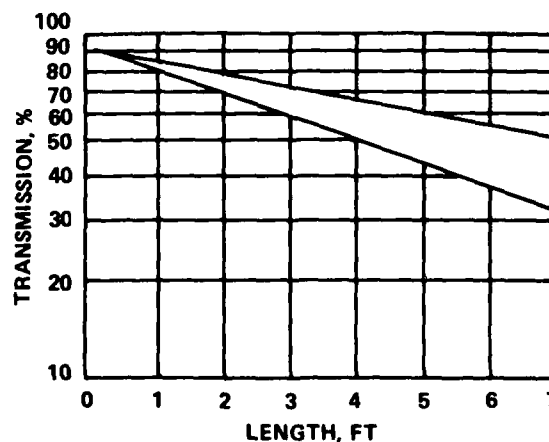


Figure 35. Crofon light guide properties.



NOTE: TRANSMISSION VALUES ARE FOR LIGHT GUIDES WITH CAREFULLY POLISHED ENDS.

R80-2038-041(T)

Figure 36. Transmissivity of Crofon light guides.

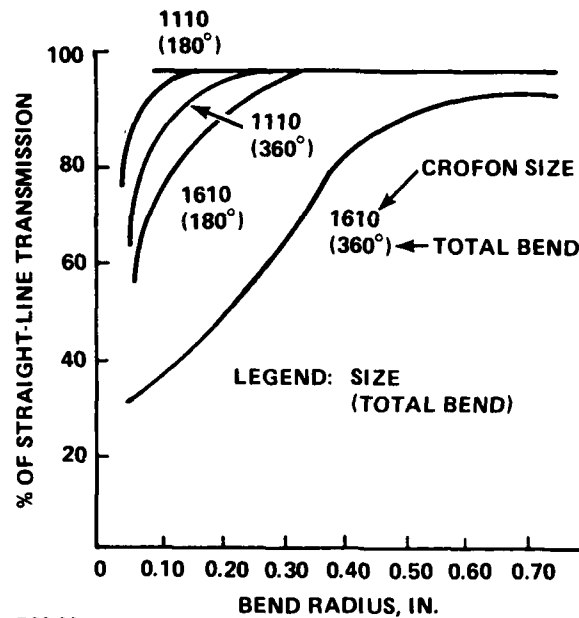


Figure 37. Effect of bend radius on light transmissivity.

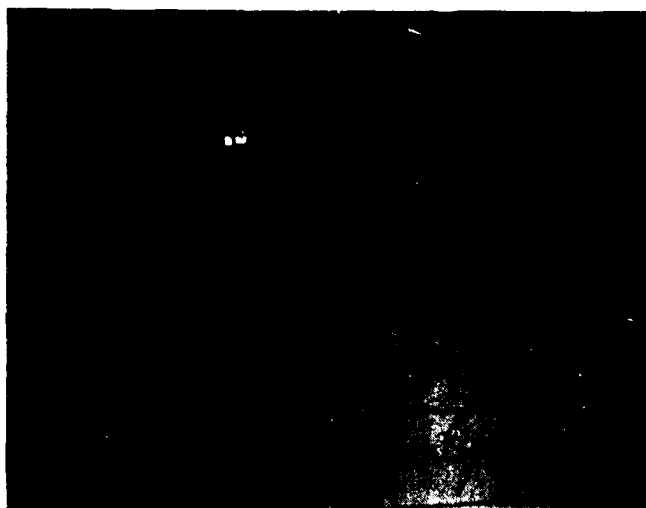
Grumman was informed that the proposed MIL-C-85044/1 Connector, Fiber-Optic, Pressurized Bulkhead, Type I, Class I was being manufactured by Sealectro Corporation, Mamaroneck, New York. Sealectro indicated that the connectors were in stock.

Sealectro part numbers and unit weights are:

● Cable Connector:	55-907-0149-89	0.1056 Oz
● In-Line Splice:	55-972-0039-89	0.1746 Oz
● Bulkhead Mounting Connector:	55-975-0049-89	0.3527 Oz

All parts are made of corrosion-resistant stainless steel. Figure 38 shows a typical fiber-optic terminal used in HYCOS. The connector has a fiber terminal diameter of 0.0465 in. (area = 0.001698 in.²). For HYCOS, special connector interfaces were designed to withstand the intended environment. Figure 39 shows a Display Panel fiber-optic terminal.

Pressure Seal. In order to transport light through a pressure seal, it became necessary to design a seal that would satisfy system integrity and provide maximum light transmissivity. Concept Number One, shown in figure 40A, employed a transfer tube containing machined and polished clean acrylic rod for light transmission. Although



R80-2038-043(T)

Figure 38. Assembled fiber-optic connector.

initial pressure testing at 3000 psi revealed good results, the optical transmission properties were very poor. Almost all of the light generated at the outside source was lost due to the optical properties of the acrylic rod. A revised approach, shown in Figure 40B, eliminated the acrylic rod and utilized the fiber-optic cable up to the external connector interface. Initial testing revealed that the plastic tended to creep and extrude under prolonged exposure to pressure. Additional development effort overcame this problem and considerably improved the overall transmission efficiency. Limited operational cycling and proof testing verified this approach. No problems were encountered during the flight test program.

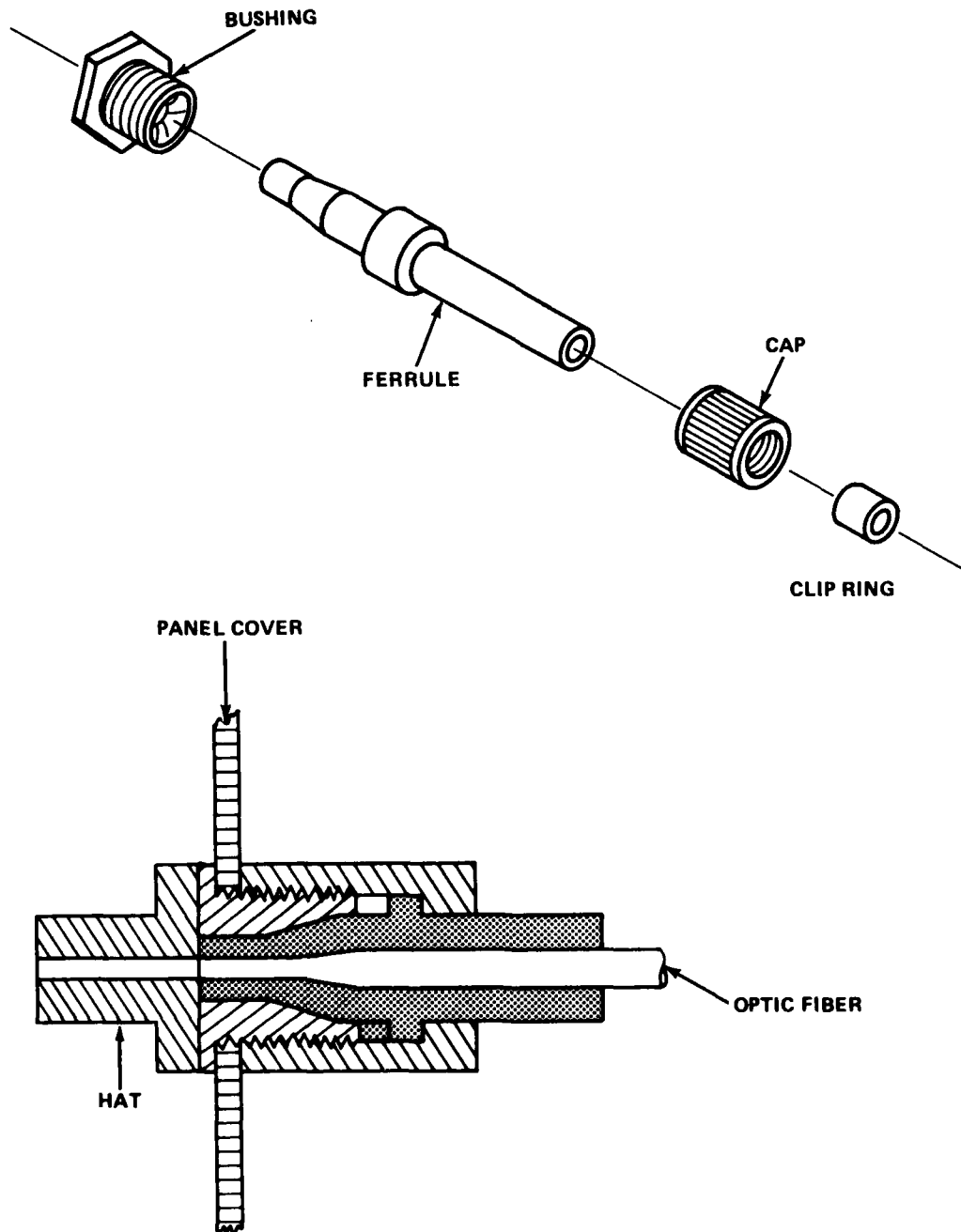
1.3.3 Hydraulic Pump/System

1.3.3.1 Flow Sensor Description

The flow sensor is a device placed in series with a hydraulic system or component which gives an external indication when a specific flow value has been exceeded under controlled conditions.

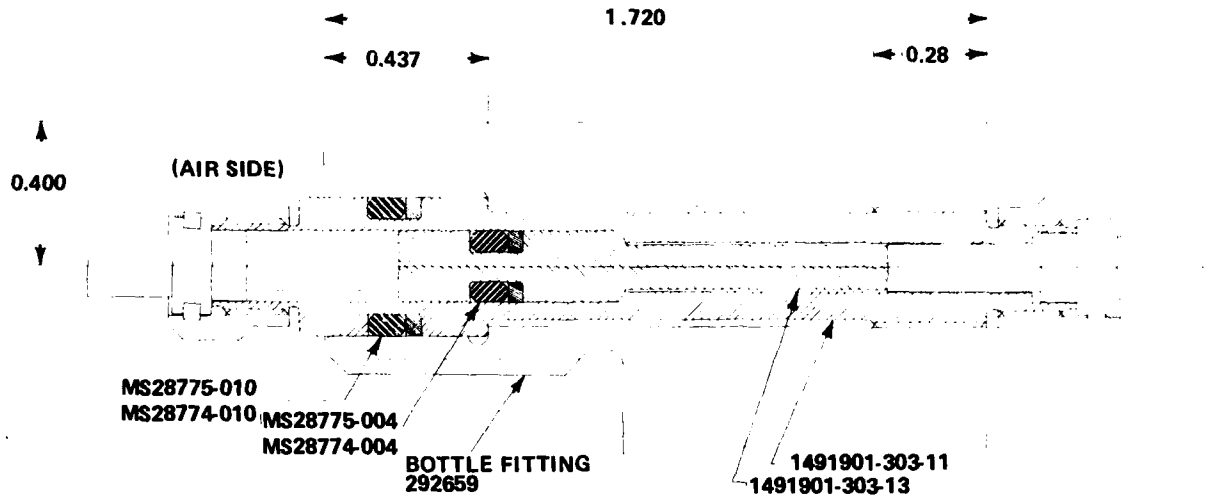
1.3.3.2 System Quiescent Flow Sensor

System quiescent flow values for the A-6E system were established at 0.5 to 1.5 gpm. This will vary depending on which system components are on the line during a no-input system demand condition. For the A-6E combined system, quiescent flow limits of 4.5 ± 1 gpm were established as excessive internal flow.

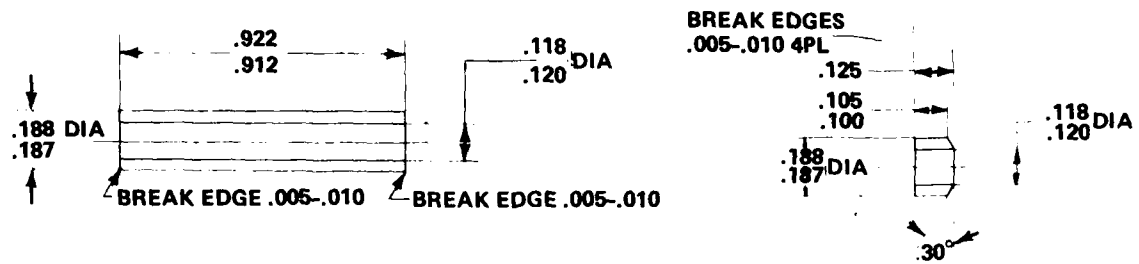


R80-2038-044(T)

Figure 39. Display panel fiber-optic terminal.

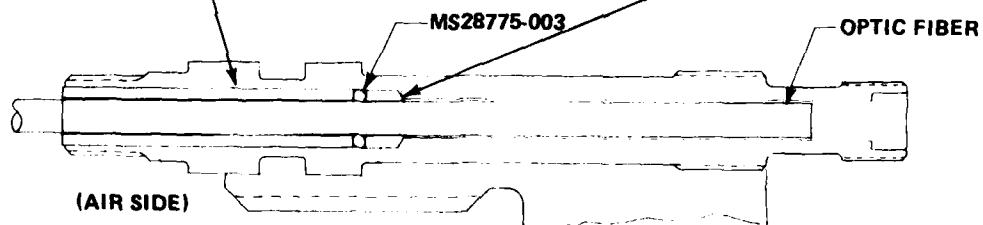


A. PNEUMATIC HIGH-PRESSURE SEAL CONFIGURATION



MATERIAL: CRES 303 1/4 HD (.250 DIA)

MATERIAL: TEFLON ROD (.250 DIA) BLACK

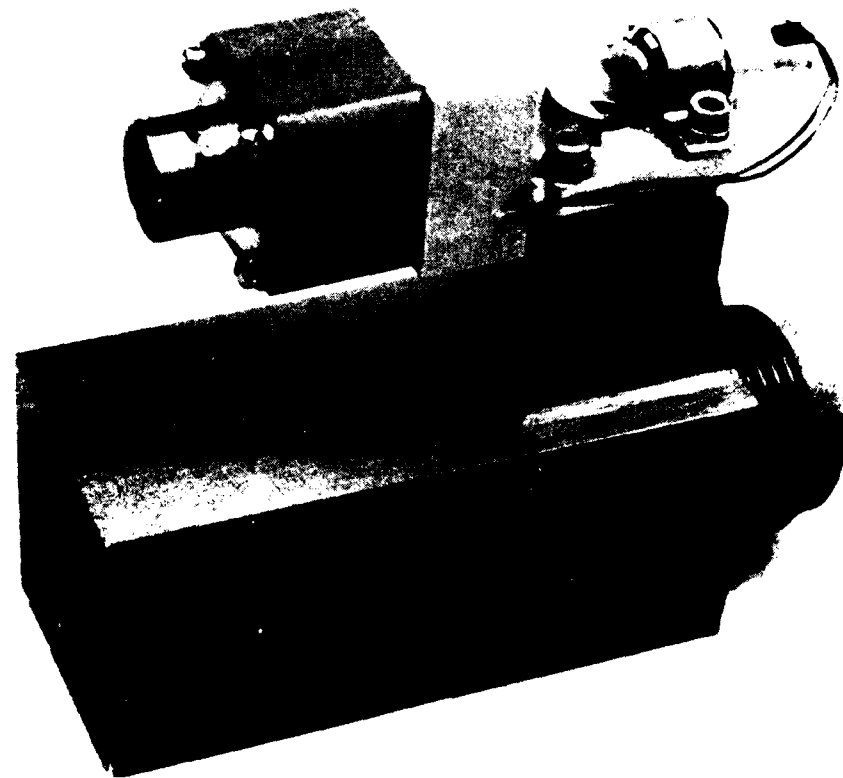


B. IMPROVED HIGH-PRESSURE SEAL

R80-2038-045(T)

Figure 40. Pressure seal.

The system flow sensor incorporates an electrically actuated locking device which prevents indicator actuation during normal system flow demands. Under quiescent flow conditions, the flow is measured through a movable orifice. Flows beyond the required measured values are shunted across the movable orifice. Figure 41 shows a typical quiescent flowmeter used in the flight test program. Once the indicator trips due to excessive flow conditions, it must be manually reset.



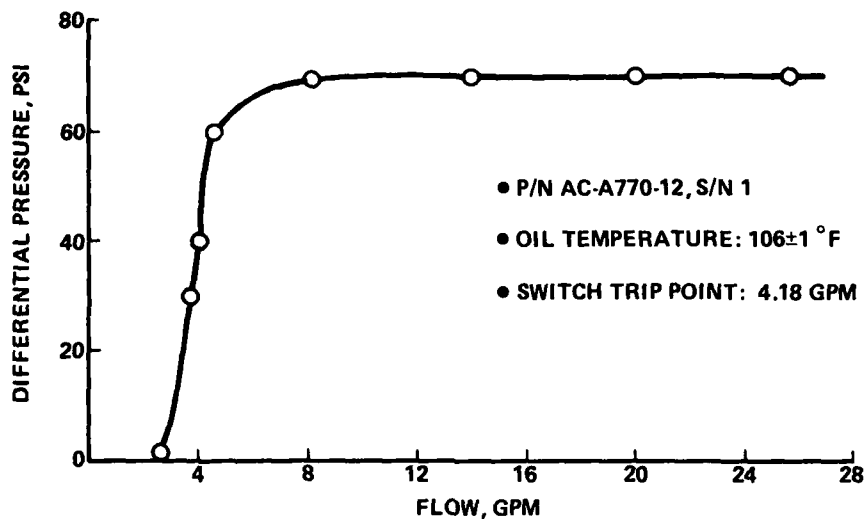
R80-2038-046(T)

Figure 41. Quiescent flow sensor.

The flow sensor meters actual quiescent flow through a flow resistor that produces a desired differential pressure. The differential pressure, equated to a specific maximum permissible quiescent flow leakage, generates a signal. During normally higher system flow demand, the calibrated restrictor bypasses through additional flow passages at acceptable additional pressure differentials across the entire sensor.

Plant 14 Hydraulic Laboratory generated calibration data that produced the curve shown in Figure 42. The curve shows a trip point of 4.18 gpm which is within the design limits. It should be noted that the curve flattens out above 8 gpm.

The actual installation on the flight test vehicle is shown in Figure 43.



R80-2038-047(T)

Figure 42. Calibration: flow sensor, bypass type, quiescent flow.

1.3.3.3 Pump Case Drain Flow Sensor

The pump case drain flow sensor is similar to the system quiescent flow sensor in design but does not incorporate a lockout device since pump case flow does not significantly vary over the hydraulic pump flow range. A failsafe bypass device is incorporated, however, to preclude high back pressure due to inadvertent momentary block liftoff. Excessive pump case flow was established at 1.25 to 1.75 gpm. Figure 44 shows a typical pump case flow sensor. A case drain flow calibration curve is presented in Fig. 45. Actual switch trip occurred at 1.47 gpm, Figure 46 shows a partially obscured installation in the A-6E test vehicle.

1.3.3.4 Rudder Actuator Quiescent Flow Sensor

Excessive rudder actuator internal leakage is detected by an in-line flow sensor located in the pressure line. The unit is similar in construction to the system quiescent flow sensor, but is sized for a lower flow. Since normal rudder actuator quiescent leakage rates are very low, a value of 0.625 to 0.875 gpm was selected for the A-6E rudder actuator. Figure 47 shows the rudder actuator quiescent flow sensor.

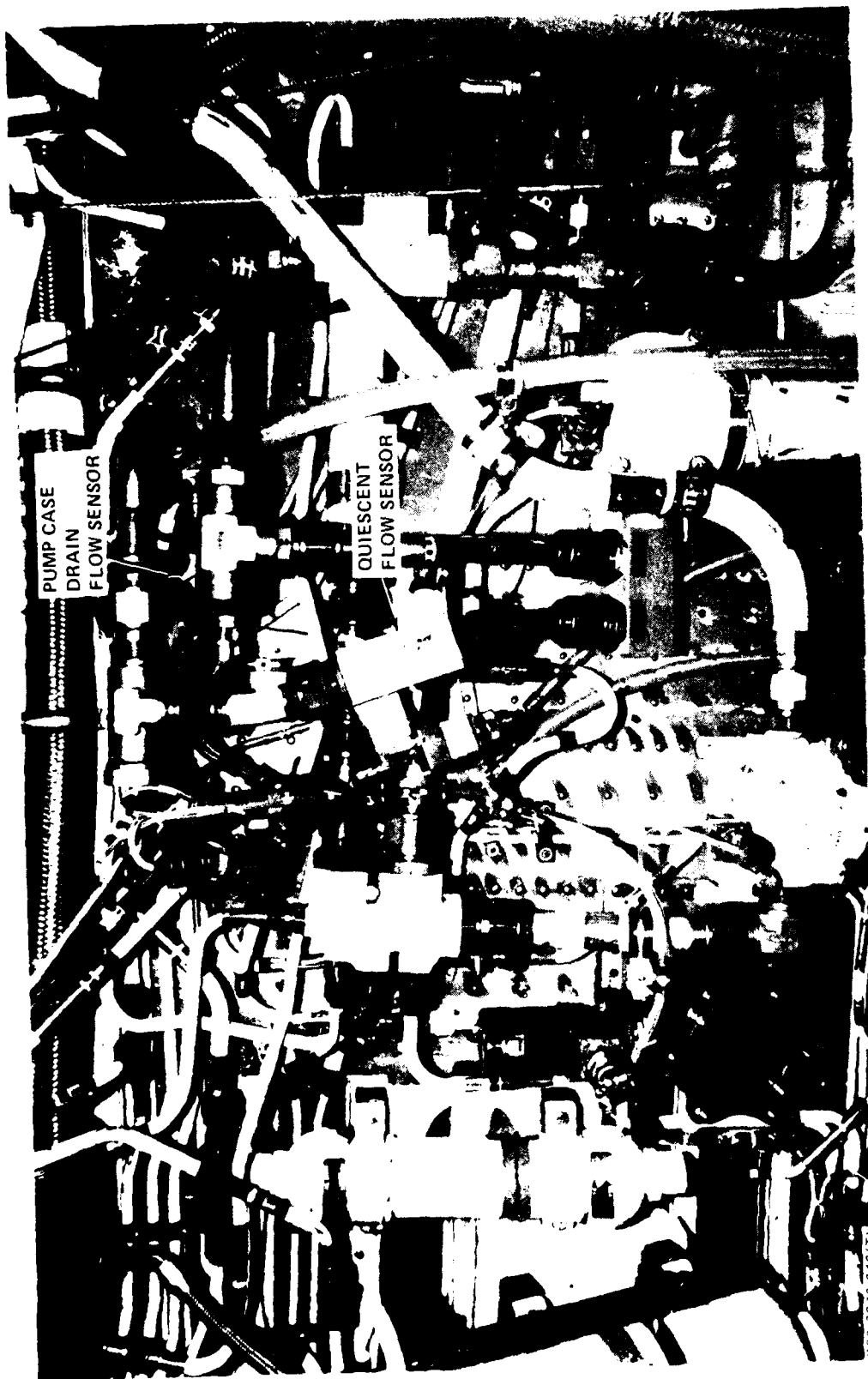
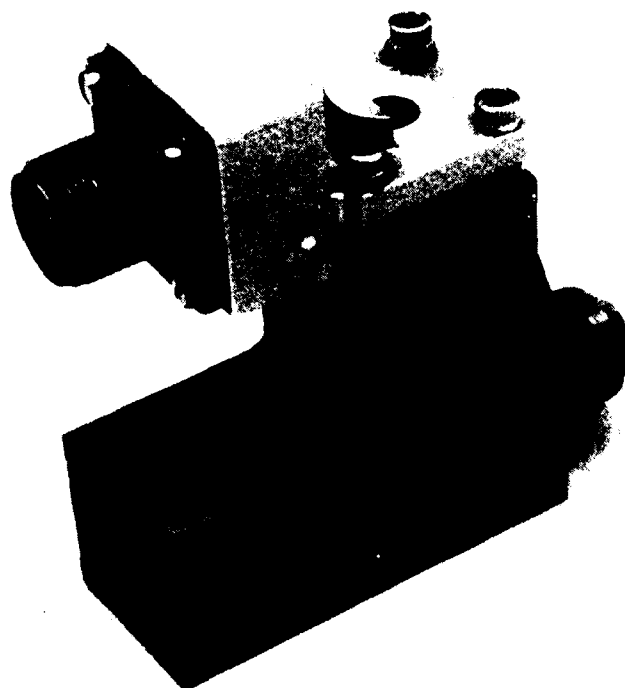


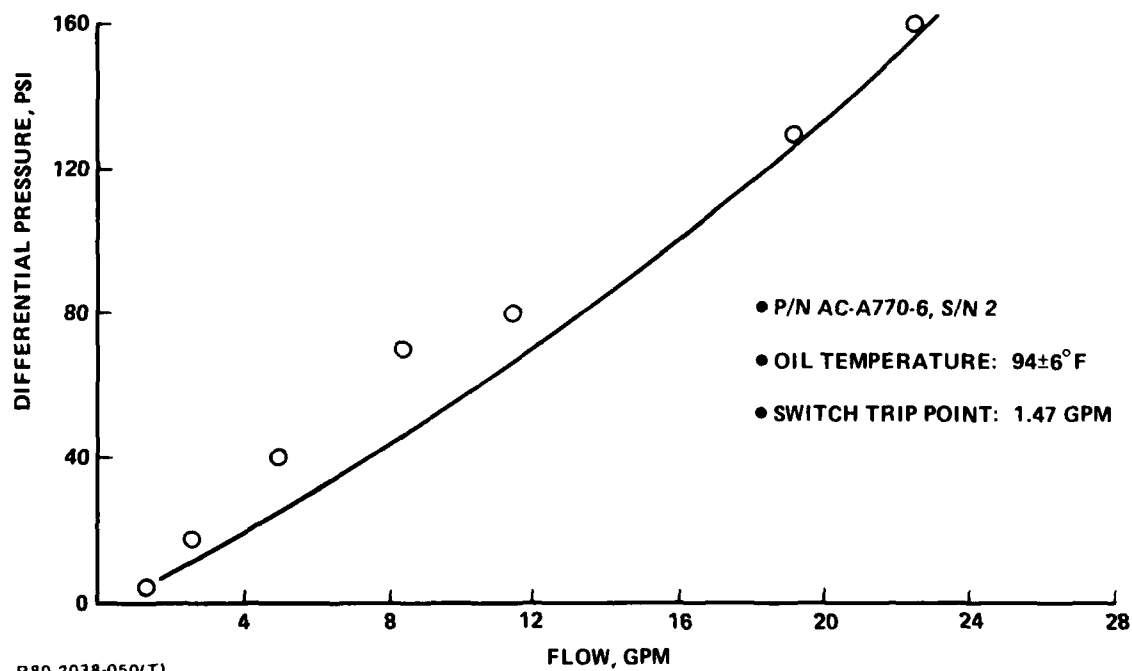
Figure 43. System quiescent flow sensor installation.

430-2036-048(1)



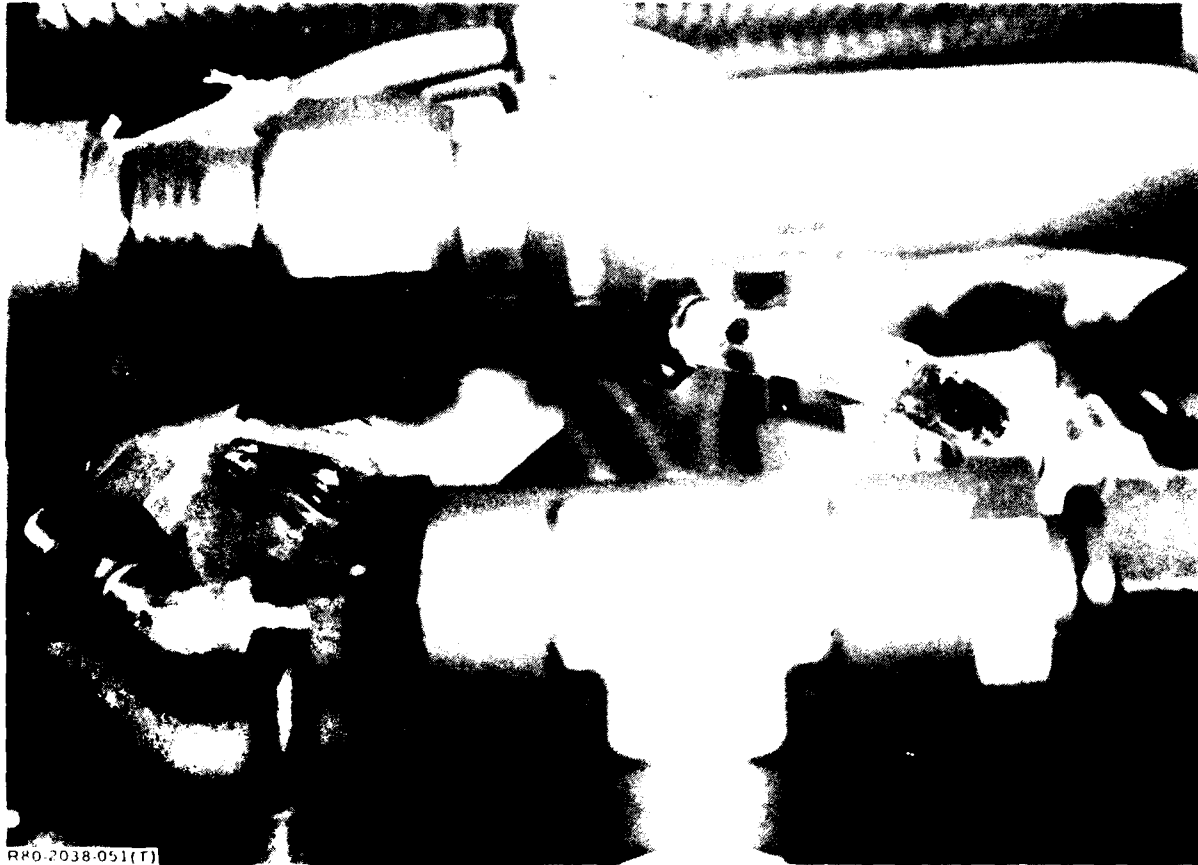
R80-2038-049(T)

Figure 44. Pump case drain flow sensor.



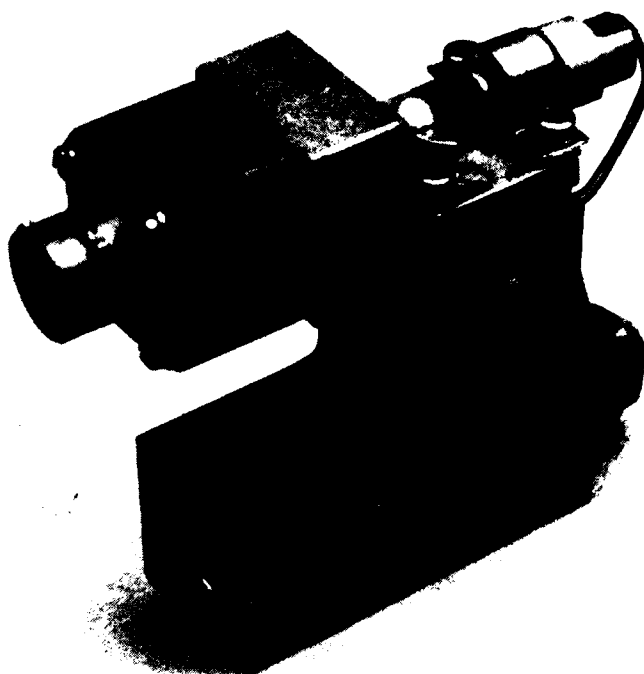
R80-2038-050(T)

Figure 45. Calibration: pump case drain flow sensor, bypass type.



RFO-2038-051(T)

Figure 46. Pump case drain flow sensor installation.



R80-2038-052(T)

Figure 47. Rudder actuator flow sensor.

Flow versus pressure drop data produced the curve shown in Figure 48. The installation is shown in Figure 49. Note that the sensor was installed in the pressure line.

1.3.3.5 System Pressure Switch

The system pressure switch serves two functions: it indicates low system pressure during system operation and provides panel circuitry to the flow sensors and elements.

The elapsed time meter on the panel is actuated by the pressure switch; the flow sensor circuits are dependent on the pressure circuit being on.

For this purpose, a switch (Figure 50) manufactured by Sigmanetics of Mountain Lakes, New Jersey, was incorporated. The switch weighs less than 0.085 lb and actuates on decreasing pressure of 2300 ± 100 psi. The switch installation is shown in Figure 51.

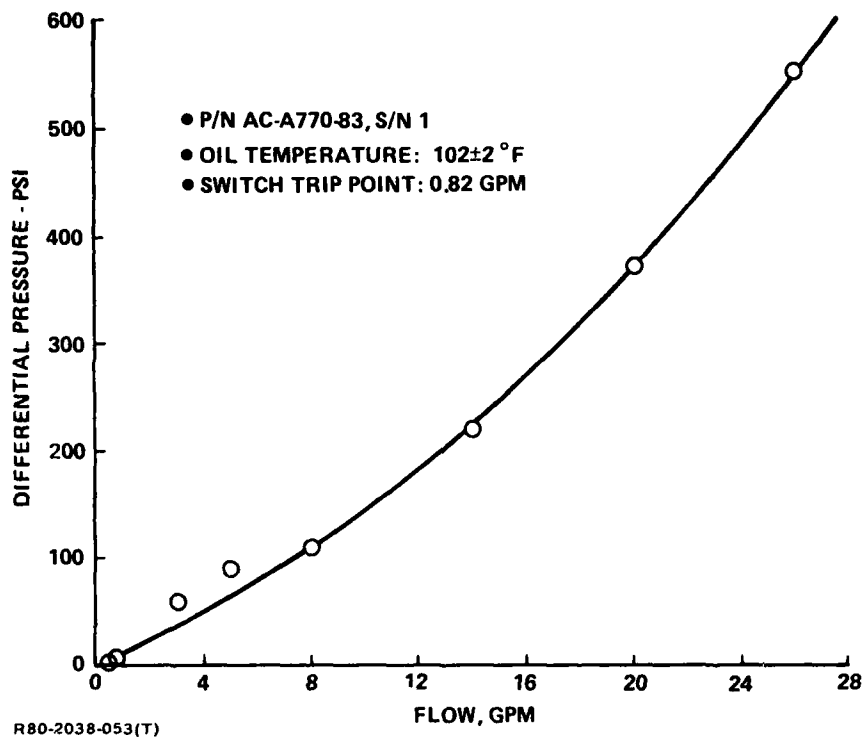


Figure 48. Calibration: rudder actuator quiescent flow sensor, bypass type.

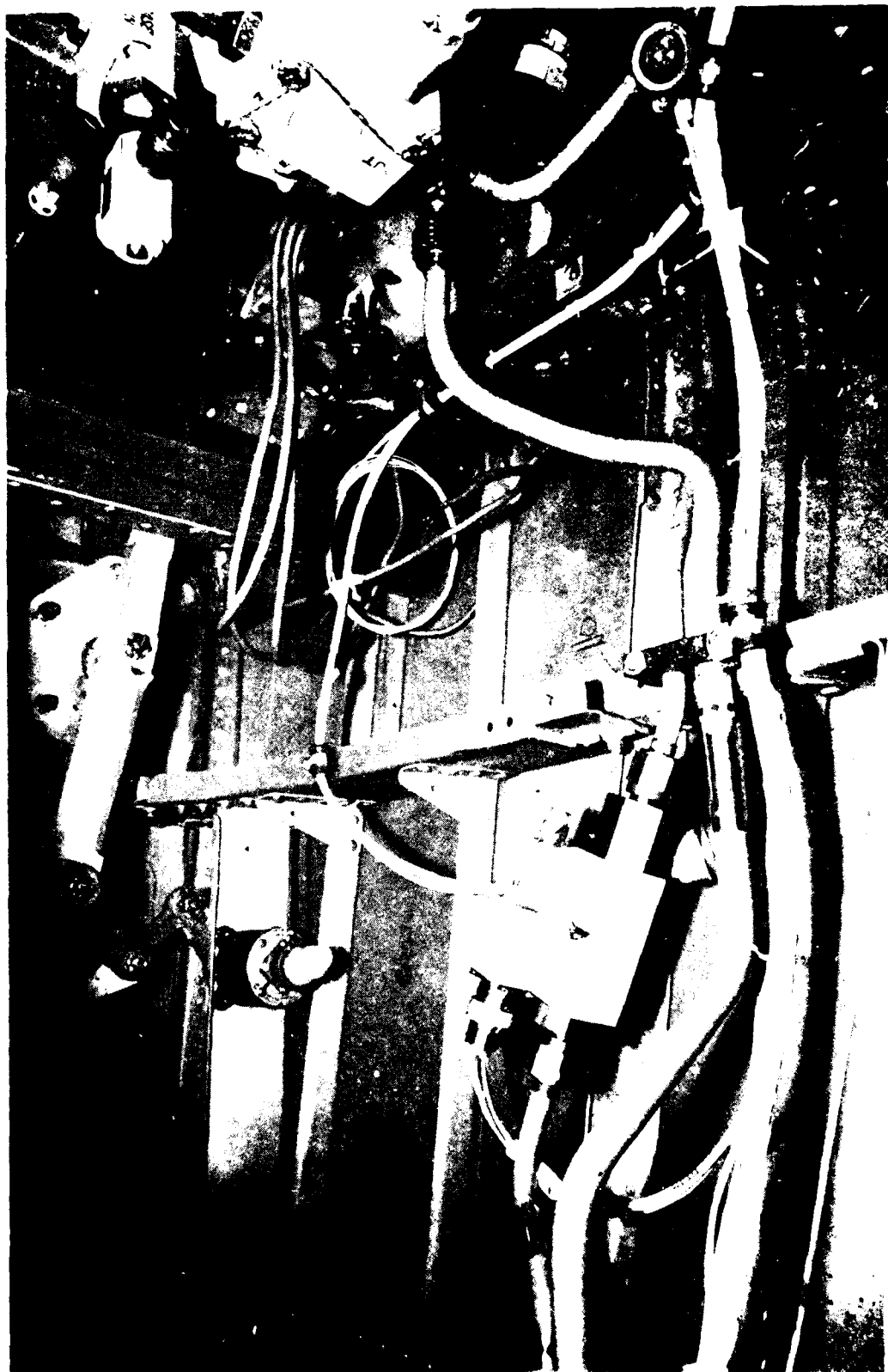
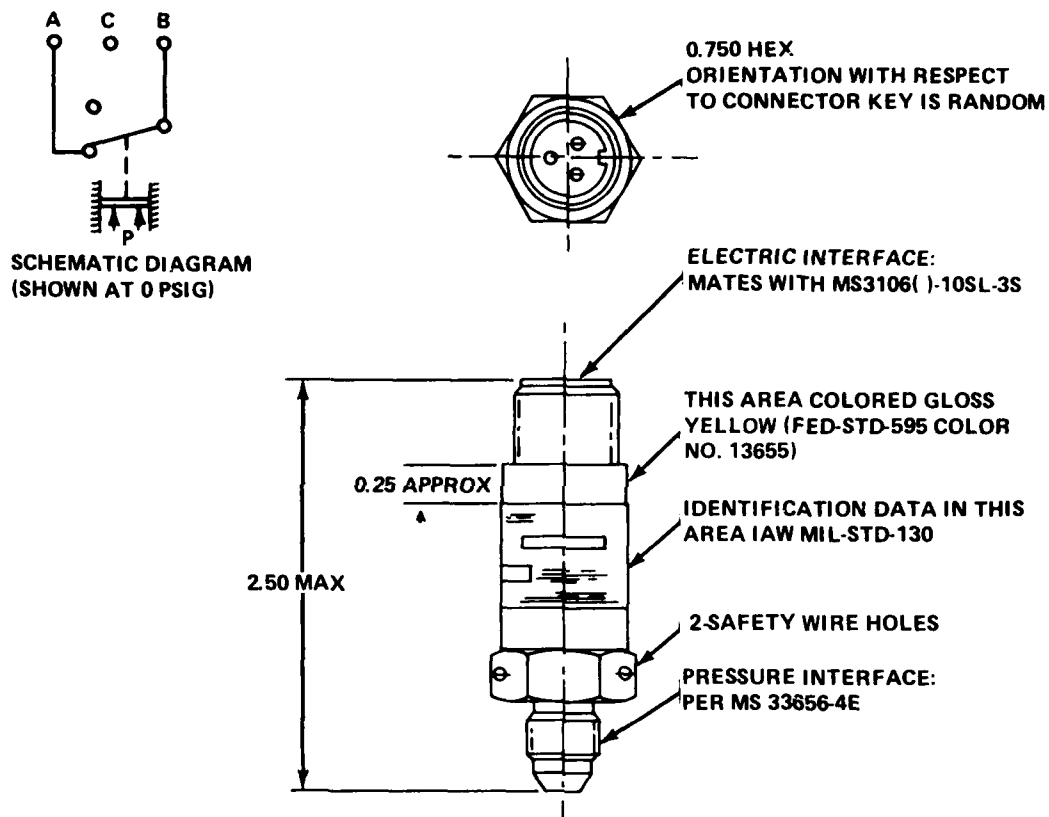


Figure 19. Rudder actuator quiescent flow sensor installation.

886-2038-054(T)



R80-2038-055(T)

Figure 50. System pressure switch.

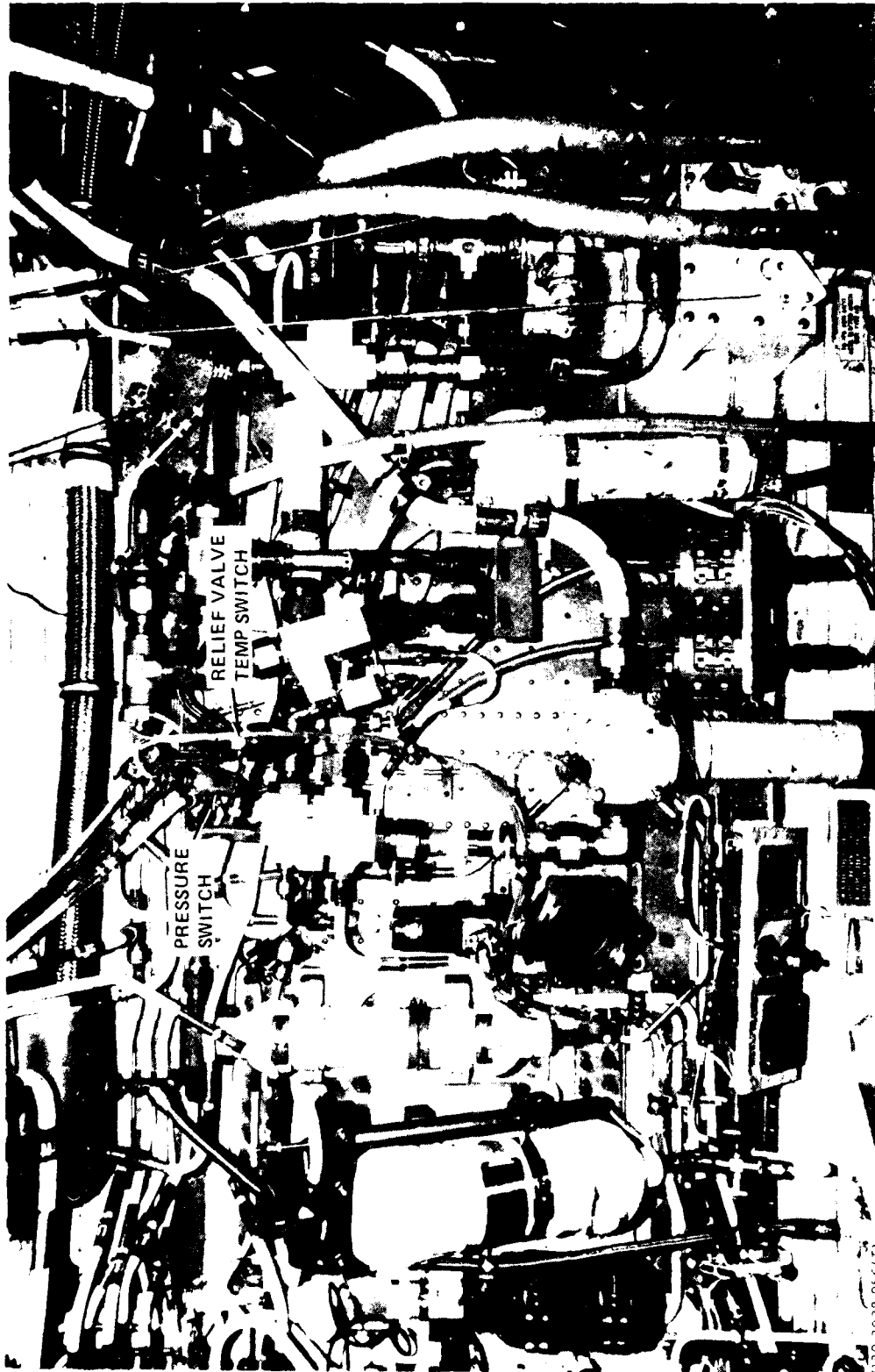


Figure 51. Relief valve temperature and system pressure switch installation.

1.3.3.6 Case Drain Flow Temperature Switch

Excessive case drain flow indicates hydraulic pump degradation, resulting in system fluid temperature rise. By installing a fluid temperature switch in series with the flow sensor, an excessive temperature limit can be detected.

Type II hydraulic systems operate at a 275°F maximum. A value of $300 \pm 20^\circ\text{F}$ was selected as the trip limit on a Texas Instrument Klixon manual reset temperature switch.

The switch was mounted to the case drain line near the pump by using a clamp-on adaptor. This switch must be manually reset after being tripped.

1.3.3.7 Relief Valve Leakage

Relief valve leakage was measured with a probe-type manual reset temperature switch as used to measure pump case drain flow. Trip setting for this switch was $300 \pm 20^\circ\text{F}$.

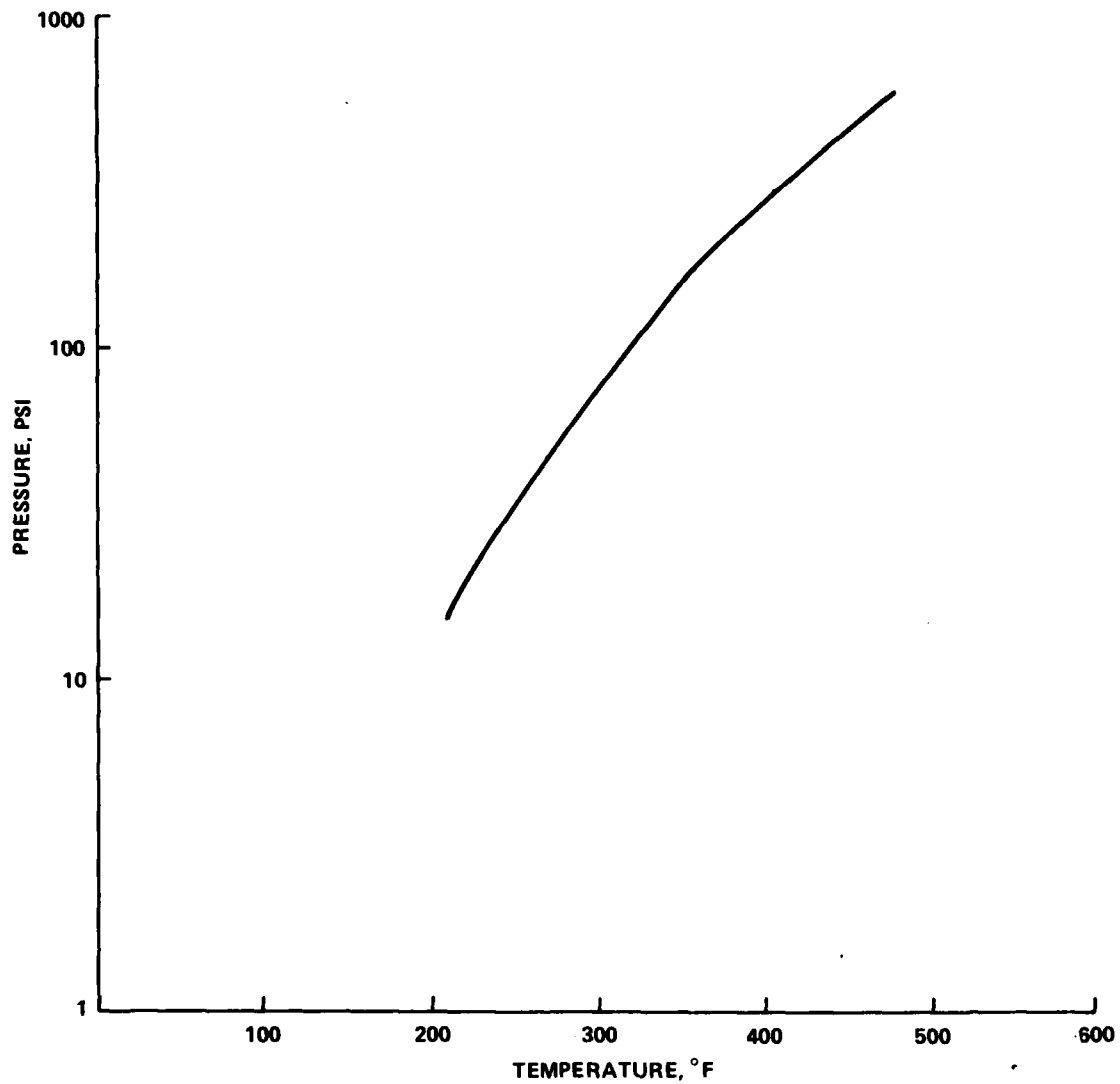
Type II hydraulic systems operate at 275°F maximum. A value of 300°F was selected as the trip limit on a Neo-Dyne model 1103TR119 manual reset temperature switch.

The switch probe is immersed in the fluid flow and contains n-propyl alcohol as the sensing medium. Temperature sensing is accomplished by exposing a welded corrosion-resistant steel diaphragm to changes in pressure created by expanding fluid in the probe. Figure 52 shows pressure versus temperature slot for this fluid at constant volume. Temperature settings are determined by a force-balance interaction between the sensing diaphragm and a snap-action Belleville spring system. An electrical switch assembly positioned within the mechanism's stroke limit provides electrical circuit control at predetermined temperatures. The manual reset button functions as both a visual indication and a mechanism reset after switch actuation. The temperature switch is illustrated in Figure 53. Installation is shown in Figure 51.

1.3.4 Hydraulic Accumulators

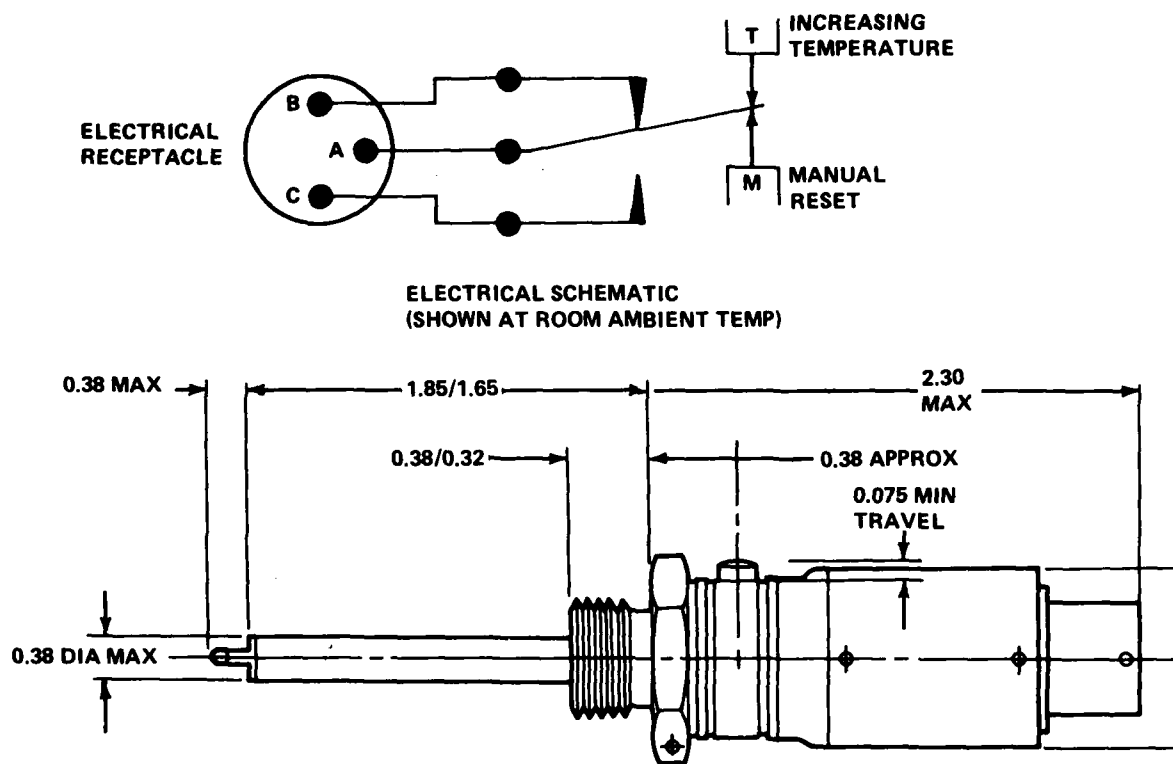
1.3.4.1 Description

Hydraulic accumulators are energy storage devices used in many aircraft hydraulic systems. They usually employ stored gas as the variable energy source. Their applications include hydraulic pump ripple attenuation, momentary system power overdemand conditions, and performance of emergency actuation functions such as deploying a ram air turbine via a hydromechanical actuator.



R80-2038-057(T)

Figure 52. Pressure versus temperature of n-propyl alcohol at constant volume.



R80-2038-058(T)

Figure 53. Manual reset temperature switch.

The work output is dependent on initial precharge pressure, precharge temperature, and delta volume change caused by piston movement under constant temperature conditions:

$$P_1 V_1 = P_2 V_2$$

and

$$W = \int_{V_1}^{V_2} P \, dv$$

If we consider an isentropic (no heat flow condition), then

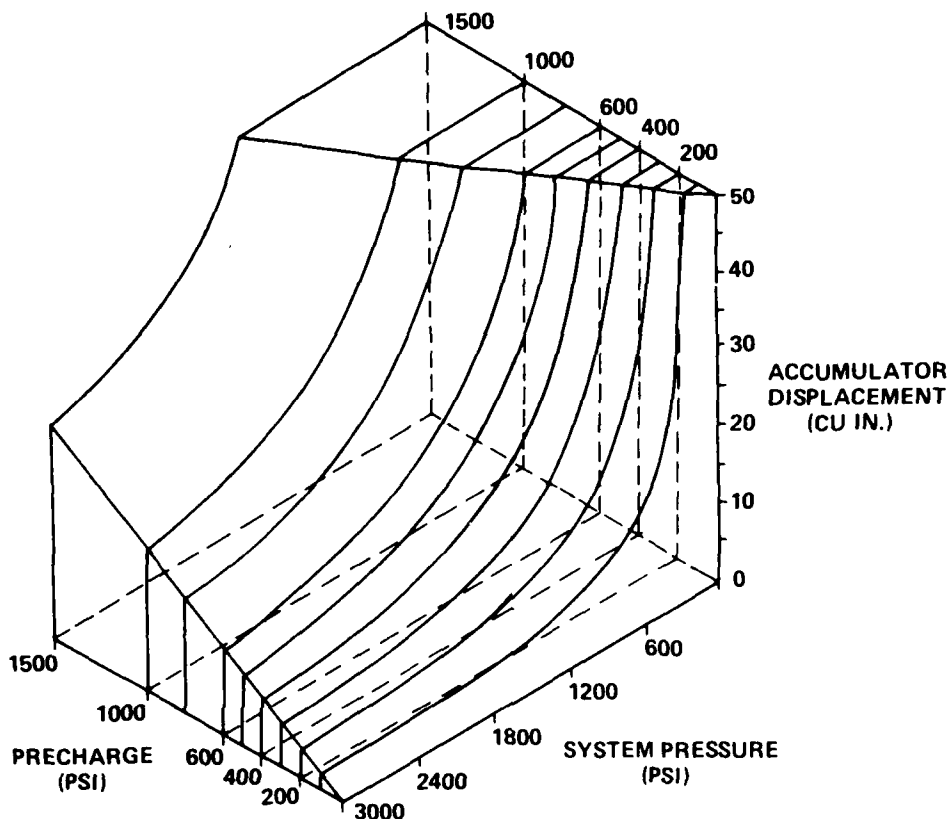
$$W = K \int_{V_1}^{V_2} \left[\frac{dv}{v^{1.4}} \right]$$

Since the variables are precharge pressure, precharge temperature, and piston displacement, the piston displacement for a final hydraulic system pressure of 3000 psi is a function of initial precharge conditions (Ref. 6, NADC TR 75168-30-Pg 33).

This monitoring effort was initiated to develop a method of determining accumulator precharge irrespective of whether the accumulator is fully or partially discharged. The variables required to determine this condition are charging pressure, temperature, and piston displacement.

Figure 54 shows the variation of piston displacement versus precharge pressure for a 50 in³. accumulator. Figure 55 shows a plot of piston displacement versus precharge pressure versus temperature at constant 3000 psi pressure. Figure 56 is a nomograph developed to determine precharge pressure.

In order to measure accumulator piston displacement, precharge pressure (accumulator pressure), and precharge temperature, various methods were investigated to ascertain their suitability to accumulator applications. These specific sensing methods will be defined in subsequent paragraphs.



R80-2038-060(T)

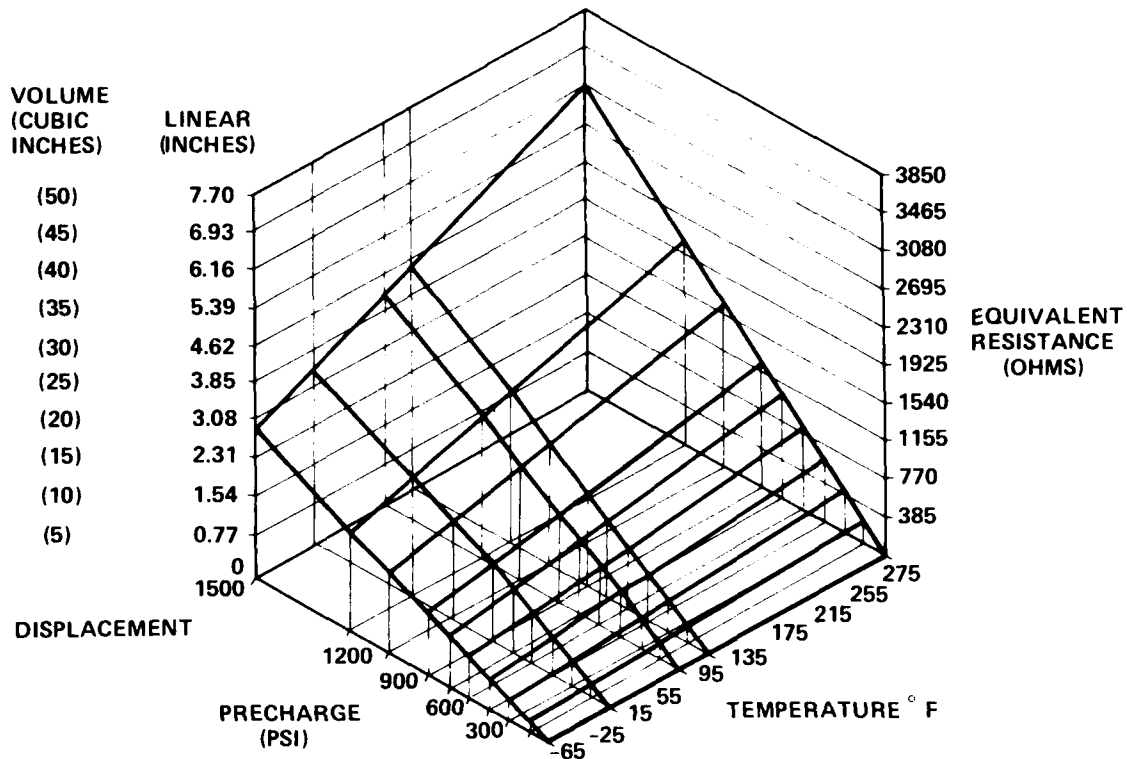
Figure 54. Accumulator piston displacement versus precharge and system pressures at constant (70°F) temperature.

1.3.4.2 Piston Displacement Sensors

Several methods of determining piston displacement within a pressurized accumulator were investigated. They include:

- A direct type in which a rod attached to the piston passes through a dynamic seal
- A reflected energy type which measures reflected IR energy from a movable surface.

The first direct type seemed to offer less development risk than the other method since the output could be processed easier with the microprocessor circuits. This direct type included a linear potentiometer with its axis parallel to the accumulator piston axis. By affixing the movable piston rod to the linear potentiometer, a direct

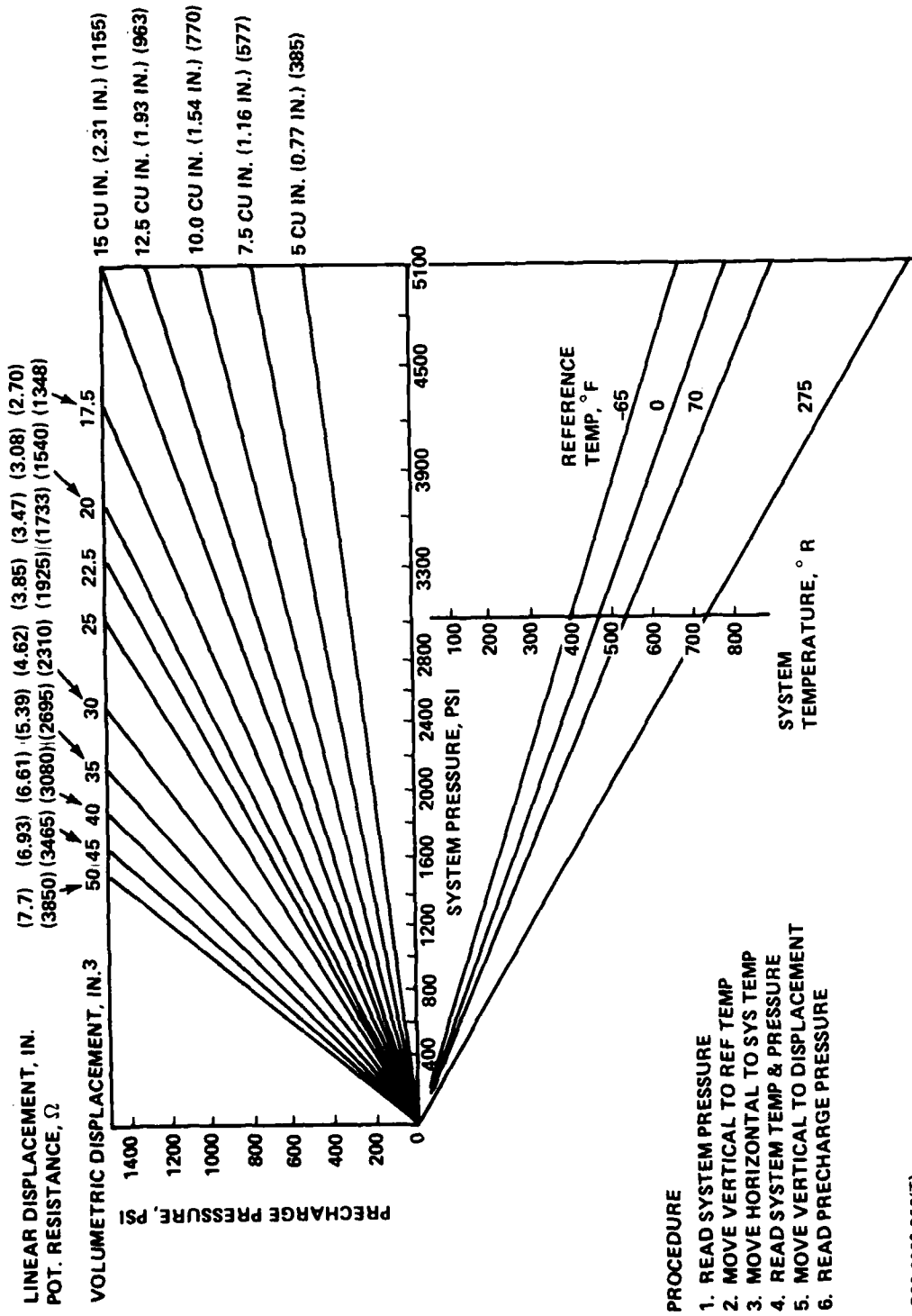


R80-2038-061(T)

Figure 55. Accumulator piston displacement versus precharge pressure versus temperature at constant (3000 psi) system pressure.

relationship can be obtained by measuring resistance versus displacement. A 4 k Bournes potentiometer was chosen for this application. Figure 57 shows this configuration installed in the A-6E test vehicle. In order to provide for potentiometer extension clearances, the mounting bracket was offset.

Normally, it has been necessary to empty the fluid from the accumulator to measure precharge pressure. However, utilizing a newly developed equation involving system pressure, volume, temperature, and displacement it is now possible to determine precharge pressure without displacing the fluid. Displacement is expressed as a ratio of resistances measured by a linear potentiometer. The equation, graphically displayed in the nomograph of Figure 56, is derived as follows:



R80-2038-062(T)

Figure 56. Precharge pressure nomograph.

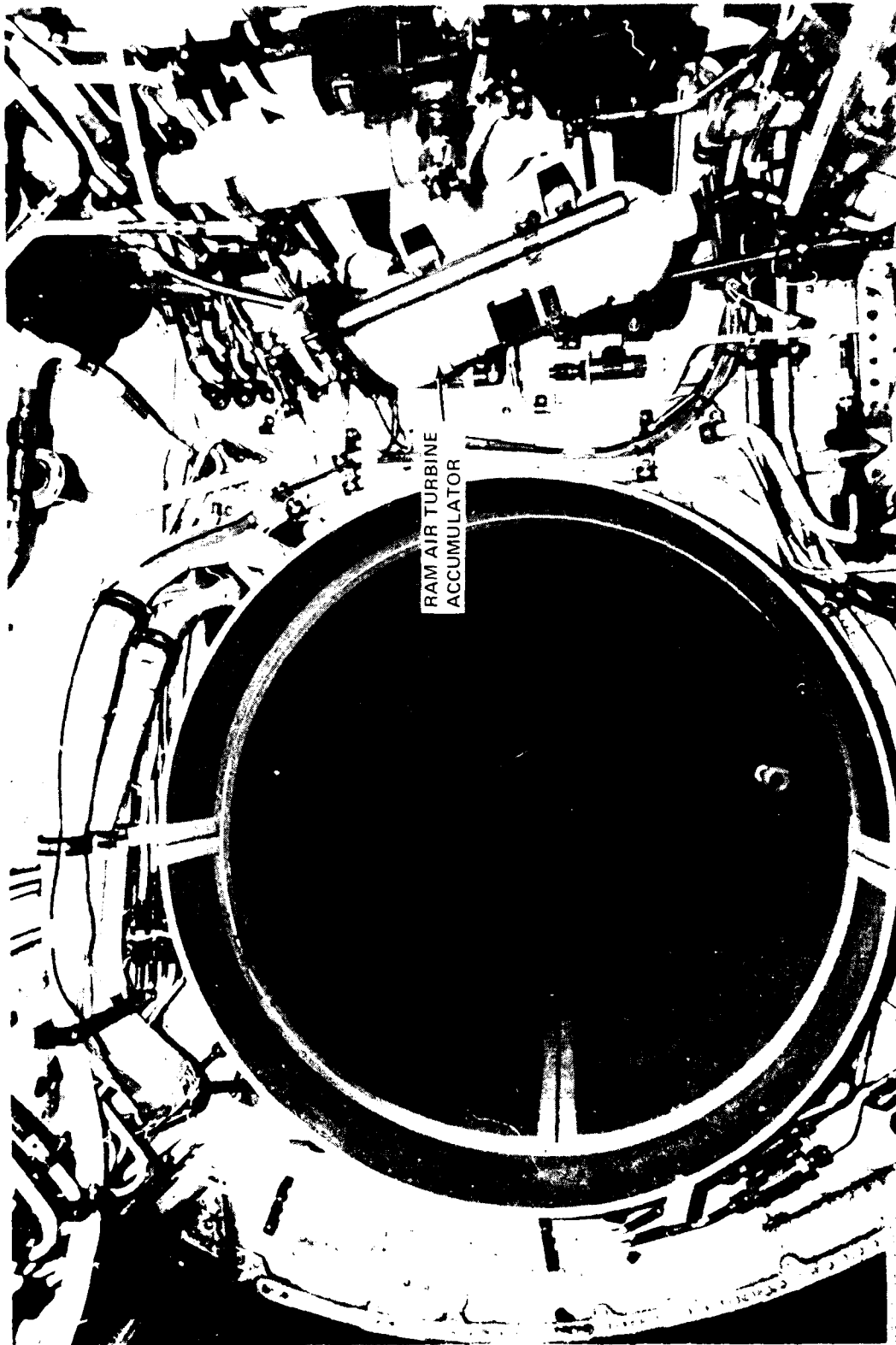


Figure 57. Ram air turbine accumulator installation.

$$\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}$$

$$P_1 = P_{\text{Precharge}} (P_{\text{pr}}), \quad V_1 = 50 \text{ in}^3, \quad T_1 = 70^\circ\text{F} = 530^\circ\text{R}$$

$$P_2 = P_{\text{system}} (P_{\text{sys}}), \quad V_2 = \text{Volumetric Displacement} = 50 \left(\frac{R}{3850} \right)$$

$$T_2 = (T_2 + 460)^\circ\text{R}$$

$$\frac{(P_{\text{pr}}) (50)}{530} = \frac{(P_{\text{sys}}) (50) (R/3850)}{(T_2 + 460)^\circ\text{R}}$$

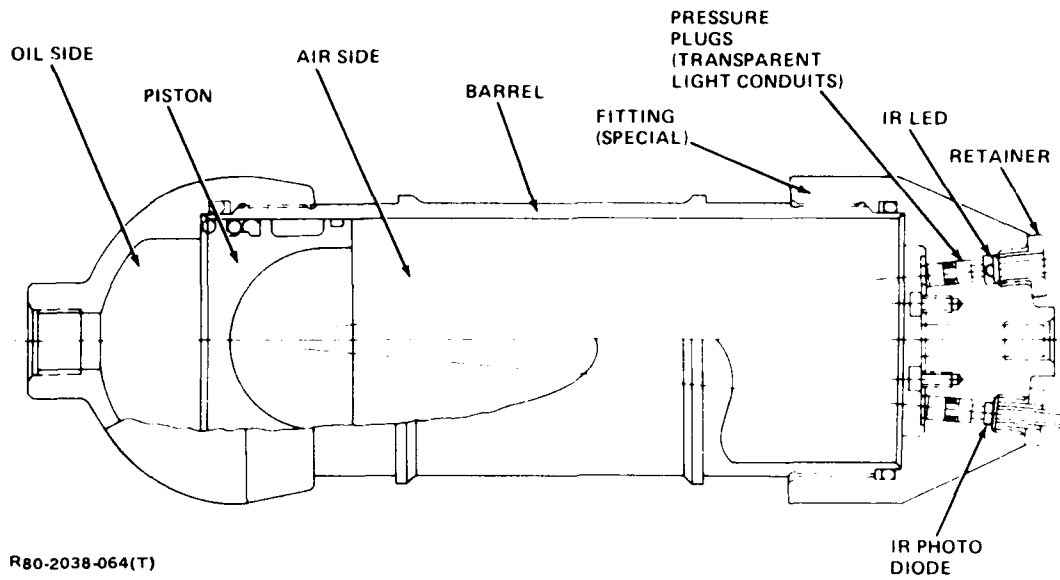
$$(530) (P_{\text{sys}}) (50) (R/3850) = (P_{\text{pr}}) (50) (T_2 + 460)$$

$$P_{\text{pr}} = \frac{(530) (P_{\text{sys}}) (R/3850)}{(T_2 + 460)}$$

Another indirect method of determining piston position using reflected IR energy was investigated. This concept, shown in Figure 58, utilizes an external IR light source whose energy is reflected from the bottom side of the accumulator piston and picked up by an IR photodiode. Preliminary nonpressurized test results are plotted in Figure 59. It should be noted that the curve is relatively flat up to approximately 4 in. of stroke and then changes markedly. The test circuit wiring is shown in Figure 60.

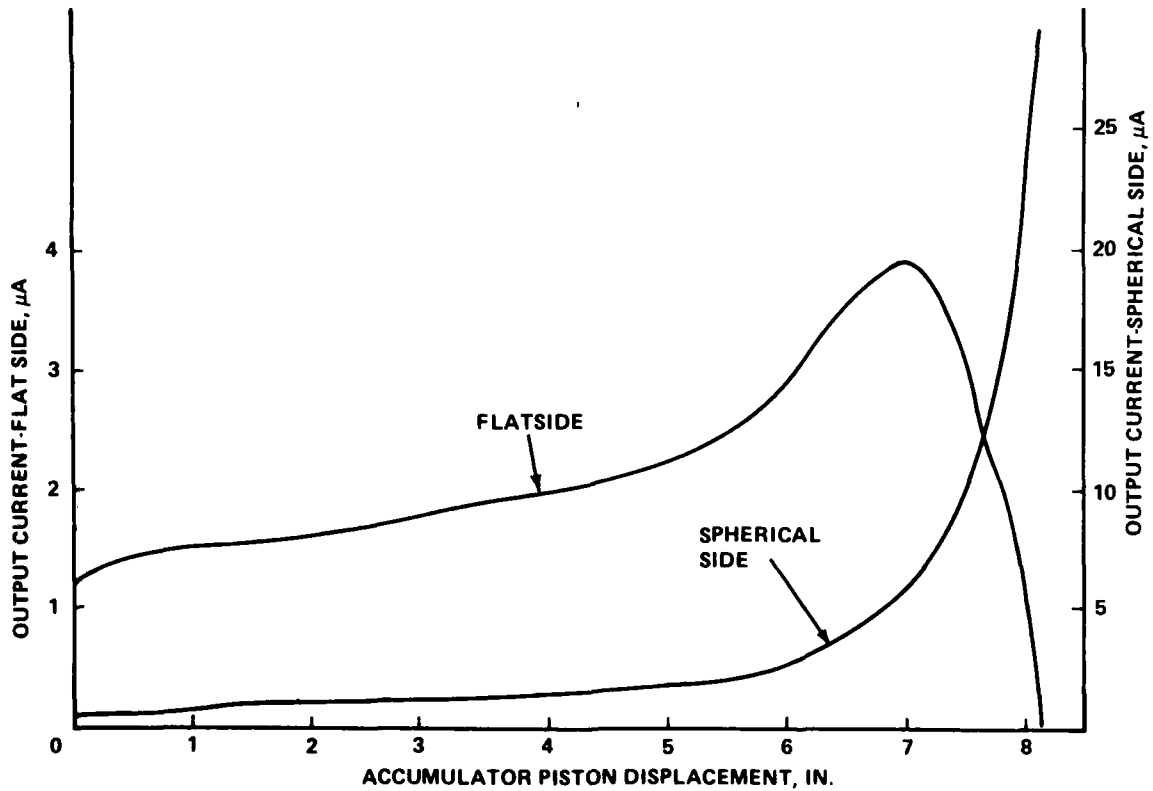
1.3.4.3 Pressure Transducers

The Entran EPS-1032 (Entran Devices, Little Falls, New Jersey) miniature pressure transducer is a thread-mounted semiconductor strain-gage sensor which fits into a 10-32 UNF threaded boss. The transducer employs a face seal and has a full-scale output of 143 mV at 3000 psi pressure with 5 V input (room temperature). There is, however, a temperature shift when tested at -40 and 250°F. Calibration curves for this unit, shown in Figure 61, are very linear over the normal operating range (0-3000 psi). Sensitivity of the transducer is 0.0485 mV/psi. The unit is normally compensated for linearity by using an external compensation module from 80 to 180°F. The wiring diagram is shown in Figure 62.



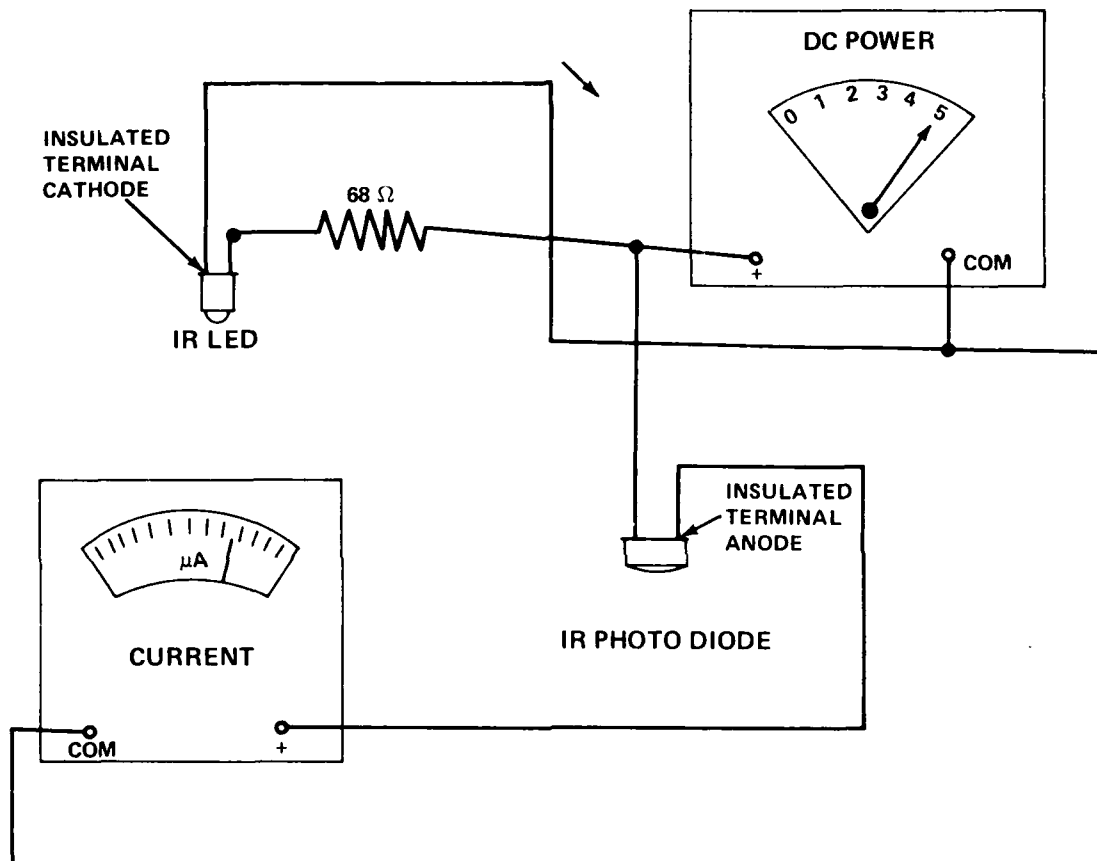
R80-2038-064(T)

Figure 58. Photo-optic accumulator piston displacement sensor.



R80-2038-065(T)

Figure 59. Photo-optic accumulator piston sensor test results.



R80-2038-066(T)

Figure 60. Photo-optic displacement sensor wiring diagram.

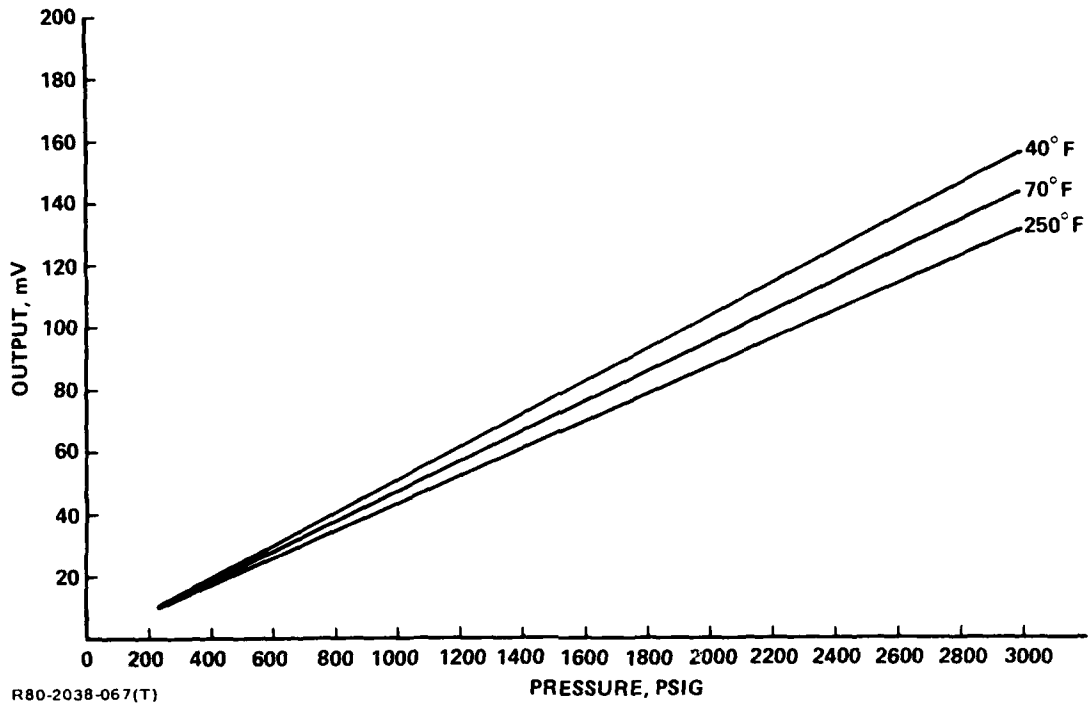


Figure 61. Entran transducer: output voltage versus pressure.

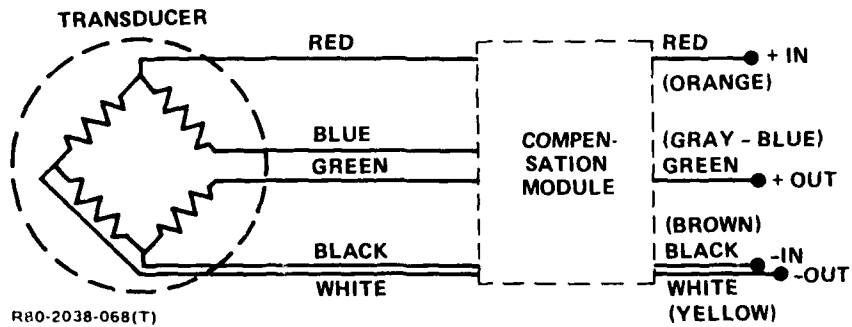


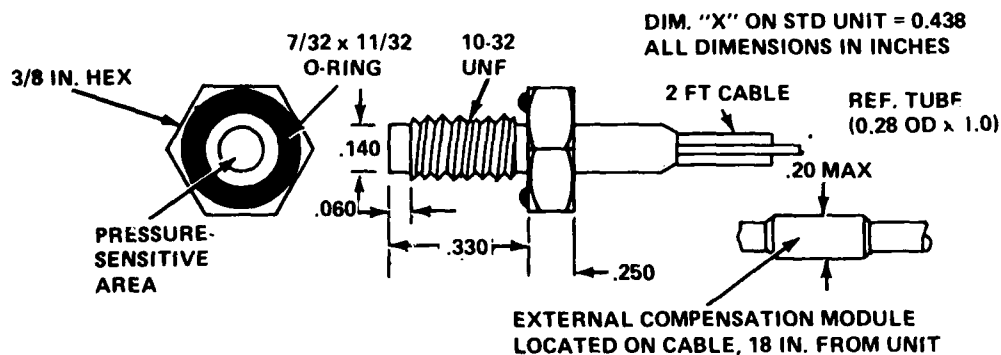
Figure 62. ESP-1032 pressure transducer wiring diagram.

Since the intended application encompassed broader temperature ranges, an extended calibrated temperature range was made. Table 6 shows performance data for the Entran ESP-1032 transducer. Envelope dimensions for a typical unit are shown in Figure 63 (Ref. 7).

TABLE 6. ENTRAN ESP-1032 TRANSDUCER DATA

• <u>MODEL</u> : EPS -1032-2500 (.33), S/N 10 H8H-C1-1	
• <u>TYPE</u> : MINIATURE PRESSURE	• <u>RANGE</u> : 2500 PSIG
• <u>EXCITATION</u> : 6.0 TO 8.0 V	• <u>OVERPRESSURE</u> : 4000 PSIG
• <u>OPERATING TEMPERATURE</u> : -60 TO 250 °F	
• <u>TEMPERATURE COMPENSATION</u> : -60 TO 250 °F	
• EXCITATION: 6 VDC	
• SENSITIVITY: 0.0469 mV/PSIG AT 77 °F	
• THERMAL SENSITIVITY SHIFT, mV/100 °F: $< \pm 2\%/100\text{ }^{\circ}\text{F}$	
• THERMAL ZERO SHIFT, mV/100 °F: $< \pm 1.5\% \text{ FS}/100\text{ }^{\circ}\text{F}$	
• INSTALLATION TORQUE: 15 IN.-LB	
• IMPEDANCE: INPUT: 430 Ω	
	OUTPUT: 239 Ω

R80-2038-070(T)



R80-2038-069(T)

Figure 63. Pressure transducer envelope.

1.3.4.4 Temperature Sensor

The temperature sensor used in the accumulator circuit is the same as that used in the hydraulic reservoir circuit. This sensor assembly uses an analog device: the AD540C integrated circuit temperature transducer. A complete description and test data can be found in Subsection 1.3.1.4.

1.3.5. Rudder

1.3.5.1 Description

As part of the control logic, the rudder was selected to demonstrate the disconnect logic. The concept was to measure and compare input-output signals at or close to the input source rudder pedal and rudder pivot axis.

Since accessibility of the rudder pedal area was not prevalent, the input potentiometer was installed in the turtle deck area.

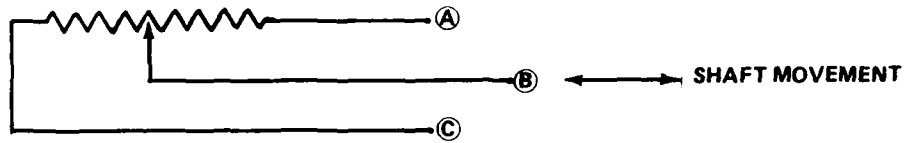
1.3.5.2 Rudder Differential Displacement Circuit

In some aircraft systems, mechanical disconnects have occurred due to disengagement of a bolt or clevis pin in the mechanical/electromechanical linkage. This would not be evident in aircraft which do not have flight-control surface display indicators on the cockpit panel.

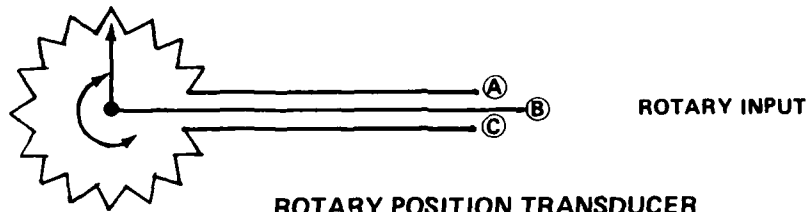
System disconnects can be detected by comparing an input signal to a corresponding output signal. If the output signal does not follow or null out the input signal, microprocessor circuitry will indicate a disconnect condition until corrective action is taken.

Linear or rotary potentiometers are another type of displacement measuring device. Rotary or rectilinear movement of the input shaft positions a contactor (wiper) along or around a continuous resolution resistance element. These devices have practically zero backlash, are insensitive to vibration, and are compact and lightweight. In addition, their cost is low. Rotary transducers are made in multiples of 360° rotation; some cover 3600° (10 turns). Figure 64 shows typical transducer wiring diagrams and a representative plot.

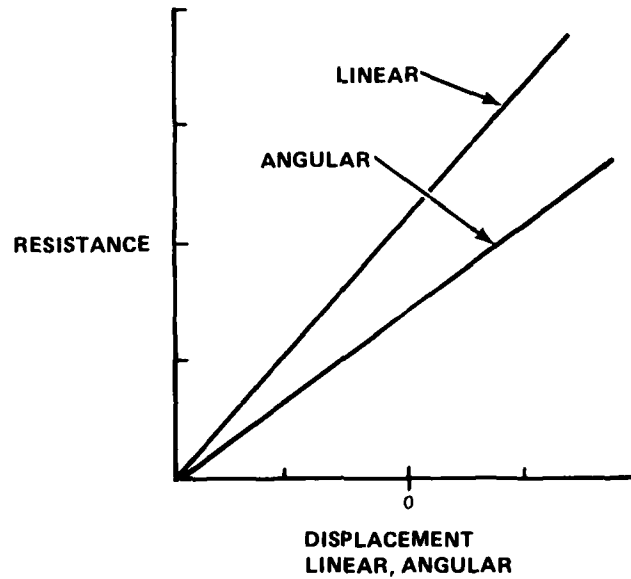
The signal on both transducers are fed to a bridge circuit which detects a variation or omission of an input signal. When this imbalance occurs, the HYCOS circuit is energized.



LINEAR POSITION TRANSDUCER



ROTARY POSITION TRANSDUCER



R80-2038-071(T) POTENTIOMETER DISPLACEMENT vs RESISTANCE

Figure 64. Potentiometer transducers.

Table 7 lists pertinent information on transducers used on the A-6E rudder actuator circuit. Figure 65 shows the turtle-deck potentiometer installation, and Figure 66 shows the rudder position potentiometer installation.

Calibration curves for the installations are shown in Figure 67.

TABLE 7. A-6E RUDDER POTENTIOMETER TRANSDUCERS.

TRANSDUCER	MANUFACTURER	SPEC NO.	TYPE	VALUES	LINEARITY
RUDDER POSITION POTENTIOMETER	ALLEN BRADLY	MIL-R-94	RV45A45D103A	10,000 Ω 2 W	$\pm 10\%$
TURTLE DECK BELLCRANK POTENTIOMETER	ALLEN BRADLY	MIL-R-94	RV45A45D103A	10,000 Ω 2 W	$\pm 10\%$

R80-2038-093(T)

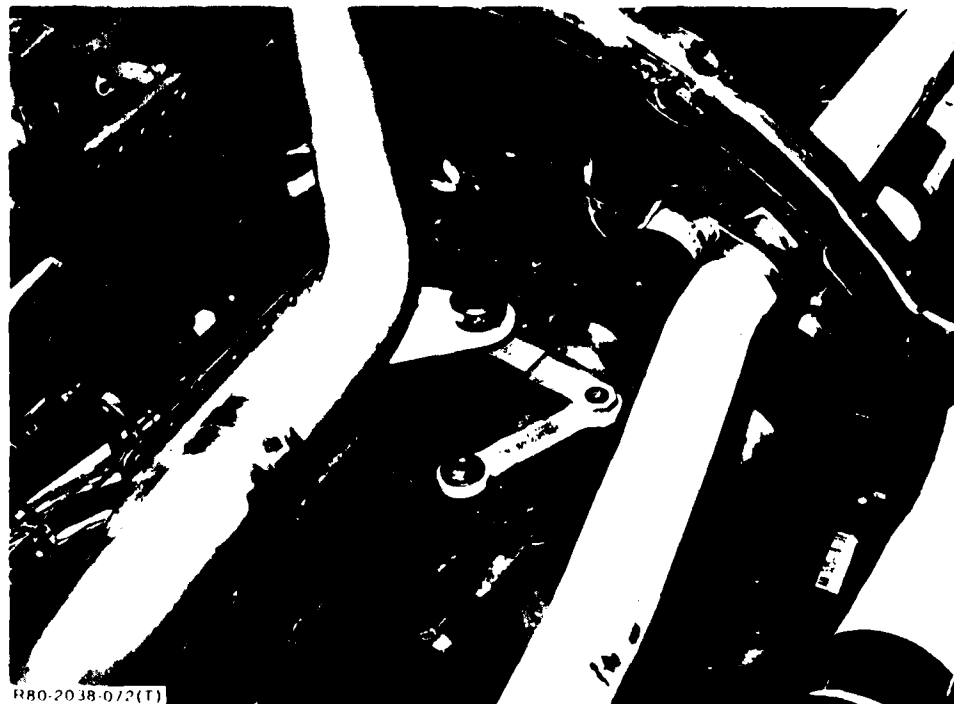


Figure 65. Turtle deck bell crank potentiometer installation.



Figure 66. Rudder position potentiometer installation.

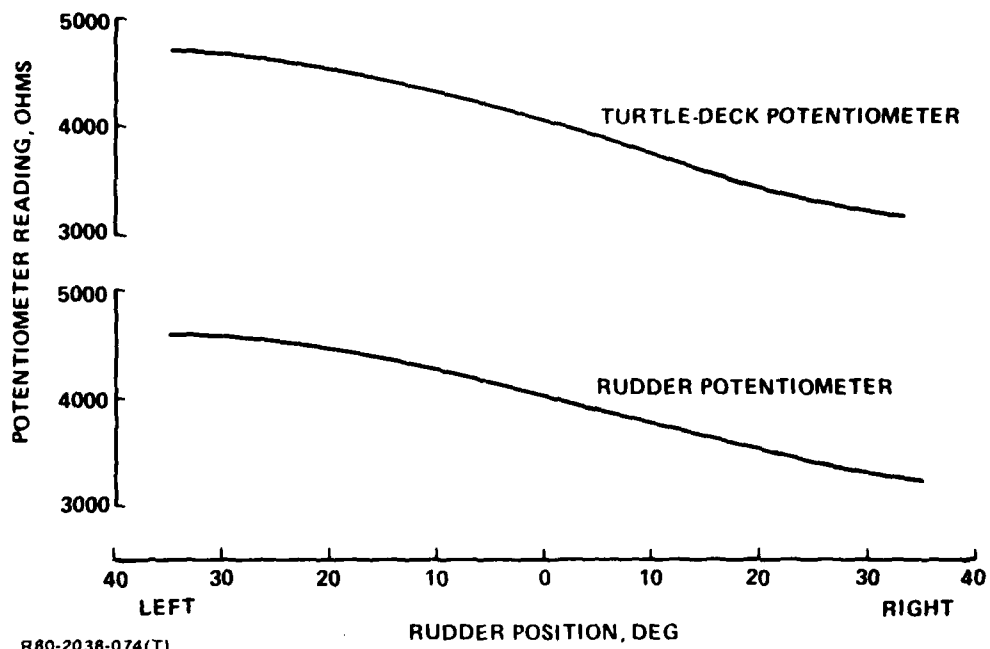
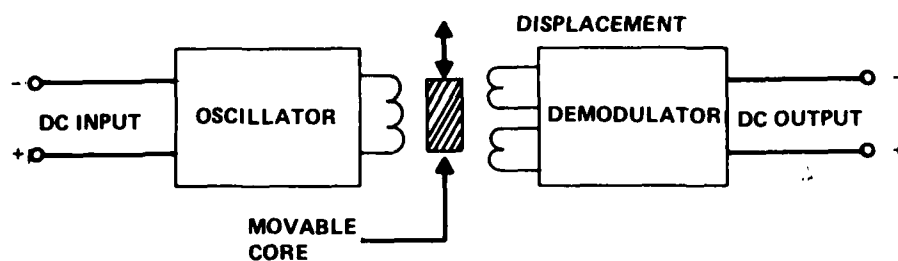


Figure 67. Rudder differential displacement potentiometer calibration.

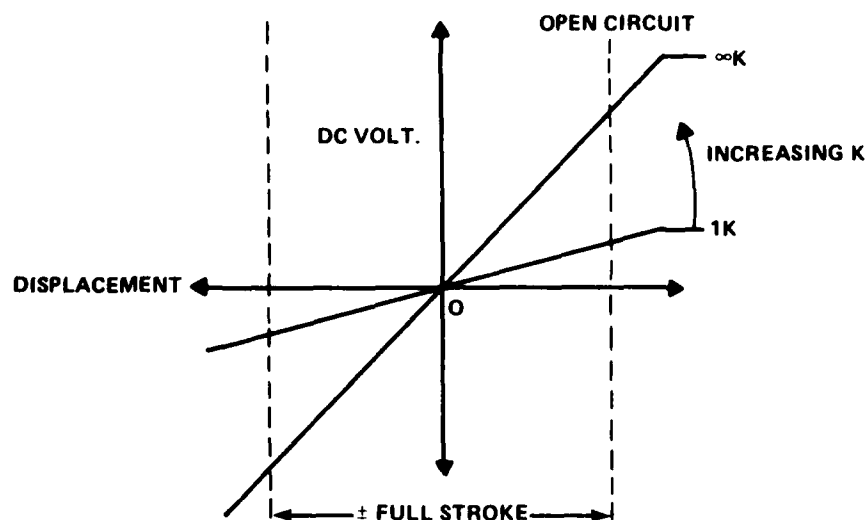
Two basic types of systems were originally considered:

- DC-DC displacement transducers
- Linear or rotary potentiometers.

In DC-DC displacement transducers, an oscillator is used to generate an AC signal which then couples a multiple-leg transformer to a moveable core. The coupling efficiency of the core then determines the position of the element being measured. The signal is then demodulated or rectified to a DC output. Figure 68 shows a typical circuit diagram and output curve.



CIRCUIT DIAGRAM



DISPLACEMENT vs OUTPUT

R80-2038-075(T)

Figure 68. DC-DC displacement transducer.

1.3.6 Display Panel

1.3.6.1 Description

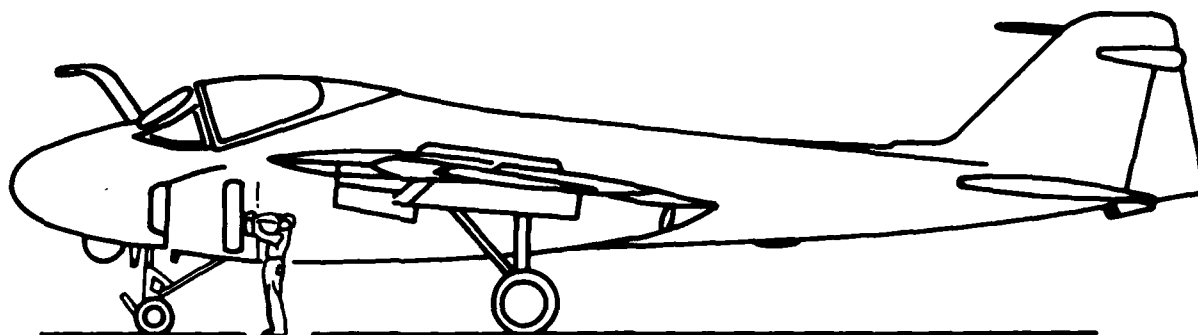
The readout panel is a ground-accessible unit which has clearly labeled lights for indicating component failure conditions. The panel is not accessible to the pilot during normal flight, although certain circuits could be interfaced with a caution-warning panel in the cockpit. Figure 69 shows a typical accessible HYCOS panel location on an operational aircraft. The panel can be interrogated both with and without aircraft or ground-support power.

The primary display panel is a self-contained unit measuring approximately 12 in. by 6.5 in. by 4.5 in. This size was chosen primarily to fit into an available existing space in the proposed flight-test vehicle. When required the size, shape, and weight could be configured to specific vehicle installations. The panel weighs 6.0 lb and contains microelectronic circuits and associated interface elements which are described in detail in subsequent subsections.

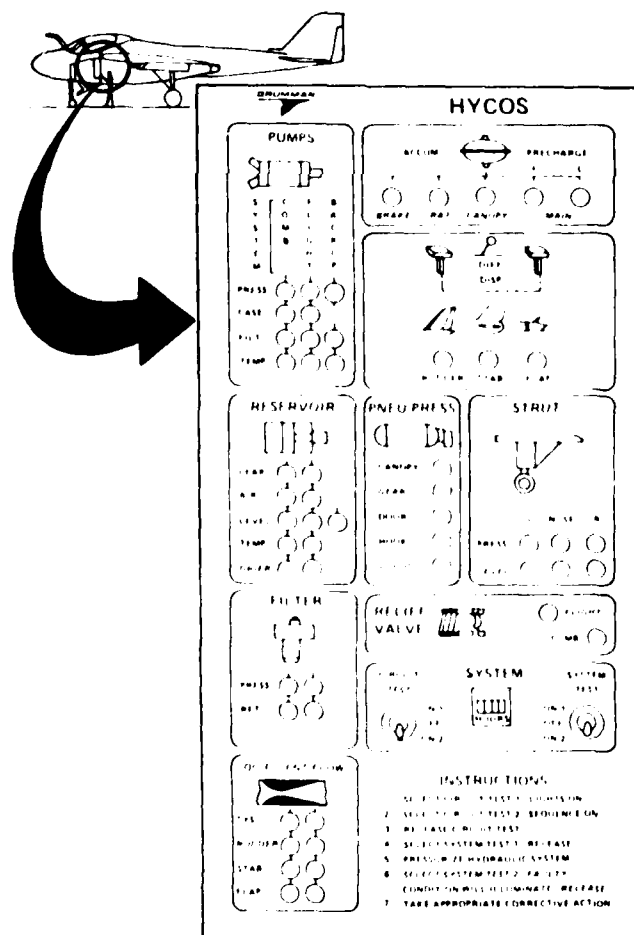
Basically, the panel houses:

- Display grain of wheat lamps
- Fiber-optic interface outlets
- Lamp drivers
- Counters
- Shift registers
- Power interface
- Sensor and system test circuits
- Microprocessor
- Analog-to-digital converters
- Memories
- Rechargeable NiCd batteries
- Battery heating and charging circuits.

Figure 70 shows the display panel connector interfaces, while Figure 71 shows the panel installed on the flight test vehicle.



TYPICAL HYCOS ACCESS LOCATION



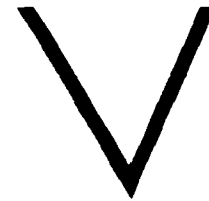
R80-2038-076(T)

Figure 69. HYCOS panel location on typical aircraft.

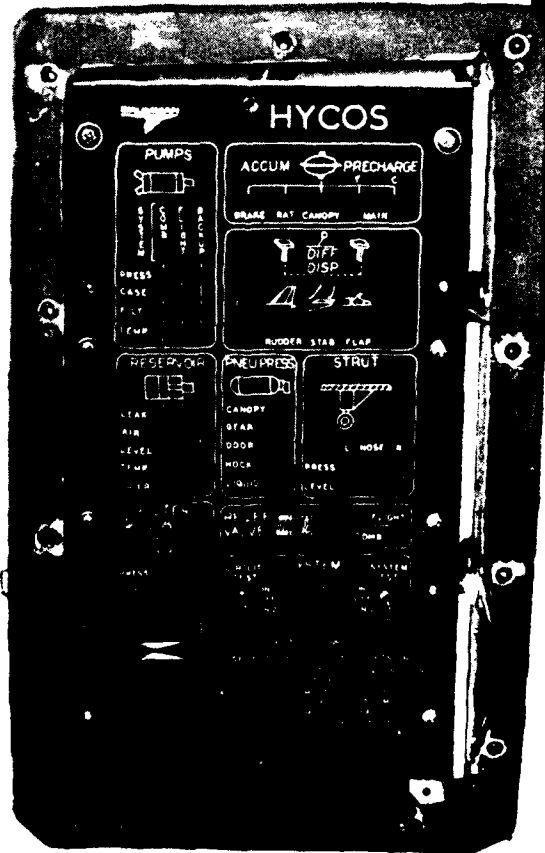


Figure 70. HYCOS panel showing bottom connectors.

TAKE



PILOTS RESCUE
PUSH →
CANOPY JETTISON ONLY



CANOPY GRD.

CIRCUIT BKR.

HB0 20 18 078(1)

AN 45W33

Figure 71. HYCOS installation in flight test vehicle.

1.3.6.2 Display Panel Indicators

Several types of display indicators were considered at the beginning of the program. These included LEDs, LCDs, LCDs with backscatter lighting, and subminiature incandescent lamps. Subminiature incandescent lamps are called "grain of wheat" bulbs due to their small size. After careful evaluation, the decision was made to utilize subminiature incandescent lamps since they offer good visibility during daylight and have an acceptable operating temperature range.

LEDs have some advantages but are not readily visible during daylight high-sun conditions. Since the intent of HYCOS is to place the display panel in an external ground-accessible area, the subminiature incandescent lamp was selected.

Table 8 compares the indicators considered. Size-for-size, the subminiature incandescent lamps exhibit good visibility under sunlight conditions. Although their current drain is higher than the other types considered, their ability to provide good daylight visibility became an overpowering factor. The use of lamps with a 60 mA rating would provide good service life (5000 hr average) and adequate illumination under sunlight conditions. Figure 72 illustrates the basic types of indicator displays (Ref. 8). Figure 73 is a plot of spectral output for various display types as observed by human eye response.

Since as many as 50 display indicators could light up under circuit test conditions, the NiCd battery momentary current drain could be 3 A or higher, neglecting the power requirements for the microprocessor and associated circuits. This condition occurs when the ship's battery and/or engine electrical power is on. This is a momentary high drain for the NiCd battery and did not significantly affect service life. With ship's power on, adequate monitoring panel and sensor current is available.

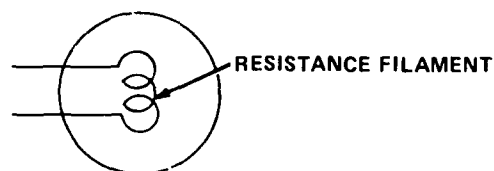
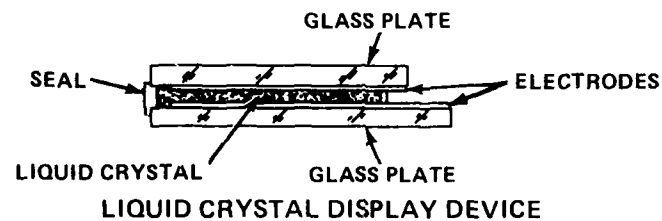
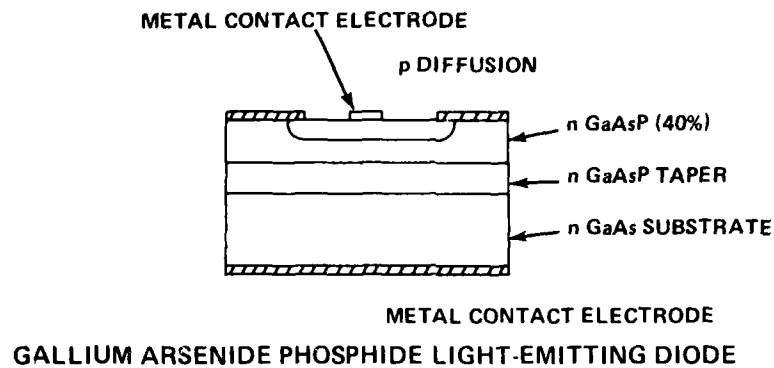
Another technique for reducing power drain is to use the microprocessor timer to sequentially test each subsection when the circuit test button is depressed. Under system test conditions, it is highly unlikely that more than five components would indicate failure modes and require power at any one time.

All grain of wheat bulbs are replaceable from the front of the panel by first removing the red plastic cover. Individual and collective circuit and bulb tests can be performed to verify the integrity of each indicator bulb.

TABLE 8. HYCOS DISPLAY INDICATOR CONSIDERATIONS.

DISPLAY TYPE	POWER REQUIREMENTS		VISIBILITY			COMMENTS
	VOLTAGE, V	CURRENT, mA	SUNLIGHT	NIGHT	BRIGHTNESS	
LED (LIGHT-EMITTING DIODES)	5	20	POOR LIMITED WITH LIGHT FILTER	GOOD	30-300 FOOT-LAMBERTS	<ul style="list-style-type: none"> • OPERATING TEMPERATURE RANGE: 58 TO 212°F • LONG LIFE • LOW OPERATING VOLTAGE • RUGGED • SMALL SIZE • RESPONSE TIME, NANOSECONDS
LCD (LIQUID CRYSTAL DISPLAYS)	5	30 (6 SEGMENTS)	GOOD	POOR	PASSIVE DISPLAY REQ. VIRES AMBIENT OR SEPARATE LIGHT SOURCE	<ul style="list-style-type: none"> • OPERATING TEMPERATURE RANGE: 14 TO 140°F (0 to 60° C) • BECOMES SLUGGISH AT LOWER TEMPERATURES • RELIES ON EXTERNAL LIGHT SOURCE FOR VIEWING AT NIGHT
LCD WITH BACK SCATTER LIGHTING	5	30+ (15 FOR BACKSCATTER LAMP)	GOOD	GOOD TO FAIR	SIMILAR TO INCANDESCANT	<ul style="list-style-type: none"> • COMPLEX, BULKY, TEMPERATURE LIMITED
SUBMINIATURE INCANDESCANT LAMPS	5	15 TO 60	GOOD	GOOD	> 1000 FOOT-LAMBERTS	<ul style="list-style-type: none"> • LIMITED BY MULTIPLE LAMP CURRENT DRAIN DURING BATTERY OPERATION • HEAT DISSIPATION A SIGNIFICANT CONSIDERATION • BRIGHTNESS OF ALL DISPLAYS • LOW VOLTAGE REQUIREMENTS • RESPONSE TIME IN MILLISECONDS • VIBRATION-RESISTANT IN SMALL SIZES

R80-2038-079(T)



R80-2030-080(T)

Figure 72. Types of display indicators.

AD-A100 730

GRUMMAN AEROSPACE CORP BETHPAGE NY
HYDRAULIC DIAGNOSTIC MONITORING SYSTEM. (U)
MAR 81 J J DUZICH

F/G 14/2

UNCLASSIFIED

NADC-TR-81073-60

N62269-78-C-0041

NL

2 OF 4

40 A
1100730



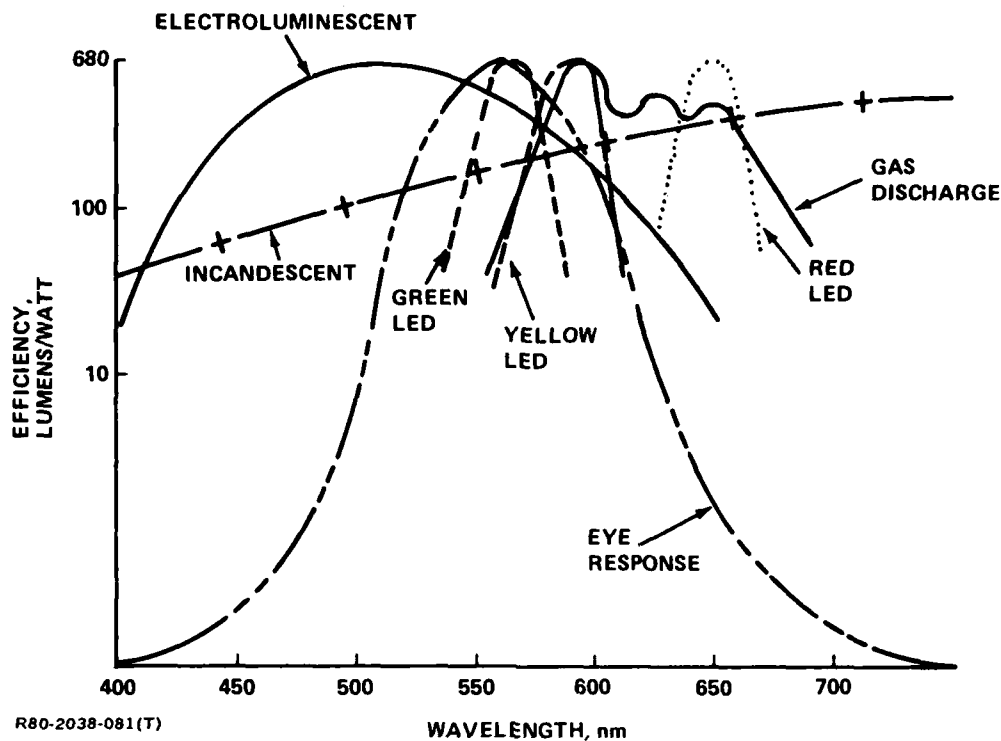


Figure 73. Spectral output of various displays compared to response of human eye.

1.3.6.3 Microprocessor

The Intel 8748 (Ref. 9) is a single-component, 8-bit microcomputer fabricated on a single silicon chip using the N-channel silicon gate MOS process. Unlike the 8048, the 8748 has an erasable program memory which can be varied for tests and evaluation during the prototype and reproduction stages. The 8748 is easily programmable and has sufficient room for additional programs and/or add-on functions. In particular, it:

- Is an 8-Bit CPU containing ROM, RAM, I/O, and a Timer in a single package
- Is powered by a single 5 VDC power supply
- Responds in a 5.0 μ sec cycle. All instructions use one or two cycles
- Has a 1K by 8-bit EPROM, 64 by 8-bit RAM, and 27 I/O lines
- Contains an internal timer/event counter
- Has a single-level interrupt.

A block diagram of the 8748 is shown in Figure 74. Figure 75 shows a typical pin arrangement for this unit.

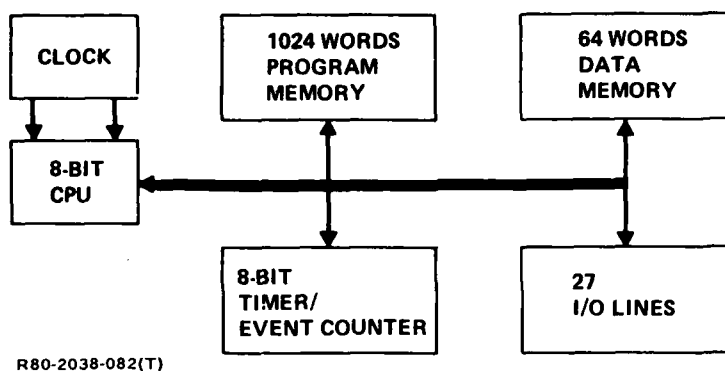


Figure 74. Intel 8748 block diagram.

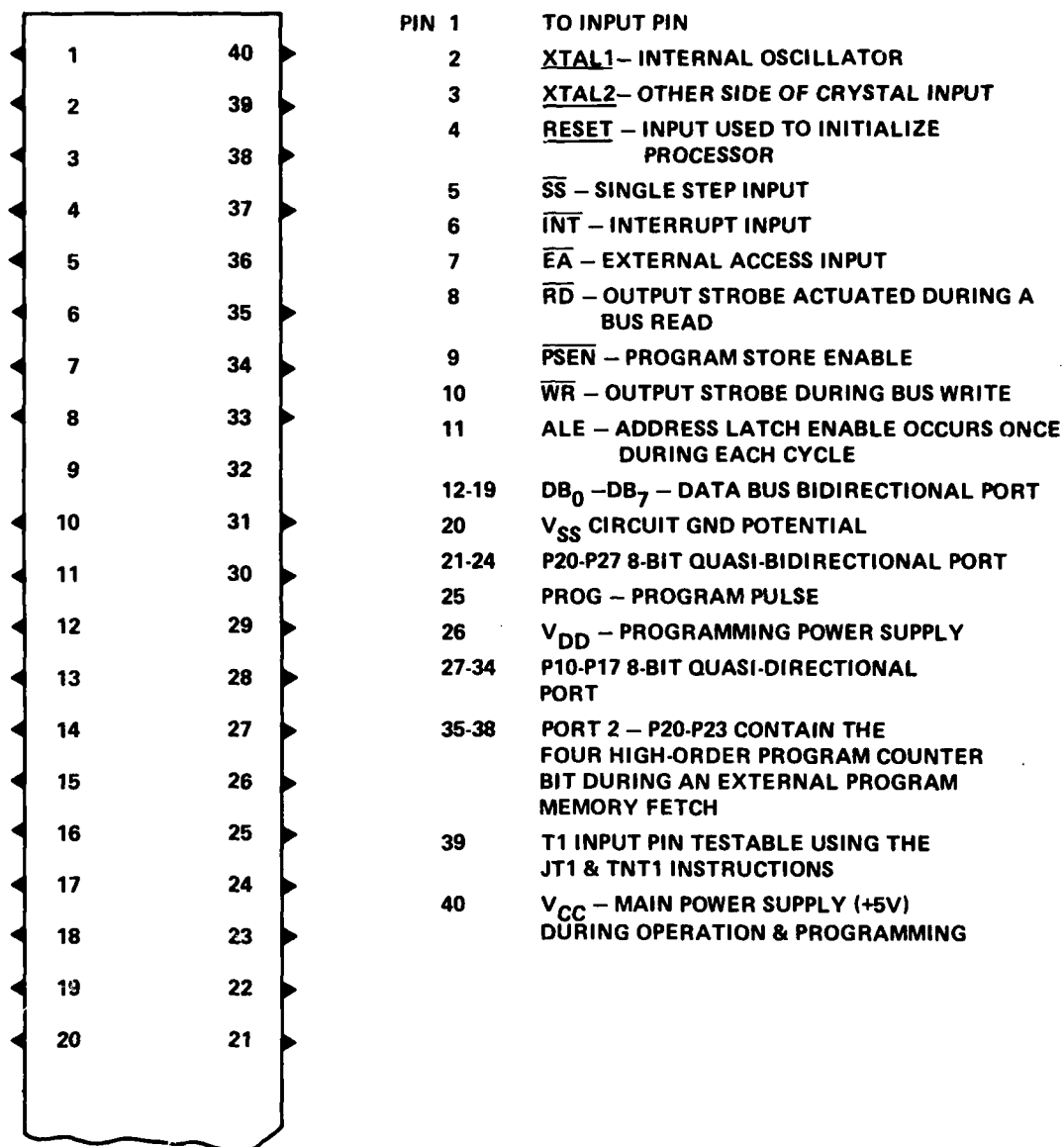
1.3.6.4 Charging Circuit

A charging circuit was designed into the system to keep the twelve nickel-cadmium batteries charged when the vehicle is on ground-support power or on an operational mission.

A transformer is used to step-down the 115 VAC, 400 Hz power supply. Rectification is accomplished by a diode to a DC value slightly higher than the 5 VDC system. Since nickel-cadmium batteries are difficult to charge below 0°C, external heaters are used to maintain battery temperatures above this value.

1.3.6.5 Heating Circuit

Since the NiCd batteries must be charged with the vehicle flying at various altitudes, thermostat-controlled battery strip heaters are incorporated. When the temperature drops below 0°, the heating strip functions until the surface temperature reaches 32°F. This thermal cycling enables the batteries to achieve and retain a full charge. Figure 76 shows charging characteristics of NiCd batteries as a function of temperature (Ref. 10). During the flight test programs, modifications were made to the battery charging circuit to reduce the charging rate and provide for an external access connector. This connector was used to check status on battery voltages and provide an external dedicated recharge capability. Both battery analysis and external battery charging circuits are discussed in Appendix I.



R80-2038-083(T)

Figure 75. Intel 8748 pin configuration.

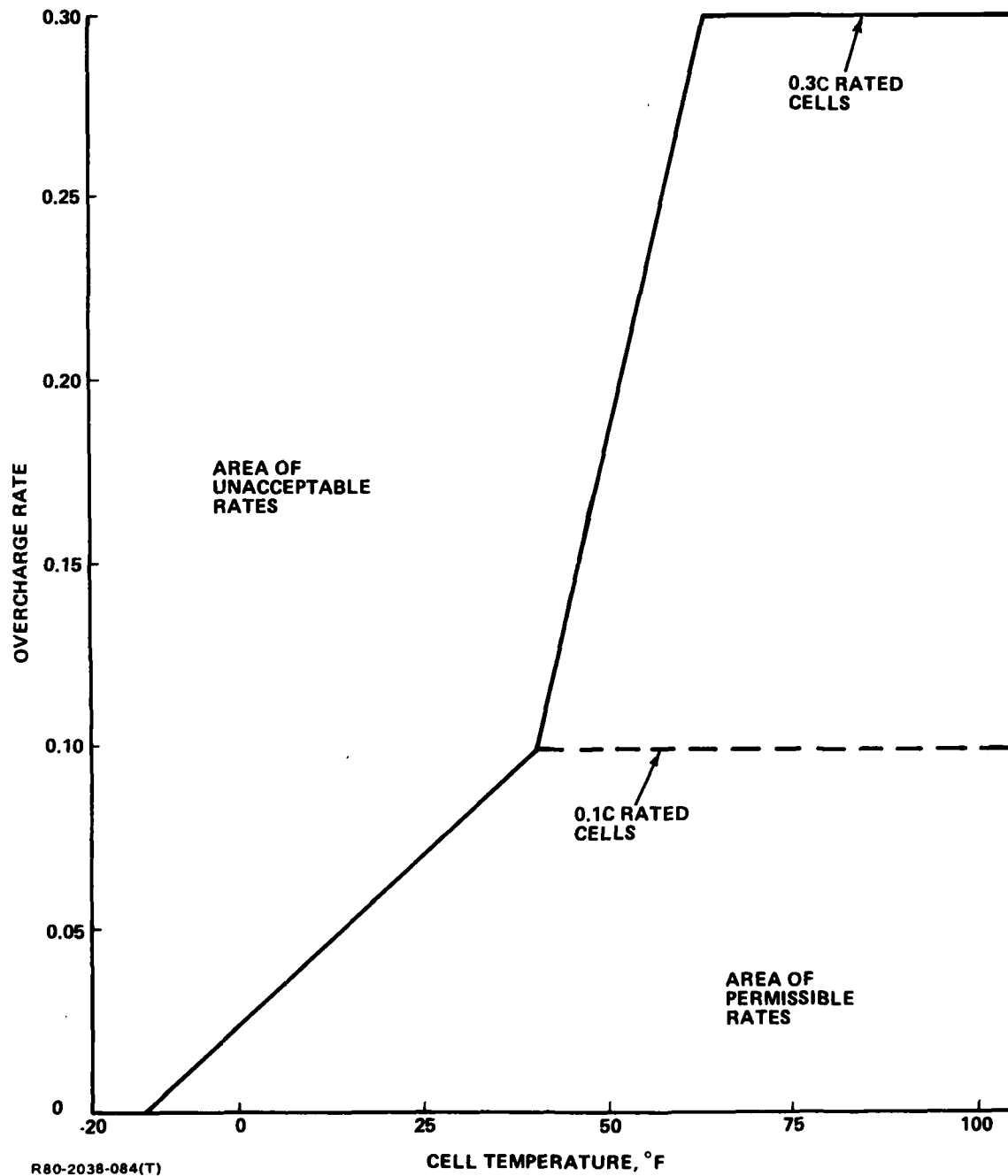


Figure 76. Nickel-cadmium battery charge characteristics.

1.3.6.6 Wiring Circuit

The basic wiring circuit is shown in Appendix I. Four removable display cards (Figure 77) comprise the major portion of the circuit and consist of the following:

- Card No. 1: Microprocessor - memory and display drivers
- Card No. 2 & 3: Counters and A/D converters
- Card No. 4: Interface circuits.

Figure 78 shows the HYCOS panel with its cover removed.

Basic card element functions are as follows:

- Microprocessor - unit, controls all calculations
- Lamp Drivers - supplies current to display lamps
- Output expanders - receives three inputs and delivers eight different outputs
- Dual flip-flops - used for data storage
- A/D converters - receives analog data and converts it to a 8-bit digital word
- Hex Buffer - used to drive data bus
- Counter latch; seven-segment driver - counts pulses, stores value, and drives seven-segment display
- Transistors - amplifies pulse input and potentiometer signals
- Schmitt Trigger - used to square waveshapes
- Diodes - used for lamp test isolation and to rectify AC for battery charging
- Batteries - 1 A-hr battery drives high-power circuits and 100 mA-hr battery supplies low-power requirements.

1.3.6.7 HYCOS Flow Diagram and Program Limits

Program limits are established for the particular subsystem in question. A math model was first established which defines the normal operating parameters. When these limits are exceeded either individually or collectively, the program subroutine detects the discrepancy and provides the proper circuit response.

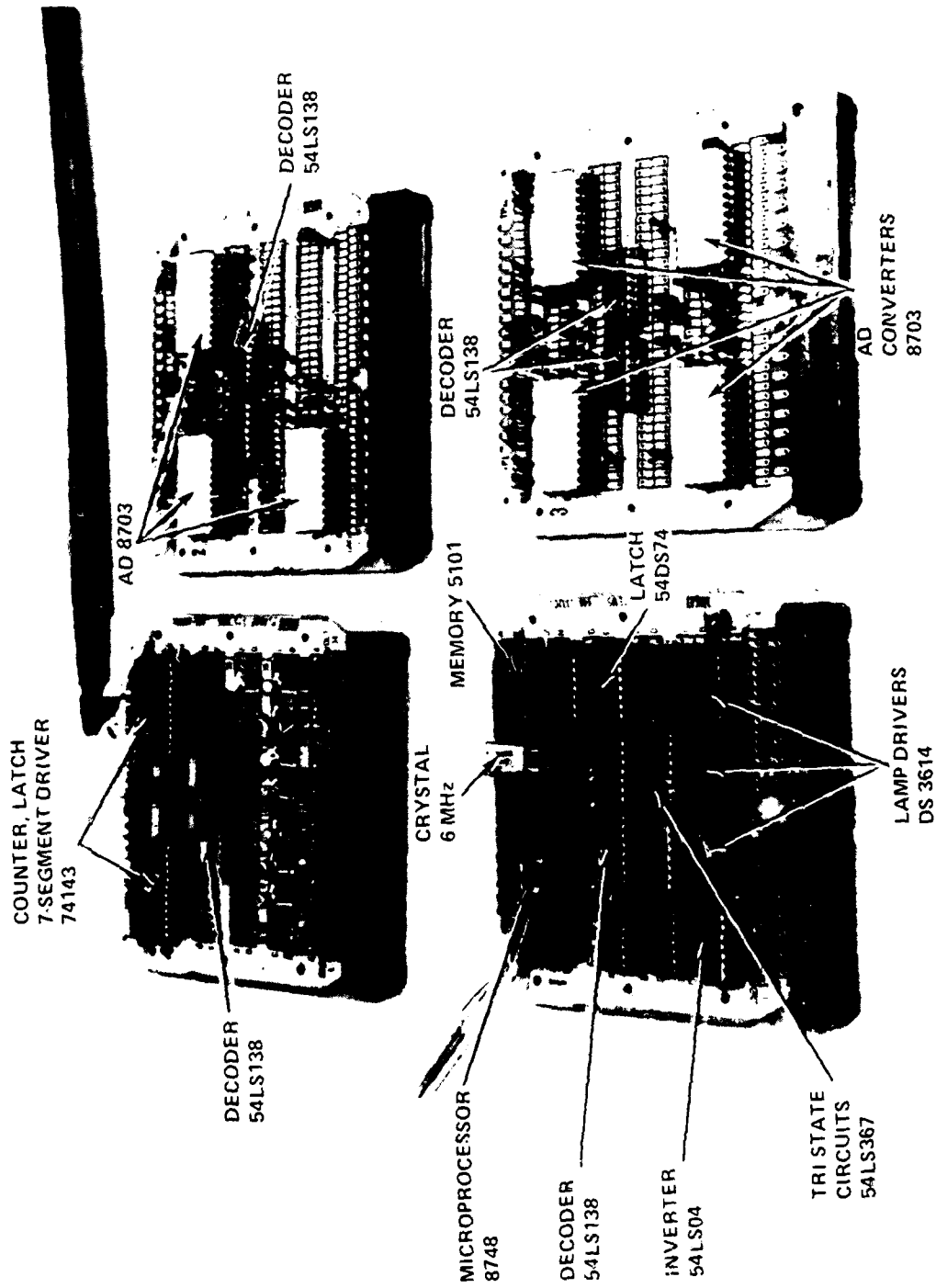
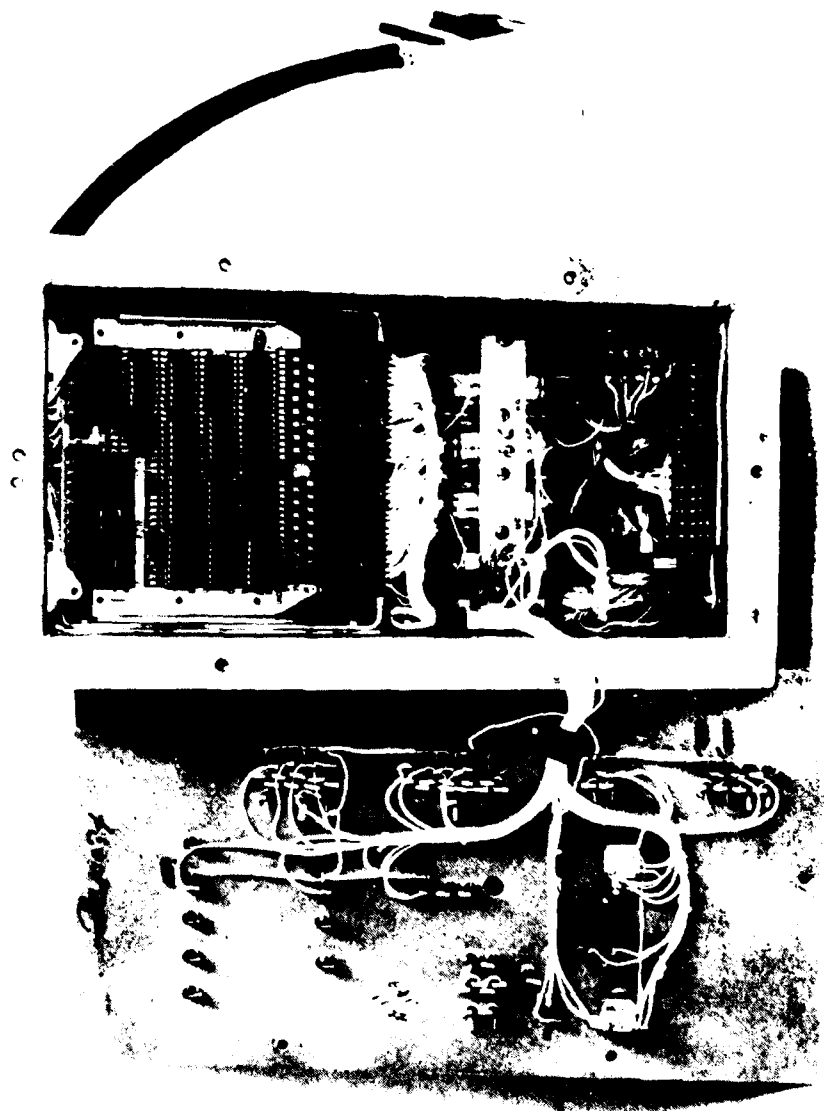


Figure 77. Removable display cards.

R80-203A-085(T)



R80-2038-086(T)

Figure 78. HYCOS panel with cover removed.

The program flow diagram is broken down into six basic routines:

- Executive Routine
- Sequence Routine
- RAM Load Routine
- Rudder Routine
- Reservoir Routine
- RAT Routine.

Additional details of the flow diagram and the microprocessor program are listed in Appendix K.

1.3.7 Hydraulic Filters

1.3.7.1 Filter Differential Pressure Indicators

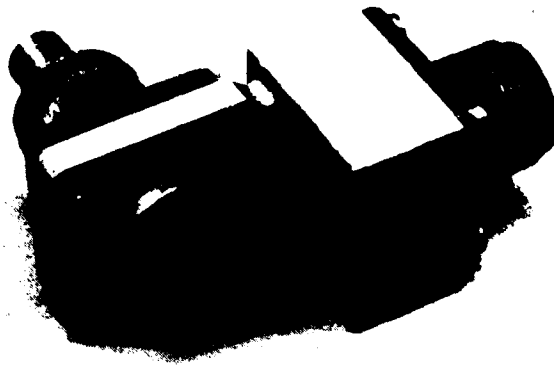
Filter differential pressure indicators, commonly used in the fluid power industry, are an indirect means of identifying contaminated filter elements which require servicing. The indicator is usually mounted to the filter head or bowl and provides a visual signal when a predetermined element differential pressure has been exceeded. In order to take into account fluid viscosity changes due to thermal conditions, various means are employed to preclude indicator operation before the system reaches normal operating temperature. One method uses a bimetallic sensing unit placed in close proximity to the visual indicator; another employs a temperature-sensitive gas, fluid, or elastomer.

To provide remote indication capability, an electrical switch may be mechanically or otherwise actuated by the primary sensor indicator. Resetting the mechanical indicator also resets the electrical circuit.

A boot or transparent cap is provided over the indicator to improve reliability by making it less susceptible to extrinsic debris and fluid. This cap is physically restrained or bonded to the adjacent element. Figure 79 shows a typical interchangeable differential pressure indicator. An actual installation photograph is shown in Appendix J.

1.3.7.2 System Fluid Sampling

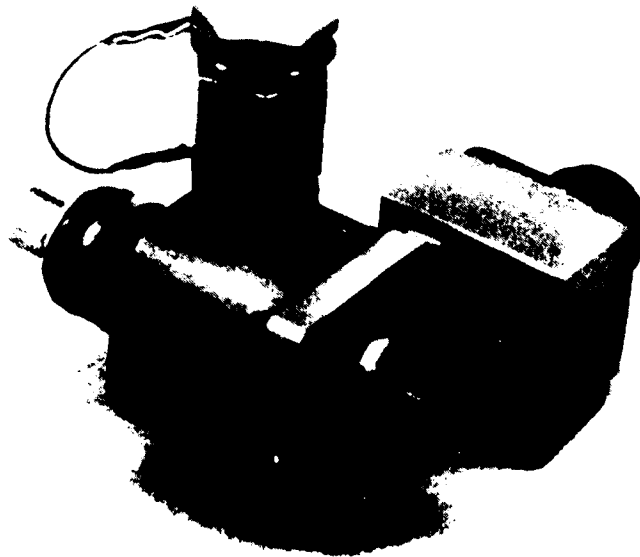
Another version of the delta-p indicator contains a sampling port which permits fluid extraction from the upstream side of the filter element while the system is pres-



R80-2038-087(T)

Figure 79. Filter differential pressure indicator.

surized. One such type of "Multicator"* is shown in Figure 80. Figure 81 shows an installation in the pump case drain filter.



R80-2038-088(T)

Figure 80. Filter differential pressure indicator with sampling valve.

* Multicator is an APM Trademark

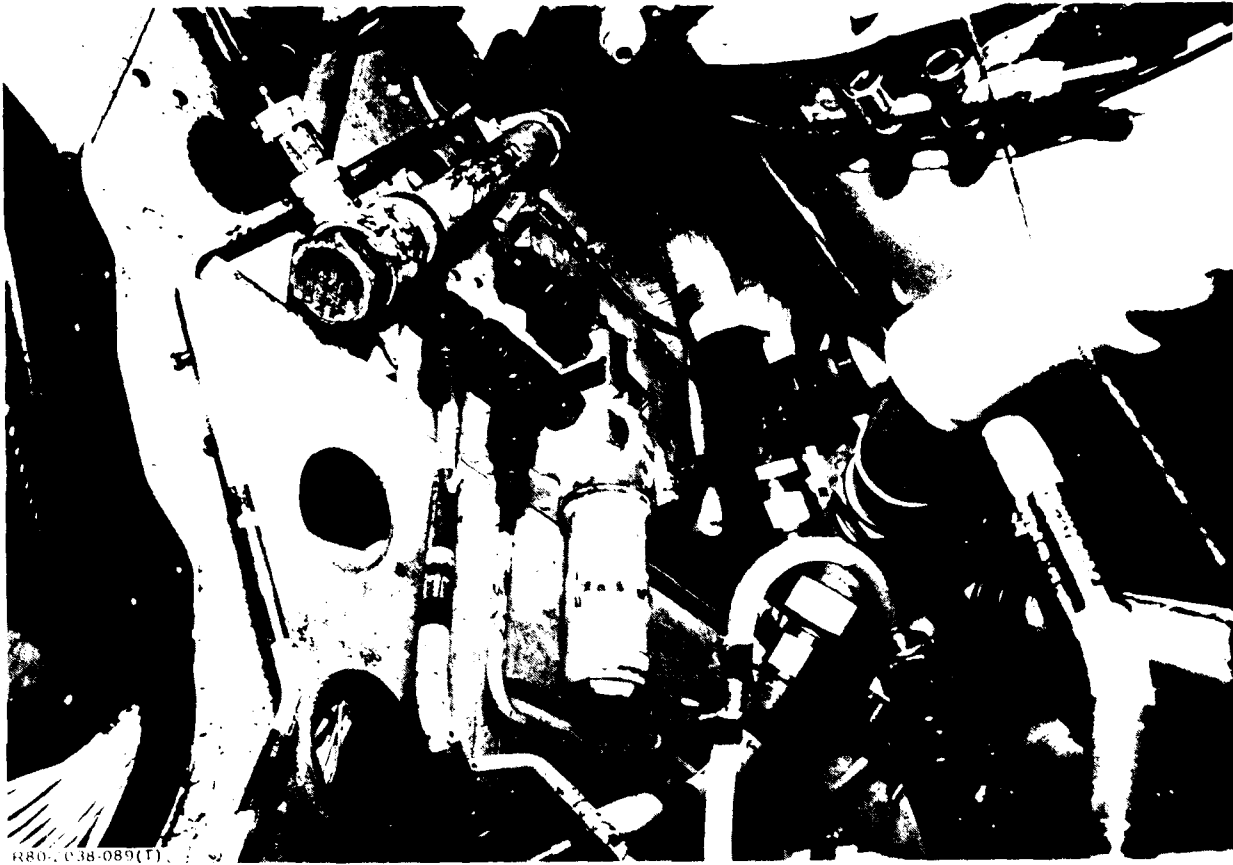


Figure 81. Multicator indicator installation in pump case drain filter.

A special wired plug is used to protect the sampling port when not in use, and also acts as a redundant pressure seal.

Grumman Specification 202 defined the pertinent parameters of each unit used for the HYCOS Program.

It should be noted that most visual and electrical indicators are usually discrete signals (Go/No-Go type). In cases where an analog signal is required, this may be provided by using the approach shown in Figure 82. This concept utilizes a linear output Hall Effect sensor actuated by a movable permanent magnet which is coupled to a spring-biased piston. Movement of the sensing piston magnet affects the magnetic flux density seen by the Hall Effect sensor, reducing the output signal. Since the sensor output varies as a function of ambient temperature, temperature compensation must be provided.

1.3.8 Flight Control Hydraulic Backup Package

A Klaxon overtemperature switch was bonded to the flight control backup module to measure system and closed-loop surface overtemperature conditions. The switch conforms to Grumman Specification 201 and has a trip setting of $300 \pm 20^\circ\text{F}$. It is manually resettable through a neoprene overmold. Figure 83 (Ref. 11) shows typical switch characteristics. Actual installation on the flight control backup module is shown in Figure 84. Operation of the hydraulic backup package occurs during preflight check and only if one hydraulic system is lost.

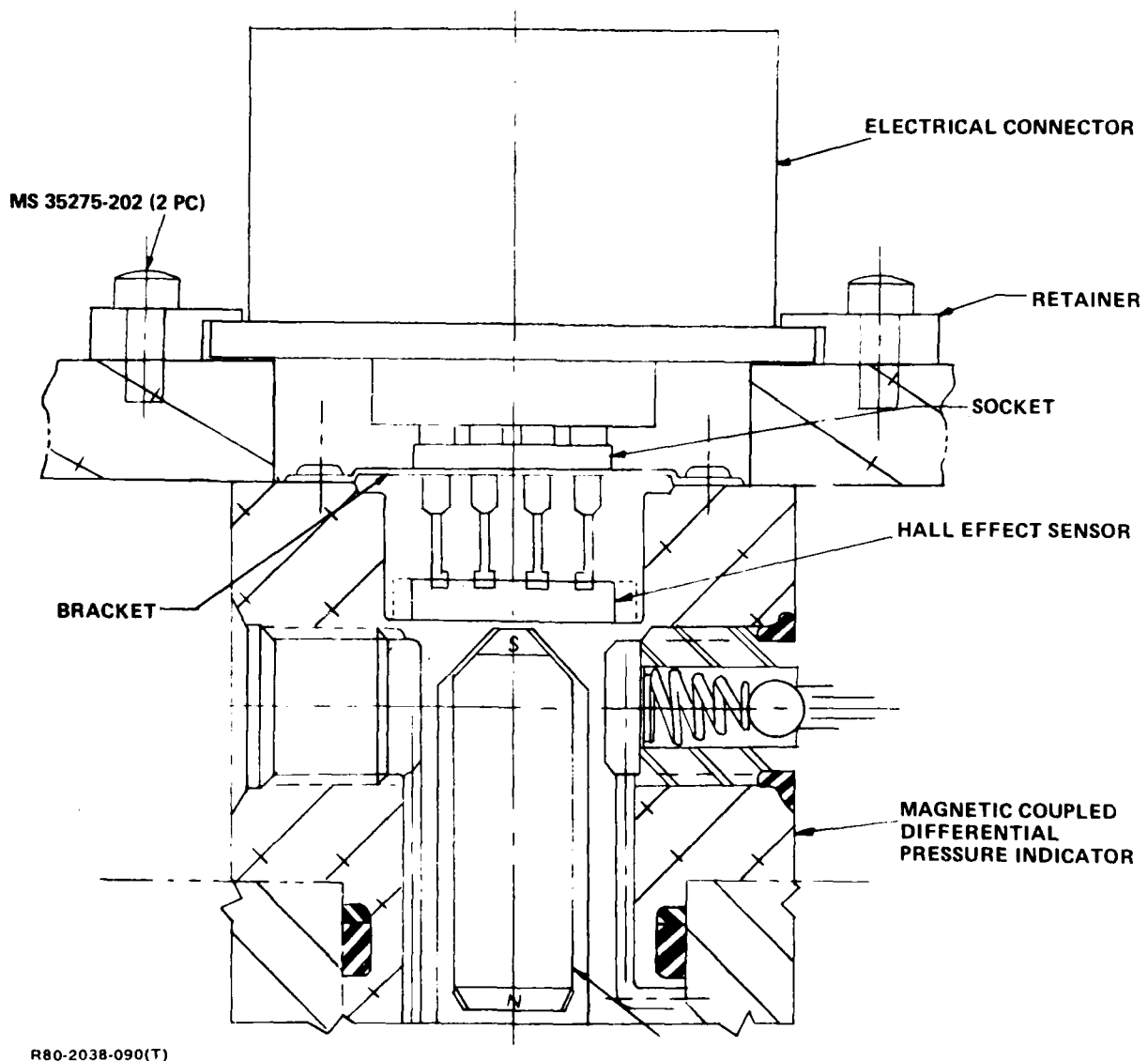


Figure 82. Linear output Hall Effect differential pressure indicator.

- SNAP-ACTION SWITCHING
- NORMALLY OPEN OR NORMALLY CLOSED
- AUTOMATIC OR MANUAL RESET
- SPST OR SPDT
- OVERMOLD OPTIONAL

PERFORMANCE CHARACTERISTICS

DIELECTRIC STRENGTH:

1250 VAC, RMS, 60 CYCLES FOR ONE MINUTE (1500 VAC RMS AVAILABLE ON SPECIAL REQUEST)

AMBIENT TEMPERATURE RANGE:

NON OVERMOLD – 65°F TO 450°F
NEOPRENE OVERMOLD – 65°F TO 160°F
SILICONE OVERMOLD – 65°F TO 450°F

SWITCH ACTION:

SPST OR SPDT (SNAP-ACTION)

LIFE CYCLE:

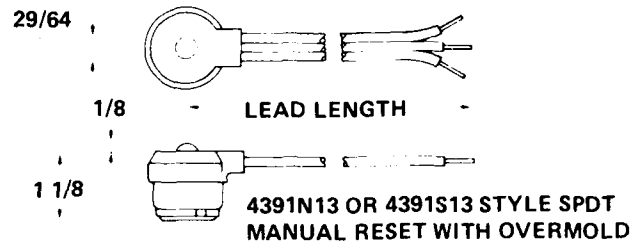
SEE ELECTRICAL RATING TABLE

VIBRATION:

STANDARD CONSTRUCTION 5-500 CPS, 3G's
HIGH VIBRATION CONSTRUCTION 5-500 CPS, 5G's

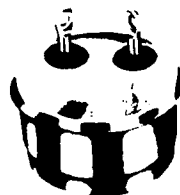
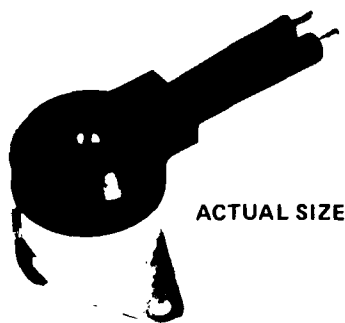
WEIGHT:

WITHOUT OVERMOLD 21 GRAMS AVERAGE
WITH OVERMOLD 56 GRAMS AVERAGE

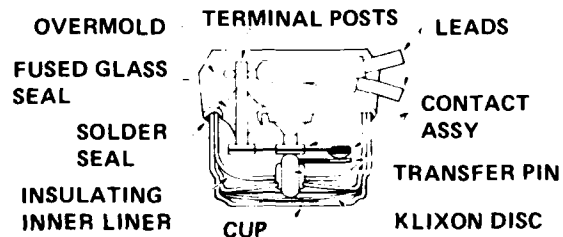


ELECTRICAL RATINGS (RESISTIVE)

AMPERES			LIFE CYCLES
30 VAC/DC	125 VAC	250 VAC	
10	4	2	100,000
11	6	3	50,000
12	8	4	25,000
13	10	5	10,000
14	12	6	5,000



CROSS-SECTION VIEW OF TYPICAL UNIT WITH OVERMOLD (AUTOMATIC RESET)



R80-2038-091(T)

Figure 83. Resettable temperature switch characteristics.

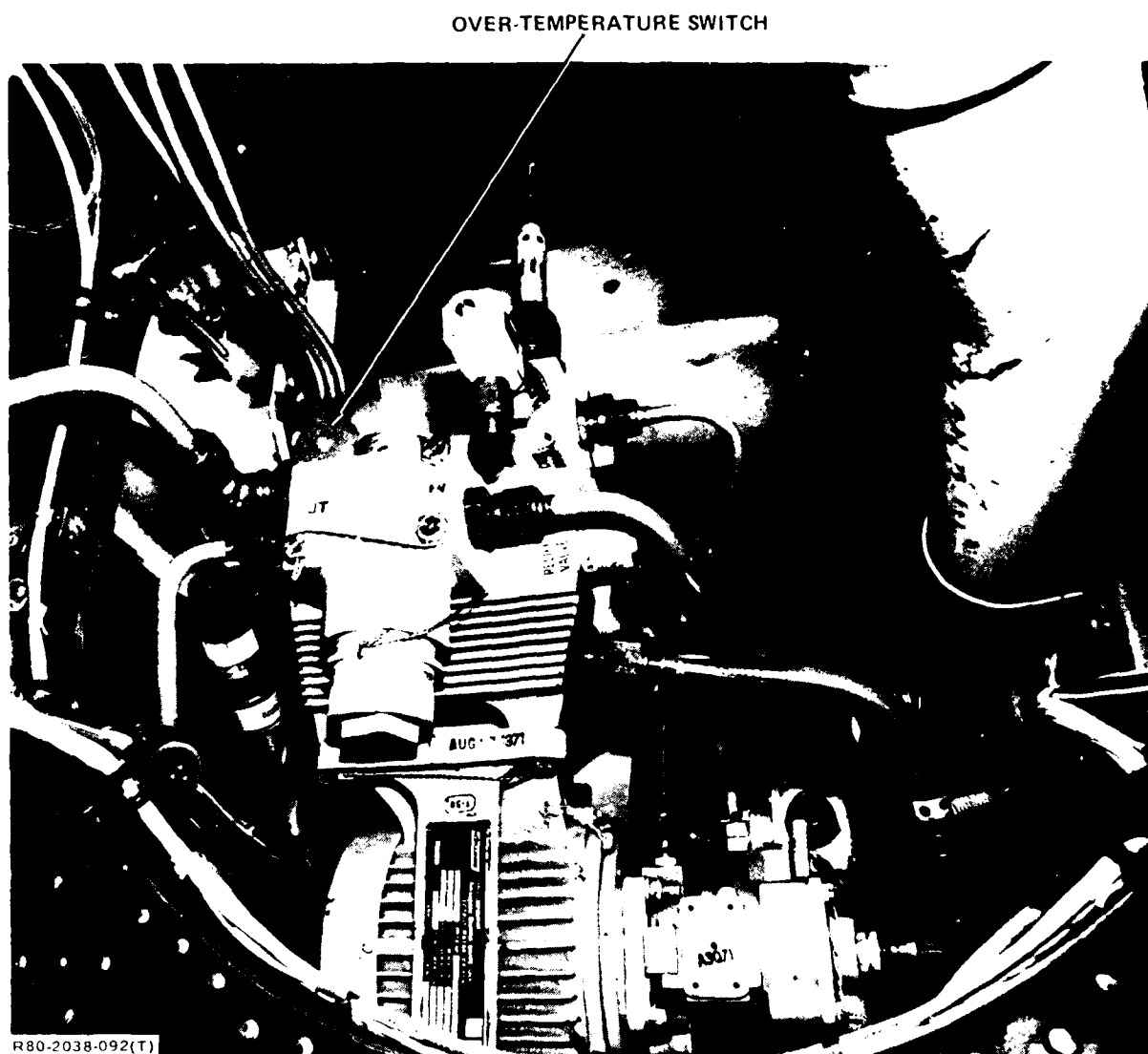


Figure 84. Flight control backup module installation.

Section 2

GROUND AND FLIGHT TESTS

2.1 SYSTEM DEBUGGING

During the early part of 1979 all sensors, hard lines and wiring were installed during vehicle buildup. In mid-May, the vehicle with sensors and HYCOS wiring was subjected to and passed the hydraulic ground check and acceptance testing. These tests verified hydraulic system integrity on both the flight system and the combined system on which HYCOS was installed.

Debugging included rerunning hydraulic reservoir displacement calibration to verify the laboratory values. All HYCOS wiring was checked between the sensor interface and display panel for continuity. A rudder differential displacement check was made after calibrating both potentiometers. Continuity checks were also made on the fiber-optic circuits. After the first flight in October 1979 it was found that the elapsed time meter (ELT) was not functioning. Investigation showed that the ELT operated through a relay after the panel switch was energized. A wiring change was made to the ELT circuit. This enabled the ELT to register every time the combined system was monitored or AC power was available on the aircraft. While the panel was being rewired, an IC chip was also replaced. Details of the wiring change is shown in the appendix.

2.2 DEVELOPMENTAL MODIFICATIONS AND IMPROVEMENTS

2.2.1 HYCOS Display Panel

Modifications were made at the onset of the program to the battery charging circuits to improve NI-CAD battery reliability. During the early phases of the program the NI-CAD batteries discharged when the aircraft was stored in the hangar over the weekend. A HYCOS battery analysis was conducted (See Appendix K) which indicated that the batteries were adequately sized and that the charging rates should be reduced from 100 mA-hr to 50 mA-hr for the 5-volt battery. The charging rates for the 3.6V and - 6V batteries was reduced from 10 mA-hr to 5 mA-hr.

The analysis also indicated that the panel should be equipped with an external accessible connector to provide direct connections to the battery plus and minus terminals. The connector would then allow external monitoring of battery voltages without removing the panel from the vehicle, and it would also provide charging access to the NI-CAD batteries using a dedicated ground support charger.

Both improvements were incorporated. A dedicated battery charger was fabricated but seldom used since, after subsequent initial charging, the ship's electrical buss maintained the batteries in a usable state.

Another improvement area was in modifying the internal power circuit to the elapsed time meter. This was done so that power to the elapsed time meter would occur when both AC and hydraulic system power was available. When the system is interrogated on the ground in the static condition no power reaches the elapsed time meter. In the same circuit, the relay was replaced with a heavy duty Leach DM 2-5.

In order to reduce the number of sequential operations, the system test switch was modified by replacing the ON, center OFF, ON configuration to an ON momentary at the panel. This reduced the system test functions to only 1:

- With the system test switch in its ON position, power is supplied to the elapsed time indicator if hydraulic power is on
- System test "ON 2" without hydraulic power checks air in the reservoir and discrete circuits
- System test "ON 2" with hydraulic power checks the reservoir, ram air turbine accumulator, and rudder differential circuit.

The addition of a top hat to the desiccant color detector terminal improved color transmission visibility at the panel.

2.2.2 Panel Support Structure

During the early part of the program, a doubler plate was added to the access plate to provide additional clearance for the load bearing fasteners. This improvement corrected the fastener retention problem caused by marginal material thickness.

2.2.3 Sensor Light Sources

As the flight test program evolved, it was determined that a more intense light source was needed at the desiccant color detector and pneumatic liquid bottle detection circuits. Three halogen lamps were added with specially designed housings for this purpose. There was a significant improvement in available light intensity.

2.2.4 Flow Sensor Indicators

Environmental vibration during a normal flight schedule caused two of the flow sensors to indicate incorrectly. After investigation and vibration testing, it was found that the resonant frequencies of the lockout solenoid armature/spring occurred. The armature/spring mass was redesigned to move the resonant frequency out of the operational envelope.

2.2.5 Desiccant Color Detector

Several improvements were made to this sensor. These included increasing the light intensity at the surface, optimizing the reflected transmitter, receiver angle, and finally developing a new desiccant color disc mounted internally in the air stream. Color transmission from irregular granular surfaces proved difficult because of the irregular granular surfaces.

Fiber-optic cable junctions should be minimized and cable runs must be carefully laid to avoid sharp bends.

Crazing of the transparent plastic tube developed later in the program. This tube was replaced with another unit of the same type. Examination of the part indicated that crazing was caused by over torquing the sensor body to its outside diameter.

Section 3

PERFORMANCE AND EVALUATION/ASSESSMENT

3.1 PROCEDURES AND METHODS

3.1.1 Objective

The purpose of the Flight Test Program is to evaluate the HYCOS System under actual operating conditions and to determine its effectiveness in detecting system and component malfunctions. It in no way replaces the normal maintenance schedules, but may be used in conjunction with such maintenance actions.

3.1.2 Procedure

This procedure defines a systematic method of conducting a "HYCOS" Interrogation. All data is to be recorded on the provided HYCOS Log Sheet and HYCOS Check-out Logic Sheet.

Three (3) checks are required:

- "A" Preflight static check is conducted with the flight vehicle in the hangar prior to towing to flight line. This provided the initial condition prior to flight. Any abnormalities or malfunctions would be corrected at this time.
- "B" Postflight dynamic check is required to measure internal system and pump leakage with no mechanical input into the control surfaces. During the time the system is pressurized, power is supplied to the elapsed time meter which keeps track of system operational time.
- "C" Postflight static check is conducted after the vehicle was moved to the hangar. This approach was used to detect any changes that may have occurred since the preflight static check.

3.1.3 Log Sheet Description

Using the HYCOS LOG SHEET:

- Enter DATE System is integrated
- Enter FLIGHT NUMBER
- Enter FLIGHT DURATION in hours
- Enter Elapsed Time Meter reading
- Enter CHECK in applicable Flight Interrogation column
- MALFUNCTION - List ANY Hydraulic System Malfunction that occurs on the combined or Flight Hydraulic System
- MAINTENANCE ACTIONS - List any maintenance actions taken on either Combined or Flight Hydraulic Systems.
- Check if malfunction or maintenance action was indicated by or on HYCOS Panel
- Plane Captain/Technician - Write name of plane captain conducting interrogation and technician performing maintenance action.

3.1.4 HYCOS Interrogation Procedure

This sheet is used in conjunction with the Log Sheet but presents more detailed information. The switch positions are broken down into three categories:

- Category "A" designates a pre-flight static check.
- Category "B" designates a post-flight dynamic check (right engine running - no power control input).
- Category "C" designates a post-flight static check.

In conducting the preflight static check, select CIRCUIT TEST ON 1 and hold. Record by code those display lights that do and do not illuminate, in column "A". Release switch.

Select and hold Circuit Test On 2. All red lights should sequence in a sub-block order. Record. This check verifies that the microprocessor timer is functioning. Release switch.

Select and hold Systems Test On 2. Record illuminated lights. This step illuminates those sensors that are out of tolerance and require visual verification. Upon visual verification conduct necessary repair or maintenance action. Record all information in Log Sheets.

3.1.5 HYCOS Display Criteria

- **PUMP (Sub-Category)**
 - PRESS - Illuminates when system pressure drops below approximately 2,200 psi in the combined Hydraulic System. The light extinguishes when the system is pressurized
 - CASE - Illuminates when pump case flow is excessive and may require pump removal. Excessive pump case flow is an indication of a worn or degraded pump
 - FILT - Illuminates when case drain flow filter button pops indicating required maintenance action. After performing maintenance action, reset the visual filter delta "P" button. This rests the electrical circuit
 - TEMP - Illuminates when the pump case drain fluid temperature is excessive (caused by high bypass). This is used in conjunction with pump case flow circuit
- **RESERVOIR (Sub-Category)**
 - LEAK - Illuminates when level drops two inches or more during flight. Also, illuminates if reservoir is not filled to specification
 - AIR - Illuminates if reservoir piston moves greater than one inch from unpressurized to pressurized
 - TEMP - Illuminates if reservoir level temperature is excessive. Indicates possible fault in system and requires additional troubleshooting
 - DRIER - When pale blue desiccant is still serviceable, when color changes to pink or pale pink, replace desiccant cartridge in system and desiccant in sensor

- **FILTER (Sub-Category)**
 - PRESS - Illuminates when pressure filter is clogged and requires replacement. When filter is serviced and indicator button is reset, light will extinguish
 - RET - Illuminates when return filter is clogged and requires replacement. When filter is serviced and indicator button is reset, light will extinguish
- **QUISCENT FLOW (Sub-Category)**
 - SYSTEM - Indicates excessive internal system leakage. This is taken during dynamic check with no control input. Flow sensor must be manually reset after taking corrective action
 - RUDDER - Indicates excessive rudder actuator internal leakage. Also taken during dynamic check with not control input. Flow sensor must be manually reset after taking corrective action. Note: Flow sensors will not indicate properly unless system is pressurized
- **ACCUM PRECHARGE (Sub-Category)**
 - RAT - Indicates low accumulator precharge irrespective of accumulator piston position. If light illuminates with system test "ON 2", service accumulator
- **DIFF DISP (Sub-Category)**
 - RUDDER - Indicates disconnect between push pull rods on and rudder actuator. Combined system must be pressurized. Rudder position follow rudder pedal inputs
- **PNEU PRESS (Sub-Category)**
 - CANOPY - Illuminates when canopy bottle (15 in.³) pressure is low and requires servicing
 - GEAR - Indicates when gear door bottle (30 in.³) pressure is low and requires servicing
- **RELIEF VALVE (Sub-Category)**
 - COMBINED - Indicates when main system relief valve is leaking (failure or improper seating)

- SYSTEM (Sub-Category)

- CIRCUIT TEST ON 1 - Checks discrete circuits to sensors thru common and on leg
- CIRCUIT TEST ON 2 - Checks microprocessor and lights in sub-block sequence
- SYSTEM TEST ON 1 - Programs the microprocessor when system is pressurized
- SYSTEM TEST ON 2 - Interrogates entire combined system (red lights only). When red lights illuminate this indicates a malfunction or requires maintenance action
- ELAPSED TIME METER - Runs when combined system is pressurized.

3.2 OVERALL EVALUATION OF HYCOS SYSTEM

As a preventative maintenance tool, the HYCOS System performed exceedingly well in determining the condition of the system. During the course of its program, it consistently detected:

- Low canopy and door gear dump pressures
- Low reservoir level during initial calibration
- Low system pressure during start up conditions
- Continuous elapsed time on system components.

There were no indications of hydraulic pump excessive case flow or case flow oil temperatures since the sensor limits were not exceeded.

Fiber-optic desiccant color detection proved difficult, even with the addition of more intense light sources. This was attributed to the improper installation of fiber-optic runs in which the bend radius were exceeded, causing excessive light loss. Another area requiring improvement is in optical terminal coupling, where losses can be considerable. Color transmission of red and pink is excellent; however, pale blue is not readily detectable.

The filter subsection gave no indication of tripped delta "p" indicators. This may be due to the fact that the vehicle flew over 150 hours and did not experience any hydraulic subsystem failures. Quiescent and rudder actuator flow sensors, when

interrogated under dynamic conditions, did not indicate excessive flows as originally established. There were, however, developmental problems caused by vibration which were subsequently solved.

The ram air turbine (RAT) accumulator functioned flawlessly with no indication of precharge loss. Pressure, temperature, and displacement sensors functioned as advertised. This component is used as an energy storage device and retains this capability even when the system is shut down.

Except for initial calibration, the differential displacement sensors operated satisfactorily since the rudder output follows the mechanical input. This portion of the circuit is not activated until the combined system is pressurized.

Indications of low pneumatic system pressure worked effectively and repeatedly within limits. Minor system leakage was detected after the vehicle remained in an inactive flight status for several days. Topping the bottles corrected this condition.

Since the relief valve did not malfunction, no indication was apparent on the display. Relief valves are usually passive devices until excessive pressures are exceeded. If this occurs and instability prevails, seat or poppet damage can occur. This results in leakage with subsequent system fluid temperature rise.

The circuit and system test switches functioned satisfactorily, but the system test switch was modified to a continuous ON 1 when the battery charging circuit was modified. Future procedures would eliminate the need for first selecting ON 1 followed by ON 2.

The lay-over time between flights determines the condition of the NI-CAD storage batteries. Although the battery charging circuit is adequate, infrequent ground charges may be necessary. This was readily accomplished by using the ground battery charger through the added electrical panel interface. This connector also provided test points to determine battery condition without removing power from the vehicle.

Section 4

RESTORATION OF THE AIRCRAFT

The flight test program terminated on November 15, 1980 when the aircraft was subjected to a debailment inspection before being turned over to Navy inventory as an updated A-6E. The inspection involved the following activities:

- The following special components were removed from the vehicle:
 - HYCOS Display Panel
 - Quiescent, rudder actuator, and pump case drain flow sensors
 - Pressure, filter, and temperature switches on the combined system pump
- The combined system reservoir was replaced with the original unit kept in storage
- Remote reading delta "P" indicators were replaced with original units
- The ram air turbine accumulator and supporting bracket was replaced with a standard unit.
- Potentiometers located on the turtle deck and rudder were removed in the differential displacement circuit
- Both the pneumatic pressure canopy and emergency gear door pump bottles were replaced with standard units
- The fluid thermal switch was removed downstream of the combined system relief valve
- All wire leads and fiber-optic cables peculiar to the HYCOS system were capped and lagged at both the panel and sensor interface
- The surface temperature switch was removed from the flight control backup module.

The power supply cable (110V 400 ~ AC) from the circuit breaker to the HYCOS panel was disconnected. The HYCOS access cover was permanently attached to the structure in accordance to an EO issued by the Structural Design Group.

After installation of standard production components, lines, and fittings, the vehicle was subjected to a hydraulic ground check to substantiate system integrity in accordance with the ATP. No problems were encountered during this refurbishment.

In addition, an engine ground run was successfully accomplished to verify flight worthiness since the port engine was removed to provide access to the keel where most of the HYCOS sensor components were located.

Section 5

CONCLUSIONS

- The flight test program met all the requirements of the work statement
- The HYCOS accumulated over 150 hours flight time during a 1-year flight test program
- Preflight checkout time takes only 1-1/2 minutes using the HYCOS, as compared to 20 - 30 minutes for a manual checkout
- The HYCOS consistently identified:
 - Low pneumatic bottle pressure
 - Low reservoir level
 - Low system pressure
 - System operating hours
 - Malfunctioned components on a post-flight check
- All other sensors operated normally and did not indicate malfunctions
- The microprocessor functioned flawlessly after final programming and integration. It also has capacity for additional fault-detection via changes in microprocessor programming
- The system is capable of detecting the health or malfunctions of components located in hazardous areas, such as when engines are operating
- The HYCOS did not impair or restrict the normal function or the combined hydraulic system
- HYCOS has demonstrated its capability as a preventative, failure, and maintenance tool
- HYCOS sensors were of the prototype configuration and were not optimized for size or weight

- As a result of the test program, it was found that the system can be further improved by:
 - Relocating the panel away from the inlet duct area
 - Reducing fiber-optic coupling & terminations and optimizing bend radii
 - Utilizing a dedicated disc detector and selecting fiber-optic cable having wider bandwidth to provide more efficient color transmission
- Since prime contractor service and maintenance is excellent, few hydraulic system malfunctions occurred during the test program. In actual squadron use, the benefits of such a system would be realized in:
 - Reduced preflight checkout time
 - Increased availability
 - Reduced turnaround time
 - Extended service intervals
 - Radio component fault indication
 - Utilization of less-skilled personnel
 - Ability to readily check inaccessible components on a preflight basis.

Section 6

RECOMMENDATIONS

- Continue developmental effort on alphanumeric (smart) terminal displays to provide quantitative information on status or malfunction in terms of order of magnitude
- Continue sensor development specifically adapted for lightweight hydraulic system vehicles with continuous monitoring
- Incorporate sensors or make provisions for adaptation/inclusion of sensors in selected components within redundant and dedicated power systems
- Expand the use of fiber-optic circuits in conjunction with digital sensors
- Determine the feasibility of a universal microprocessor display capable of multiple vehicle use
- Incorporate several advanced systems in a training squadron in order to obtain a more representative evaluation (larger statistical sample)
- Update current military component specifications to provide for optional (dedicated) sensors in major flight-critical components.

Section 7

REFERENCES

1. Analog Devices, Norwood, Mass., Technical Data Sheets.
2. The Condensed Chemical Dictionary, 8th Edition, Van Nostrand Zeinhold Company, Pages 223 and 719.
3. NAVAIR 01-85ADA-6-4 Landing Gear Emergency Operational Check.
4. Designing with Dupont "Croron" Fiber Optics (11/76)
5. Machine Design, March 16, 1978, Page 130.
6. NADC TR 75168-30 Final Engineering Report, Phase I, HYCOS (Hydraulic Check Out System), Page 33.
7. Entran Devices, Little Falls, N.J., Technical Data Sheets.
8. Nolan, J.F., "Survey of Electronic Displays," Owens Illinois Technical Center, Toledo, Ohio.
9. Intel MCS-48 Microcomputer Product Description, Pages 23 - 24.
10. Nickel-Cadmium Battery Application - Engineering Handbook, General Electric Company, Pages 4 - 36.
11. Texas Instruments, Attleboro, Mass., Technical Products Literature.

NADC 81073-60

APPENDIX A

HYCOS LOG SHEET FORMAT AND
TYPICAL FLIGHT LOG SHEET

DATE: _____ FLIGHT NO. _____		HYCOS CHECKOUT LOGIC A6E MOD 229 B/N 155628											
REVISION "A"		CIRCUIT TEST						SYSTEM TEST					
SENSOR		SWITCH POSITION						SWITCH POSITION					
		ON1			ON2			ON1			ON2		
		A	B	C	A	B	C	A	B	C	A	B	C
PUMPS													
PRESS. _____													
CASE _____													
FILT _____													
TEMP _____													
RESERVOIR													
LEAK _____													
AIR _____													
LEVEL _____													
TEMP _____													
DRIER _____													
FILTER													
PRESS. _____													
RETURN _____													
QUIESCENT FLO													
SYS _____													
RUDDER _____													
ACCUMULATOR													
RAT _____													
DIFF DISP													
RUDDER _____													
PNEU PRESS													
CANOPY _____													
GEAR _____													
LIQUID _____													
RELIEF VALVE													
COMBINED _____													

NOTES: 1. DRIER LIGHT TRANSMITS COLOR LIGHT BLUE TO PINK
 2. "A" DESIGNATES PREFLIGHT CHECK (STATIC)
 "B" DESIGNATES POSTFLIGHT CHECK (DYNAMIC)
 "C" DESIGNATES POSTFLIGHT CHECK (STATIC)
 3. MARK "X" IN BOX TO INDICATE LIGHT ON.

R80-2038-099(T)

Figure A-1. HYCOS log sheet format used during program.

DATE: <u>08/06/80</u>		HYCOS CHECKOUT LOGIC						FLT TIME					
FLIGHT NO. <u>77</u>		A6E MOD 229 B/N 155628						1.8 HR					
REVISION "A"													
SENSOR		CIRCUIT TEST						SYSTEM TEST					
		SWITCH POSITION						SWITCH POSITION					
		ON1			ON2			ON1			ON2		
		A	B	C	A	B	C	A	B	C	A	B	C
PUMPS													
PRESS. _____													
CASE _____		X	X	X							X		X
FILT _____		X	X	X									
TEMP _____		X	X	X									
RESERVOIR													
LEAK _____		X	X	X									
AIR _____		X	X	X									
LEVEL _____		X	X	X									
TEMP _____		X	X	X									
DRIER _____		X	X	X							O	O	O
FILTER													
PRESS. _____		X	X	X									
RETURN _____		X	X	X									
QUIESCENT FLO													
SYS _____		X	X	X									
RUDDER _____		X	X	X									
ACCUMULATOR													
RAT _____		X	X	X									
DIFF DISP													
RUDDER _____		X	X	X									
PNEU PRESS													
CANOPY _____		X	X	X									
GEAR _____		X	X	X									
LIQUID _____											O	O	O
RELIEF VALVE													
COMBINED _____		X	X	X									
<p>NOTES: 1. DRIER LIGHT TRANSMITS COLOR LIGHT BLUE TO PINK</p> <p>2. "A" DESIGNATES PREFLIGHT CHECK (STATIC)</p> <p>"B" DESIGNATES POSTFLIGHT CHECK (DYNAMIC)</p> <p>"C" DESIGNATES POSTFLIGHT CHECK (STATIC)</p> <p>3. MARK "X" IN BOX TO INDICATE LIGHT ON.</p> <p>ELT PRE-FLT 89.6 HR</p> <p>ELT POST-FLT 91.8 HR</p> <p>R80-2038-099(T)</p>													

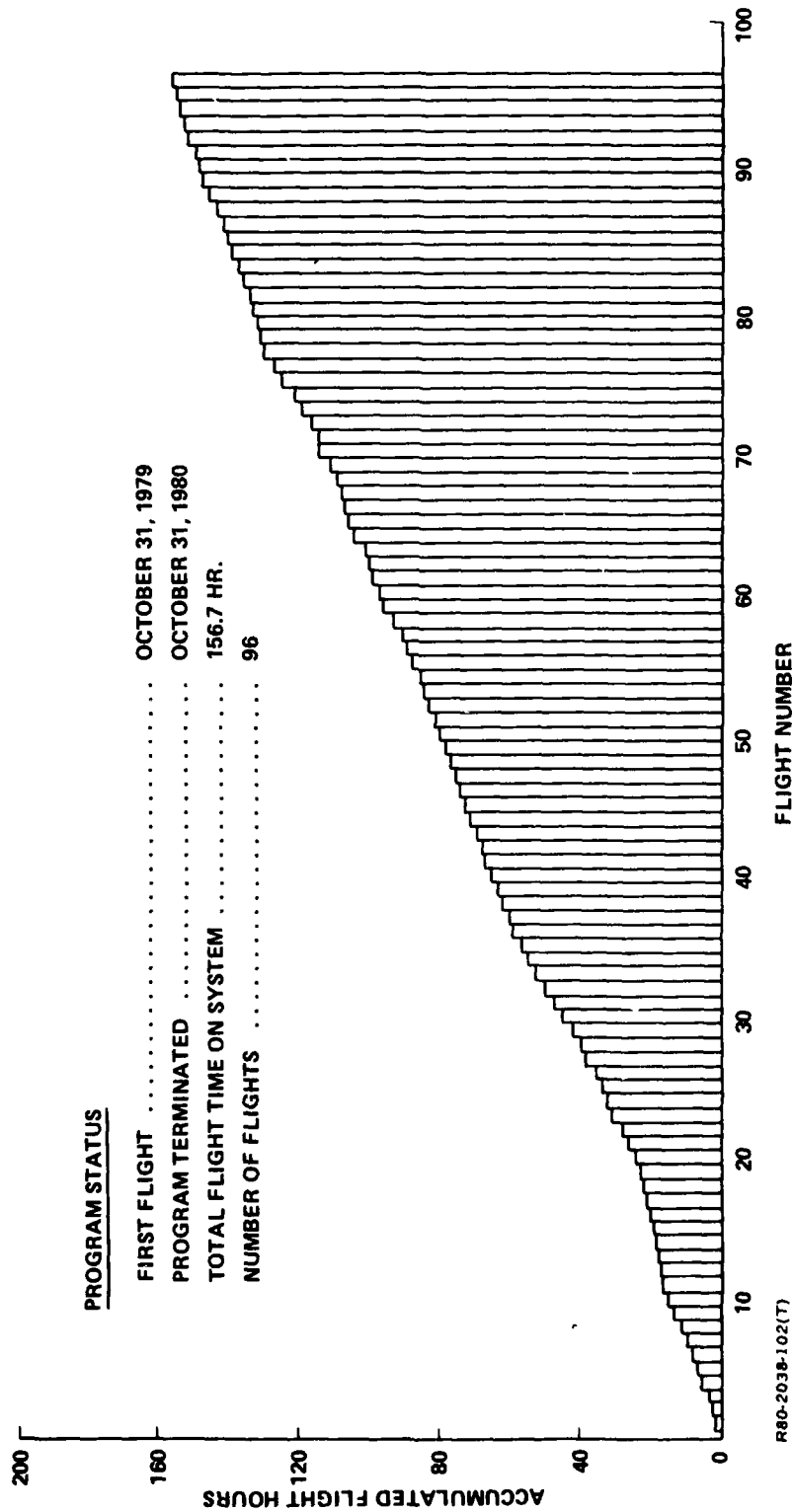
Figure A-2. Typical HYCOS flight log sheet.

NADC 81073-60

APPENDIX B
FLIGHT-HOUR ACCUMULATED LOG

FLIGHT-HOUR ACCUMULATED LOG

SHIP # M229		MODEL A-6E		BUREAU # 155628	
FLT NO.	FLT-HR	ACCUM FLT-HR	FLT NO.	FLT-HR	ACCUM FLT-HR
1	1.5	1.5	49	1.4	79.2
2	.5	2.0	50	1.7	80.9
3	.7	2.7	51	1.7	82.6
4	2.2	4.9	52	1.5	84.1
5	1.5	6.4	53	1.4	85.5
6	1.5	7.9	54	1.1	86.6
7	1.4	9.3	55	2.0	88.6
8	2.0	11.3	56	1.2	89.8
9	2.2	13.5	57	2.5	92.3
10	1.6	15.1	58	2.2	94.5
11	1.3	16.4	59	2.4	96.9
12	1.1	17.5	60	0.8	97.7
13	1.0	18.5	61	2.0	99.7
14	.6	19.1	62	1.0	100.7
15	1.0	20.1	63	1.4	102.1
16	1.0	21.1	64	3.6	105.7
17	.6	21.7	65	1.4	107.1
18	1.6	23.3	66	0.8	107.9
19	.3	23.6	67	0.9	108.8
20	1.3	24.9	68	1.2	110.0
21	2.0	26.9	69	2.4	112.4
22	1.6	28.5	70	2.8	115.2
23	2.3	30.8	71		
24	1.8	32.6	72	2.5	117.7
25	1.7	34.3	73	2.5	120.2
26	2.3	36.6	74	2.3	122.5
27	2.1	38.7	75	3.0	125.5
28	1.5	40.2	76	3.0	128.5
29	2.5	42.7	77	1.8	130.3
30	3.0	45.7	78	1.0	132.3
31	2.4	48.1	79	1.2	132.5
32	2.1	50.2	80	1.3	133.8
33	2.9	53.1	81	1.2	135.0
34	1.9	55.0	82	1.3	136.3
35	2.1	57.1	83	1.9	138.2
36	2.7	59.8	84	1.4	139.6
37	.5	60.3	85	1.1	140.5
38	2.2	62.5	86	1.5	142.2
39	1.2	63.7	87	1.9	144.1
40	2.3	66.0	88	2.0	146.1
41	1.6	67.6	89	2.1	148.2
42	.9	68.5	90	1.0	149.2
43	1.4	69.9	91	1.0	150.2
44	1.8	71.7	92	1.7	151.9
45	1.6	73.3	93	1.6	153.5
46	1.6	74.9	94	0.3	153.8
47*	1.0	75.9	95	1.4	155.2
48	1.9	77.8	96	1.5	156.7
*HYCOS REMOVED FOR REPAIR					
R80 2038-101(T)					



PROGRAM STATUS

FIRST FLIGHT OCTOBER 31, 1979
 PROGRAM TERMINATED OCTOBER 31, 1980
 TOTAL FLIGHT TIME ON SYSTEM 156.7 HR.
 NUMBER OF FLIGHTS 96

APPENDIX C
ABBREVIATED CHRONOLOGICAL LOG

Dec. '77

- Kickoff meeting
- Display panel daylight visibility
- Started specifications

Jan. '78

- Generated specifications for sensor
 - Thermal switch
 - Delta p indicators
 - Flow sensors
 - Pressure switch

Feb. '78

- Continue sensor specification generation
- Start RLS layout defining panel block diagram
- Proceed with panel layout

May '78

- Review flow sensor; develop pressure probes
- Established display panel size and configuration

April '78

- Reservoir sensor development continues
- Mockup model of panel fabrication

May '78

- Installed sensors in F-14 reservoir
- Started A-6 reservoir layout
- Desiccant color detector
- Pressure transducer investigations
- Started installation of F-14 simulator

June '78

- Calibrated F-14 reservoir, issued P/O for A-6 reservoir parts
- Started testing pressure transducers at high and low temperatures
- Flow sensor manufacturing is in progress
- E.E.D. manufactured panel test set

July '78

- Started modification of A-6 reservoir
- Installed panel on F-14A hydraulic simulator

August '78

- Received flow sensors
- Received optical sensors
- Acceptance-tested thermal switches
- Completed F-14 simulator wiring

September '78

- Develop desiccant color detector
- Develop liquid detector
- Started programming microprocessor for F-14 system

October '78

- Completed A-6 reservoir modifications
- A-6 flow sensors at vendors test

Nov. '78

- Ran displacement calibration on A-6 reservoir
- Ran F-14A HYCOS simulator demo

Dec. '78

- Flight-test vehicle tentatively established Mod 229
- Continue sensor development

Jan. '79

- Authorization received from NAVAIR to install HYCOS on Mod 229
- Vehicle is in second stage of buildup
- Issued Engineering Orders for
 - Brackets
 - Lines
 - Component modification
 - Sensor installation in keel area

Feb. '79

- Installation continues on wiring and hardware installation
- Continue sensor development and integration
- Conducted pressure seal tests

March '79

- Start hydraulic hard lines mockup
- Wiring runs for sensor installation begun
- Start sensor installations on port keel

April '79

- All hydraulic hard lines fabricated
- All wiring before sensor and display panel completed
- System pressurized

- Start electrical run line check
- Submitted interim report

May '79

- Completed hydraulic ground check and acceptance testing
- Instrumentation lines with exception of F/O circuit installed
- Vehicle passed through paint shop
- Vehicle ground run tested

June '79

- Vehicle delayed 5 weeks due to structural bulkhead repairs
- Continue fiber-optic color detection development; investigate halogen lamp

20 June '79

- Investigate halogen lamps
- Added resistor to reduce voltage from 5 VDC to 3.5 VDC

30 July '79

- Ordered incandescent lamps
- Started interface and ground checkout on bailed A/C

August '79

- Structural mods made to vehicle to accept panel
- Started debugging system

Sept. '79

- Started rudder differential displacement calibration
- Reservoir calibration information supplied to E.E.D. for burn-in

Oct. '79

- Calibration rudder differential displacement
- Run circuit check using panel jumper
- Flew A/C for 1-1/2 hr
- ELT not operational

Nov. '79

- Removed panel
- Replaced I/C chip for ELT problem
- NICAD batteries nearly discharged. Changed battery charging rate from 0.100 A to 0.200 - 0.300 A

Dec. '79

- Rudder and quiescent flow sensor found tripped after flight
- Modified optical viewing port at panel terminal
- Conducted lab tests on halogen lamp; 20 to 1 improvement verified
- Received solenoid rework to negate armature resonance on flow sensors

Jan. '80

- Reduced NICAD battery charging rate (50 MAH for 5 V batteries and 5 MAH for +3.6 and 6 V batteries)
- Added regulated power supply to ELT circuit
- Modified system test switch from 2 momentary ON (ON center of ON) to ON - ON (ON momentary ON)
- Added battery test plug on panel face for external charging and battery checking
- Reprogrammed M/P to eliminate erroneous over temp light (Rev. 18, Jan. 80)
- EO 128FT80001 installs improved light source on reservoir pressurization circuit
- 128FT80002 installs wiring to light sources
- 128FT80003 changes flow sensor locking solenoids
- 128FT80005 supplies BATT power instead of transformer power to both light sources
- Conducted resonance vibration test on flow sensors - 18-25 Hz resonance occurred. Made improvements. Modified solenoid has no resonance points at 5-2000 Hz @ 5, 10, 15 G ranges

Feb. '80

- High intensity of F/O pneumatic circuit improved at display panel
- Color intensity transmission requires additional development

- External battery charger completed at Plant 14
- ELT stops functioning - suspected relay
- Generated EO 128FT80006 which installs second high-intensity light at pneumatic bottle test circuit
- Issued EO 128B1636 to add spacer on access door

March '80

- Dessicant sensor approach using internal fiber investigation not successful
- Fabricated third high-intensity source for pneumatic bottle circuit; EO 128FT80006 will install unit in vehicle
- Procured high-capacity ELT relay

April '80

- Developed new dessicant sensor (cobalt chloride/potassium bromide disc)
- Installed access door spacer

May '80

- Improved optical dessicant sensor with plastic spacer for isolation due to chemical reaction

June '80

- Added short fiber cable link between modified dessicant optic receiver and junction
- Increased light loss

July '80

- Detected poor F/O cable runs with 32 dbm losses instead of 10 dbm, which might be expected
- Investigate F/O improvements

August '80

- Continue flight test program

Sept. '80

- Continue system interrogation and assessment

Oct. '80

- Continue system flight test and assessment

Nov. '80

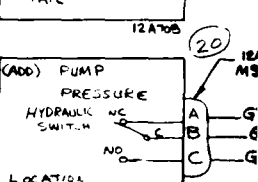
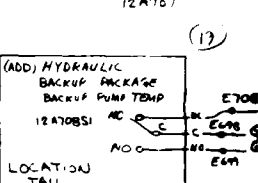
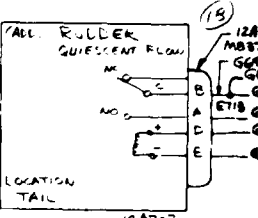
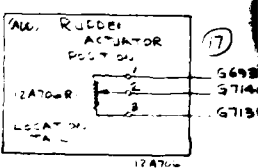
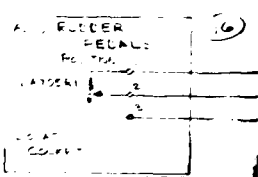
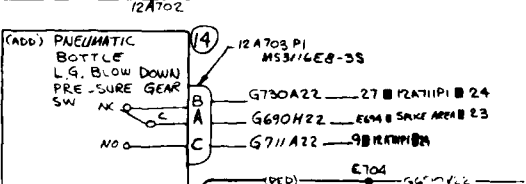
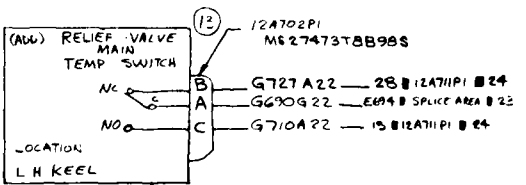
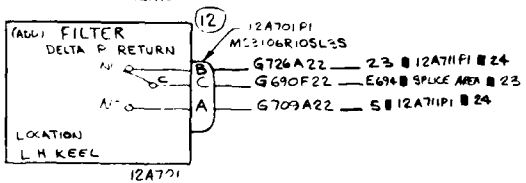
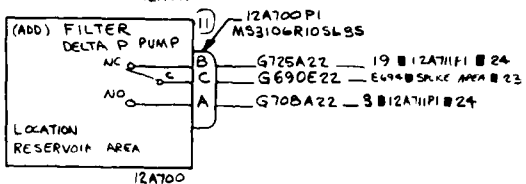
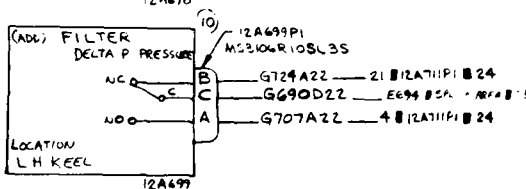
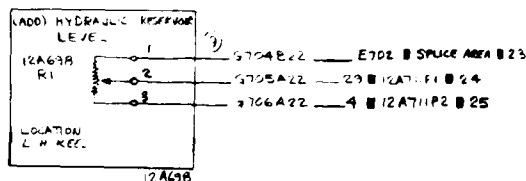
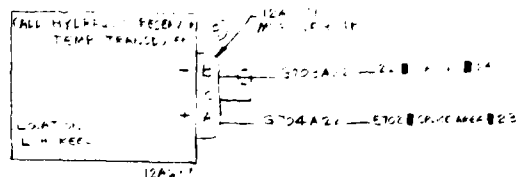
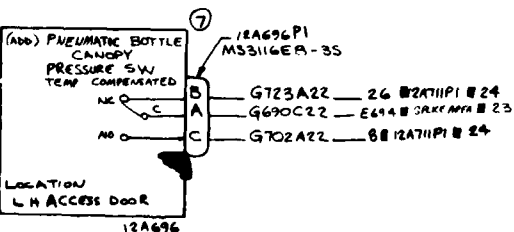
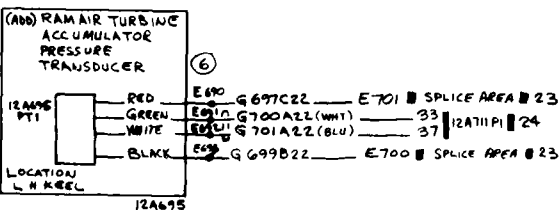
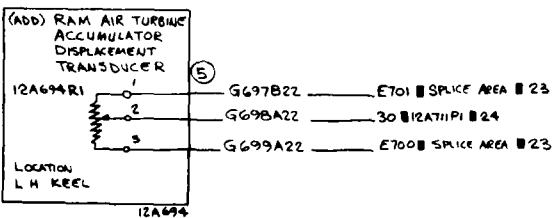
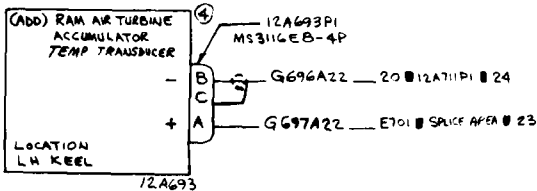
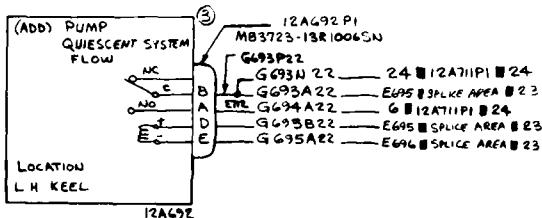
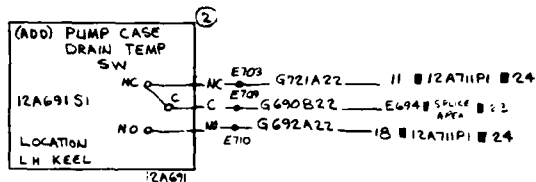
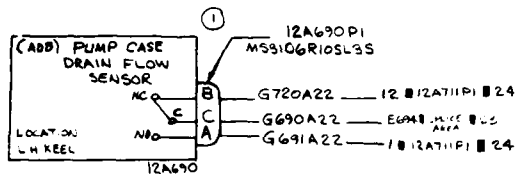
- Issue system debailment EO for HYCOS

Dec. '80

- Return test vehicle to U.S. Navy
- Complete final report

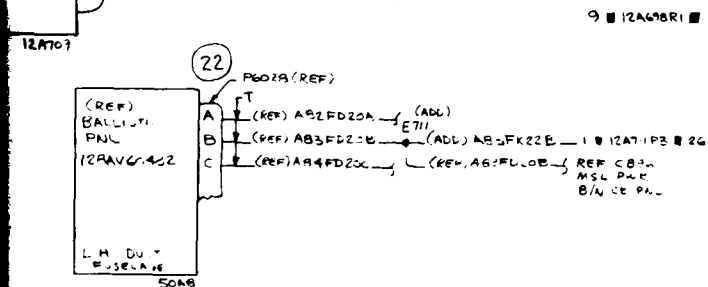
NADC 81073-60

APPENDIX D
HYCOS WIRING DIAGRAM



(REF) BALLISTIC PNL 12PAV601

L.H. DOW FUSERS



(24) 12A711P1
MB1511/56FD0153

(ADD) DISPLAY PANEL		
11 12A700P1 B	G725A22	19 FILTER DELTA P PUMP
1 12A690P1 B	G720A22	12 PUMP CASE DRAIN FLOW
2 12A691S1 E705	G721A22	11 PUMP CASE DRAIN TEMP
19 12A708S1 E708	G729A22	10 BACKUP PUMP TEMP
10 12A699P1 B	G724A22	21 FILTER DELTA P PRESSURE
12 12A701P1 B	G726A22	23 FILTER DELTA P RETURN
7 12A696P1 B	G723A22	26 PNEUMATIC BOTTLE CANOPY PRESSURE
14 12A703P1 B	G730A22	27 PNEUMATIC BOTTLE LG BLOW DOWN PRESSURE
13 12A702P1 B	G727A22	28 RELIEF VALVE MAIN TEMP
1 12A693P1 A	G691A22	1 PUMP CASE DRAIN FLOW
11 12A700P1 A	G708A22	3 FILTER DELTA P PUMP
2 12A691S1 E710	G692A22	18 PUMP CASE DRAIN TEMP
19 12A708S1 E699	G716A22	16 BACKUP PUMP TEMP
10 12A699P1 A	G707A22	4 FILTER DELTA P PRESSURE
12 12A701P1 A	G709A22	5 FILTER DELTA P RETURN
7 12A696P1 C	G702A22	8 PNEUMATIC BOTTLE CANOPY PRESSURE
14 12A703P1 C	G711A22	9 PNEUMATIC BOTTLE LG BLOW DOWN PRESSURE
13 12A702P1 C	G710A22	13 RELIEF VALVE MAIN TEMP
3 12A692P1 E712	G693N 22	17 PUMP PRESSURE
18 12A707P1 E713	G693Q 22	24 PUMP QUIESCENT SYSTEM FLOW
20 12A709P1 A	G717A 22	25 RUDDER QUIESCENT FLOW
3 12A697P1 A	G694A22	2 PUMP PRESSURE HYDRAULIC SWITCH
18 12A701P1 A	G713A22	4 PUMP QUIESCENT SYSTEM FLOW
17 12A709P1 2	G714A22	7 RUDDER QUIESCENT FLOW
16 12A708P1 2	G712B22	34 RUDDER ACTUATOR POSITION
8 12A697P1 B	G703A22	35 RUDDER PEDALS POSITION
9 12A698P1 2	G705A22	22 RESERVOIR TEMP
4 12A695P1 B	G696A22	15 RESERVOIR LEVEL
5 12A694P1 2	G698A22	29 RAM AIR TURBINE ACCUMULATOR TEMP
6 12A695P1 E691	G700A22 (SWITCH)	30 RAM AIR TURBINE ACCUMULATOR DISPLACEMENT
23 12A701P1 E700	G701A22 (BLW)	33 RAM AIR TURBINE ACCUMULATOR PRESSURE
20 12A701P1 C	G699C22	37 RAM AIR TURBINE ACCUMULATOR PRESSURE
	G713A22	36 PUMP PRESSURE HYDRAULIC SWITCH

(25) 12A711P2
MB1511/46FB0151

23 12A695P1 E694	G690U22	10 TO + T1
23 12A695P1 E695	G693M22	6 + SV SW
23 12A695P1 E696	G695C22	5 GRD
23 12A695P1 E697	G713D22	1 GRD
23 12A695P1 E700	G699D22	8 GRD
23 12A695P1 E701	G697D22	7 + SV
23 12A695P1 E702	G704C22	3 + SV
9 12A698P1 3	G706A22	4 GRD

(26) 12A711P3
MB1511/46FA0151

22 12A602B E711	AB3FK22B	1 115VAC 400HZ PH B PRIMARY
	G719A22N	2 GRD

LOCATION
L H BOARDING LADDER

12A711

APPENDIX E
PARTICIPATING FIRMS

Aircraft Porous Media	Glen Cove, N.Y.
Walter Kidde & Company	Belleville, N.J.
Valtec	West Boyleston, Mass.
Sigma-Netics	Mountain Lakes, N.J.
Sprague Engineering Corporation	Gardena, California
Bourns Incorporated	Riverside, California
Neo-Dyn Inc.	Chatsworth, California
De Laval Special Products Division	Cleveland, Ohio
Entran Devices	Norwood, Massachusetts
Frisby Airborne Hydraulics	Freeport, N.Y.
E.I. du Pont de Nemours	Wilmington, Delaware
Intel Corporation	Santa Clara, California
Texas Instruments	Attleboro, Mass.
Hunter Spring Division of Ametek	Hatfield, PA
Russel Associates	Bay Shore, N.Y.
Eagle Technology	Arlington, Virginia
Kulite Semiconductor Products	Ridgefield, N.J.
Sealectro Corporation	Mamaroneck, N.Y.
Ultra Sensors	Minneapolis, Minnesota
Resistoflex Corporation	Vineland, N.J.
Analog Devices	Norwood, MA
Photodyne Incorporated	West Lake Village, CA
Polaroid Corporation	Cambridge, MA
Roylan Optics Company	Arcaria, CA

NADC 81073-60

APPENDIX F

ESTIMATED WEIGHT OF PROTOTYPE
FULL-BLOWN SYSTEM

ITEM	DESCRIPTION	COMBINED	FLIGHT
1	DISPLAY PANEL	6.00	—
2	RESERVOIR		
	• PISTON DISPLACEMENT — POTENTIOMETER — BRACKETS, ADAPTORS, & HOUSING	0.08 2.38	0.08 2.38
	• TEMPERATURE TRANSDUCER	0.12	0.12
3	FILTER DIFFERENTIAL PRESSURE		
	• INDICATORS	0.57 (6)	0.57 (5)
	• MULTICATORS	0.36 (1)	0.36 (1)
4	PRESSURE SWITCH		
	• TEMPERATURE COMPENSATED	0.25 (5)	—
5	FLOW SENSORS		
	• QUIESCENT	1.39	1.39
	• RUDDER ACTUATOR	0.57	—
	• PUMP CASE	0.52	0.52
6	PRESSURE SWITCH SYSTEM	0.09	0.09
7	TEMPERATURE SWITCH		
	• CASE DRAIN FILTER MODULE (R.V.)	0.13 (2)	0.13 (2)
	• FLIGHT CONTROL BACKUP MODULE, TEMPERATURE SWITCH		—
8	POTENTIOMETER ROTARY		
	• RUDDER PEDALS	0.08	—
	• RUDDER ACTUATOR	0.08	—
9	TRANSDUCER, PRESSURE	0.18 (3)	0.18
10	TRANSDUCER, TEMPERATURE	0.12 (3)	0.12
11	WIRING, CLAMPS & CONNECTORS, BRACKETS	3.00	3.00
12	DETECTOR, LIQUID	0.03 (5)	—
		20.78	11.35
		TOTAL: 32.13	

R80-2036-096(T)

APPENDIX G
ENGINEERING ORDERS

NUMBER	TITLE
128FT80001A	Sensor, Optical Desiccant
128FT80002A	Installation Dwg, Fuselage
128FT80003A	Flow Sensor, Bypass Type
128FT80005A	Installation Dwg, Fuselage
128FT80006	Installation Dwg, Fuselage
128FT80007	Sensor, Optical Desiccant
128FT81003	Hycos, Removal
128EL10401AFZ	Lines Installation, Fuselage
128EL10401AF3	Lines Installation, Fuselage
128EL10401 -	Lines Installation, Fuselage
128EL4118T4	Lines Installation, Fuselage
128EL4222 -	Lines Installation, Fuselage
128EL10403T4	Lines Installation, Fuselage
128EL10403T5	Lines Installation, Fuselage
128EL66010L4	Lines Installation, Fuselage
128EL66013M1	Lines Installation, Fuselage
128EL66021L2	Lines Installation, Fuselage
128EL66041K5	Lines Installation, Fuselage
128EL66047M2	Lines Installation, Fuselage
128EL66053K5	Lines Installation, Fuselage
128EL66058F2	Lines Installation, Fuselage
128EL66060L4	Lines Installation, Fuselage
128AB60012	Exterior Markings
128AV66014U5	Installation Drawing, Fuselage
128AV66014V2	Installation Drawing, Fuselage
128B11380AB1	Duct Assembly, Fuselage
128C130001P1	Controls Installation, Directional

NADC 81073-60

NUMBER	TITLE
128CS10000 -	Potentiometer Installation, Rudder
128CS10000W1	Potentiometer Installation, Rudder
128H10009V1	Components Installation
128H10009V2	Components Installation
128H10009V3	Components Installation
128H10049J1	Components Installation
128H10127F1	Reservoir Installation
128H10127F2	Reservoir Installation
128H10136N1	Regulator Installation
128H10136N2	Regulator Installation
128H10312G1	Installation, Components
128H10009W2	Components Installation

[illegible]

[illegible]

GRUMMAN AEROSPACE CORPORATION						CODE BODY 26512	E0	175 FT 80002	DASH NO.	PV A
									SER NO.	
									MFG PART NO.	
									E0 CONT NO.	SN NO Z

FLIGHT TEST E.O. - NOT TO BE
INCORPORATED ON DRAWINGS REMOVE
FROM AIRCRAFT PRIOR TO 19 MAY 80

REV	DESCRIPTION	CTD	ENDS	RUST
A	EXTEND TO 9-19-80	OAS 4-19-80	N/A	4-19-80 4-19-80

OAC 1044
 1072 (PART B)

**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER**

GRUMMAN AEROSPACE CORPORATION											
WFG PART NO		WCO REV		ACD		ECP		SEQ NO		CONFIDENTIAL	
								26512		EO	
PLT/DEPT		OPERATIONS		INSP		PLT/DEPT		INSP		END ITEM NO	
										ACTY NO	
										CONFIG REQ D CONFIG NOT REQ D	
										REPLACES PART NO	
										SH / OF	
										2	
CONTRACT NO N62269-78C-0041											
DWS TITLE INSTALLATION DWG FUSELAGE											
ACTION		QTY WA		QTY EI		PART NUMBER		NOTE		NEXT ASSEMBLY DWG	
										SD EFF	
										1 2/4/11 TA 79-143 AGE	
										M229	

FLIGHT TEST INFO:

NOT TO BE INCORPORATED ON DRAWING

TO BE REMOVED AT TIME OF HYDROS

REMOVAL PRIOR TO MAY 1980 OR

AS EXTENDED BY REVISION TO THIS

EO "

SERVICE AREA CHANGES

(NOT ONLY, NOT TO BE INCORPORATED ON DWG.)

DATE	REMOVE	WIRE #	CONNECT	WIRE #
E694	G697E22			
E694	G690Y22			
E696	G695A22			G750E22
E696	G695B22			
E697	G695A22			G695A22
E697	G695B22			G695B22
E700	G699E22			G697E22
E701	G750E22			
E702	G699E22			G699E22
E702	G690Y22			G690Y22

REV	DESCRIPTION	STD	ENG	CU	T
A	EXTERNAL TO 51 SD	44-480	N/A	40	40-480

ACTION		PART NUMBER		NOTE		NON-INCULCATURE		COMMERCIAL SPECIFICATION		MATERIAL SPECIFICATION		PROC		FIN		ZONE	
								CODE IDENT - COM PART NO									
REASON FOR CHANGE																	
TO SUPPLY BATTERY POWER TO HALOGEN LAMPS INSTEAD OF TRANSFORMER - CHARGED POWER																	
APPROVED BY		GROUP LDR		SUPPORT		RELIABILITY		STRESS		PROD ENG		PROD ENG		RELEASE		CUSTOMER	
SIGNATURE		DATE		DATE		DATE		DATE		DATE		DATE		DATE		DATE	
SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER		SECTION FLUID POWER	
PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357		PLANT GROUP 357/357	
DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80		DATE EXT 2-1-80	

ENGINEERING ORDER /
MANUFACTURING CHANGE ORDER

SPALICE AREA 1 23	
---	G699E22 --- E700
---	G697E22 --- E694
---	G750E22 --- E701

(15) — G690Y22 — E694 1 SPICE AREA 1 23
WAS

(23)

SOURCE AREA

REMOVE

6697E22 --- E694 --- 6690V22 --- 6690U22 ---

6695A22 --- REMOVED --- G750E22 --- ADD ---

6695B22 --- ADD --- 6695C22 ---

G73A22 --- E697 --- 373D22 ---

G73B22 --- 6698C22 ---

6699A22 --- F700 --- 6699D22 ---

6699B22 --- 6699E22 ---

6697E22 --- ADD --- 6699F22 ---

6697A22 --- F701 --- 6697D22 ---

6697B22 --- 6697C22 ---

G704A22 --- F702 --- G704C22 ---

G704B22 --- 6699G22 --- 6690J22 ---

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

GRUMMAN AEROSPACE CORPORATION										REV
MFG PART NO		ECO REV		ECO NO		CODE IDENT		DASH NO		REV
		ACD		ECP		25512		128FT 80007		
PLT/DEPT		OPERATIONS		INSP		PLT/DEPT		CHG CL		QTY/EI
CONTRACT NO		N62-69-78C-0041								
DUNS TITLE		SENSOR, OPTICAL DESICCANT								
ACTION		QTY/HA	QTY/EI	PART NUMBER	NOTE	REASSEMBLY DNG	SD EFF	EST	AUTHORITY	END ITEM
									1 2141:TK 19-43	M 229
		<p>FLIGHT TEST INFO:</p> <p>NOT TO BE INCORPORATED ON DRAWING</p> <p>TO BE REMOVED AT TIME</p> <p>OF HYDROS REMOVAL PRIOR TO</p> <p>SEPTEMBER 1980 OR AS EXTENDED</p> <p>BY REVISION TO THIS E.O.</p>								
REASON FOR CHANGE		<p>TO USE NEW IMPROVED MOISTURE DETECTOR</p> <p>INITIAL DETECTOR HAD INSUFFICIENT COLOR</p> <p>INTENSITY</p>								
APPROVED BY		SIGNATURE		DATE		RELIABILITY		STRESS		PROD ENGINE
PREPARED BY		JONN DUECH		6/9/80		6/9/80		6/9/80		6/9/80
SECTION		FLUID POWER		35-357		35-357		35-357		35-357
PLANT GROUP		35-357		35-357		35-357		35-357		35-357
DATE		6/9/80		6/9/80		6/9/80		6/9/80		6/9/80
EXT		6/9/80		6/9/80		6/9/80		6/9/80		6/9/80
QTY PER ASSY		1		1		1		1		1
PART NUMBER		-901		-901		-901		-901		-901
COMMERCIAL SPECIFICATION		CODE IDENT - COM PART NO		NOTE		NOMENCLATURE		MATERIAL SPECIFICATION		PROD FTR
ZONE		A		D		D		D		D
REASON FOR CHANGE		NOTED								
APPROVED BY		SIGNATURE		DATE		RELIABILITY		STRESS		PROD ENGINE
PREPARED BY		JONN DUECH		6/9/80		6/9/80		6/9/80		6/9/80
SECTION		FLUID POWER		35-357		35-357		35-357		35-357
PLANT GROUP		35-357		35-357		35-357		35-357		35-357
DATE		6/9/80		6/9/80		6/9/80		6/9/80		6/9/80
EXT		6/9/80		6/9/80		6/9/80		6/9/80		6/9/80
QTY PER ASSY		1		1		1		1		1
PART NUMBER		-901		-901		-901		-901		-901
COMMERCIAL SPECIFICATION		CODE IDENT - COM PART NO		NOTE		NOMENCLATURE		MATERIAL SPECIFICATION		PROD FTR
ZONE		A		D		D		D		D

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

**ENGINEERING ORDER,
MANUFACTURING CHANGE ORDER**

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

[illegible]

ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

GRUMMAN AEROSPACE CORPORATION										CONTRACT NO.	EO	REV.														
										26512		128EL10401														
										EO CONTRACT NO.		128EL4710														
										REV.		2														
ACTION	QTY	MA	QTY	ET	PART NUMBER	NOTE	TEST ASSEMBLY DWG	SD	ET	EE	AUTHORITY	MODEL	END ITEM	GAC UNIT NO.												
											128EL10401-901P-6	M229														
THIS IS A RECORD E.D.																										
128H10014-995P-6 REPLACES 128EL10401-901P-6																										
					-1703P-6						-903P-6															
					-2277P-12						-905P-12															
					-2125P-6						-906P-6															
					-2360P-6						-908P-6															
					-2315P-12						-911P-12															
					-1776P-4						-912P-4															
					-2367P-4						-913P-4															
					-994P-4						-914P-4															
128H10014-1626P-6 REPLACES 128EL10401-915P-6																										
ADD					128H10014-994P-4						TUBE ASSY			A 5 1												
					-2376P-4									A 5 1												
					-1776P-4									A 5 1												
					-1776P-4									A 5 1												
					-2388P-12									A 5 1												
					-2360P-6									A 5 1												
					-2125P-6									A 5 1												
					-2277P-12									A 5 1												
					-1626P-6									A 5 1												
					-1703P-6									A 5 1												
					-2388P-4									A 5 1												
ADD					128H10014-994P-4						TUBE ASSY			A 5 1												
					-1						LINES INSTL			A 5 1												
ACTION	QTY	PER	ASSY		PART NUMBER						NOTE	COMMERCIAL SPECIFICATION CODE IDENT.	MATERIAL SPECIFICATION	PROC	FIN	ZONE	1	2	3	4	5	6	7	8	9	10

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

GRUMMAN AEROSPACE CORPORATION									
THIS IS A RECORD E.D.									
128H10014-995P-6 REPLACES 128EL10401-901P-6									
128H10014-1626P-6 REPLACES 128EL10401-915P-6									

GRUMMAN AEROSPACE CORPORATION		SKETCH NO. 26512	EO	128EL10403	DATE-N	128EL4711	
W.P. H. N.	OPERATIONS	ECOP	RECEIVED	RECEIVED	RECEIVED	RECEIVED	
PT. DESK	OPERATIONS	RECEIVED	RECEIVED	RECEIVED	RECEIVED	RECEIVED	
CONTRACT NO. N62289-78-C-0041		DOW DATE		DOW DATE		DOW DATE	
ACTION		ACTION		ACTION		ACTION	
REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE	
DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION	
PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC	
SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165	
PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40	
DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78	
QTY PER ASSY		QTY PER ASSY		QTY PER ASSY		QTY PER ASSY	
PART NUMBER		PART NUMBER		PART NUMBER		PART NUMBER	
NOMENCLATURE		NOMENCLATURE		NOMENCLATURE		NOMENCLATURE	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
LINES INSTL		LINES INSTL		LINES INSTL		LINES INSTL	
COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION	
CODE IDENT		CODE IDENT		CODE IDENT		CODE IDENT	
DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE	
CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6	
REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE	
DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION	
PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC	
SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165	
PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40	
DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78	
QTY PER ASSY		QTY PER ASSY		QTY PER ASSY		QTY PER ASSY	
PART NUMBER		PART NUMBER		PART NUMBER		PART NUMBER	
NOMENCLATURE		NOMENCLATURE		NOMENCLATURE		NOMENCLATURE	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
LINES INSTL		LINES INSTL		LINES INSTL		LINES INSTL	
COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION	
CODE IDENT		CODE IDENT		CODE IDENT		CODE IDENT	
DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE	
CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6	
REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE	
DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION	
PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC		PREPARED BY: BOBAC	
SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165		SECTION: E/M-1165	
PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40		PLANT GROUP: 40	
DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78		DATE: 12-27-78	
QTY PER ASSY		QTY PER ASSY		QTY PER ASSY		QTY PER ASSY	
PART NUMBER		PART NUMBER		PART NUMBER		PART NUMBER	
NOMENCLATURE		NOMENCLATURE		NOMENCLATURE		NOMENCLATURE	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
TUBE ASSY		TUBE ASSY		TUBE ASSY		TUBE ASSY	
LINES INSTL		LINES INSTL		LINES INSTL		LINES INSTL	
COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION		COMMERCIAL SPECIFICATION	
CODE IDENT		CODE IDENT		CODE IDENT		CODE IDENT	
DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE		DESCRIPTION OF CHANGE	
CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6		CHANGED 128EL10403-223-1-6	
REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE		REASON FOR CHANGE	
DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION		DE-BOILED AIR ENH TO IMPROVE THERMAL PROTECTION	

[illegible]

[illegible]

[illegible]

**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT**

GRUHMANN AEROSPACE CORPORATION

CODE IDENT 26512 **EO** **128EL66023**

DASH NO **REV** **M7**

SER NO **ED CONT NO** **128EL4116**

128 NO **12**

VIEW LKG INBD
L.H. KEEL

COMPONENTS AND PARTS:

- ACCUMULATOR
- PNEU RESER VOIR
- COMB SYS PRES FILTER
- COMB SYS RET FILTER
- PI02 REF
- PI03 REF
- PI04 REF
- PI05 REF
- PI06 REF
- PI07 REF
- PI08 REF
- PI09 REF
- PI10 REF
- PI11 REF
- PI12 REF
- PI13 REF
- PI14 REF
- PI15 REF
- PI16 REF
- PI17 REF
- PI18 REF
- PI19 REF
- PI20 REF
- PI21 REF
- PI22 REF
- PI23 REF
- PI24 REF
- PI25 REF
- PI26 REF
- PI27 REF
- PI28 REF
- PI29 REF
- PI30 REF
- PI31 REF
- PI32 REF
- PI33 REF
- PI34 REF
- PI35 REF
- PI36 REF
- PI37 REF
- PI38 REF
- PI39 REF
- PI40 REF
- PI41 REF
- PI42 REF
- PI43 REF
- PI44 REF
- PI45 REF
- PI46 REF
- PI47 REF
- PI48 REF
- PI49 REF
- PI50 REF
- PI51 REF
- PI52 REF
- PI53 REF
- PI54 REF
- PI55 REF
- PI56 REF
- PI57 REF
- PI58 REF
- PI59 REF
- PI60 REF
- PI61 REF
- PI62 REF
- PI63 REF
- PI64 REF
- PI65 REF
- PI66 REF
- PI67 REF
- PI68 REF
- PI69 REF
- PI70 REF
- PI71 REF
- PI72 REF
- PI73 REF
- PI74 REF
- PI75 REF
- PI76 REF
- PI77 REF
- PI78 REF
- PI79 REF
- PI80 REF
- PI81 REF
- PI82 REF
- PI83 REF
- PI84 REF
- PI85 REF
- PI86 REF
- PI87 REF
- PI88 REF
- PI89 REF
- PI90 REF
- PI91 REF
- PI92 REF
- PI93 REF
- PI94 REF
- PI95 REF
- PI96 REF
- PI97 REF
- PI98 REF
- PI99 REF
- PI00 REF
- PI01 REF
- PI02 REF
- PI03 REF
- PI04 REF
- PI05 REF
- PI06 REF
- PI07 REF
- PI08 REF
- PI09 REF
- PI10 REF
- PI11 REF
- PI12 REF
- PI13 REF
- PI14 REF
- PI15 REF
- PI16 REF
- PI17 REF
- PI18 REF
- PI19 REF
- PI20 REF
- PI21 REF
- PI22 REF
- PI23 REF
- PI24 REF
- PI25 REF
- PI26 REF
- PI27 REF
- PI28 REF
- PI29 REF
- PI30 REF
- PI31 REF
- PI32 REF
- PI33 REF
- PI34 REF
- PI35 REF
- PI36 REF
- PI37 REF
- PI38 REF
- PI39 REF
- PI40 REF
- PI41 REF
- PI42 REF
- PI43 REF
- PI44 REF
- PI45 REF
- PI46 REF
- PI47 REF
- PI48 REF
- PI49 REF
- PI50 REF
- PI51 REF
- PI52 REF
- PI53 REF
- PI54 REF
- PI55 REF
- PI56 REF
- PI57 REF
- PI58 REF
- PI59 REF
- PI60 REF
- PI61 REF
- PI62 REF
- PI63 REF
- PI64 REF
- PI65 REF
- PI66 REF
- PI67 REF
- PI68 REF
- PI69 REF
- PI70 REF
- PI71 REF
- PI72 REF
- PI73 REF
- PI74 REF
- PI75 REF
- PI76 REF
- PI77 REF
- PI78 REF
- PI79 REF
- PI80 REF
- PI81 REF
- PI82 REF
- PI83 REF
- PI84 REF
- PI85 REF
- PI86 REF
- PI87 REF
- PI88 REF
- PI89 REF
- PI90 REF
- PI91 REF
- PI92 REF
- PI93 REF
- PI94 REF
- PI95 REF
- PI96 REF
- PI97 REF
- PI98 REF
- PI99 REF
- PI00 REF
- PI01 REF
- PI02 REF
- PI03 REF
- PI04 REF
- PI05 REF
- PI06 REF
- PI07 REF
- PI08 REF
- PI09 REF
- PI10 REF
- PI11 REF
- PI12 REF
- PI13 REF
- PI14 REF
- PI15 REF
- PI16 REF
- PI17 REF
- PI18 REF
- PI19 REF
- PI20 REF
- PI21 REF
- PI22 REF
- PI23 REF
- PI24 REF
- PI25 REF
- PI26 REF
- PI27 REF
- PI28 REF
- PI29 REF
- PI30 REF
- PI31 REF
- PI32 REF
- PI33 REF
- PI34 REF
- PI35 REF
- PI36 REF
- PI37 REF
- PI38 REF
- PI39 REF
- PI40 REF
- PI41 REF
- PI42 REF
- PI43 REF
- PI44 REF
- PI45 REF
- PI46 REF
- PI47 REF
- PI48 REF
- PI49 REF
- PI50 REF
- PI51 REF
- PI52 REF
- PI53 REF
- PI54 REF
- PI55 REF
- PI56 REF
- PI57 REF
- PI58 REF
- PI59 REF
- PI60 REF
- PI61 REF
- PI62 REF
- PI63 REF
- PI64 REF
- PI65 REF
- PI66 REF
- PI67 REF
- PI68 REF
- PI69 REF
- PI70 REF
- PI71 REF
- PI72 REF
- PI73 REF
- PI74 REF
- PI75 REF
- PI76 REF
- PI77 REF
- PI78 REF
- PI79 REF
- PI80 REF
- PI81 REF
- PI82 REF
- PI83 REF
- PI84 REF
- PI85 REF
- PI86 REF
- PI87 REF
- PI88 REF
- PI89 REF
- PI90 REF
- PI91 REF
- PI92 REF
- PI93 REF
- PI94 REF
- PI95 REF
- PI96 REF
- PI97 REF
- PI98 REF
- PI99 REF
- PI00 REF
- PI01 REF
- PI02 REF
- PI03 REF
- PI04 REF
- PI05 REF
- PI06 REF
- PI07 REF
- PI08 REF
- PI09 REF
- PI10 REF
- PI11 REF
- PI12 REF
- PI13 REF
- PI14 REF
- PI15 REF
- PI16 REF
- PI17 REF
- PI18 REF
- PI19 REF
- PI20 REF
- PI21 REF
- PI22 REF
- PI23 REF
- PI24 REF
- PI25 REF
- PI26 REF
- PI27 REF
- PI28 REF
- PI29 REF
- PI30 REF
- PI31 REF
- PI32 REF
- PI33 REF
- PI34 REF
- PI35 REF
- PI36 REF
- PI37 REF
- PI38 REF
- PI39 REF
- PI40 REF
- PI41 REF
- PI42 REF
- PI43 REF
- PI44 REF
- PI45 REF
- PI46 REF
- PI47 REF
- PI48 REF
- PI49 REF
- PI50 REF
- PI51 REF
- PI52 REF
- PI53 REF
- PI54 REF
- PI55 REF
- PI56 REF
- PI57 REF
- PI58 REF
- PI59 REF
- PI60 REF
- PI61 REF
- PI62 REF
- PI63 REF
- PI64 REF
- PI65 REF
- PI66 REF
- PI67 REF
- PI68 REF
- PI69 REF
- PI70 REF
- PI71 REF
- PI72 REF
- PI73 REF
- PI74 REF
- PI75 REF
- PI76 REF
- PI77 REF
- PI78 REF
- PI79 REF
- PI80 REF
- PI81 REF
- PI82 REF

1987

[illegible]

4000 2073

NUMBER OF PROBABILITY										
P	Q	R	S	T	U	V	W	X	Y	Z
1	2	3	4	5	6	7	8	9	10	11
12	13	14	15	16	17	18	19	20	21	22
23	24	25	26	27	28	29	30	31	32	33
34	35	36	37	38	39	40	41	42	43	44
45	46	47	48	49	50	51	52	53	54	55
56	57	58	59	60	61	62	63	64	65	66
67	68	69	70	71	72	73	74	75	76	77
78	79	80	81	82	83	84	85	86	87	88
89	90	91	92	93	94	95	96	97	98	99
100	101	102	103	104	105	106	107	108	109	110
111	112	113	114	115	116	117	118	119	120	121
122	123	124	125	126	127	128	129	130	131	132
133	134	135	136	137	138	139	140	141	142	143
144	145	146	147	148	149	150	151	152	153	154
155	156	157	158	159	160	161	162	163	164	165
166	167	168	169	170	171	172	173	174	175	176
177	178	179	180	181	182	183	184	185	186	187
188	189	190	191	192	193	194	195	196	197	198
199	200	201	202	203	204	205	206	207	208	209
210	211	212	213	214	215	216	217	218	219	220
221	222	223	224	225	226	227	228	229	230	231
232	233	234	235	236	237	238	239	240	241	242
243	244	245	246	247	248	249	250	251	252	253
254	255	256	257	258	259	260	261	262	263	264
265	266	267	268	269	270	271	272	273	274	275
276	277	278	279	280	281	282	283	284	285	286
287	288	289	290	291	292	293	294	295	296	297
298	299	300	301	302	303	304	305	306	307	308
309	310	311	312	313	314	315	316	317	318	319
320	321	322	323	324	325	326	327	328	329	330
331	332	333	334	335	336	337	338	339	340	341
342	343	344	345	346	347	348	349	350	351	352
353	354	355	356	357	358	359	360	361	362	363
364	365	366	367	368	369	370	371	372	373	374
375	376	377	378	379	380	381	382	383	384	385
386	387	388	389	390	391	392	393	394	395	396
397	398	399	400	401	402	403	404	405	406	407
408	409	410	411	412	413	414	415	416	417	418
419	4									

**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT**

[illegible]

GRUMMAN AEROSPACE CORPORATION		PRIORITY	SEQ. NO.	CODE IDENT	EO	12BEL66058	DTG	FI
Q = 12A707-PI		Q = 12A708-SI		EQUIP INSIDE AREA		SER. NO.		
Q = 12A706-AI						MFG. PART NO.		
						EO CONT. NO.		12BEL9116
						SH. NO.		19

ACTION	REFERENCE DESIGNATION	ELECTROMAGNETIC COMPATIBILITY	CABLE ASSEMBLY AND ROUTING CODE ALL CABLES ARE PREFIXED BY: 128AV	REFERENCE DESIGNATOR/ROUTE LETTERS																EFFECTIVITY								
				A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P		Q	R	S	T	U	V	W	X
ADD	Δ		61014 (BP) *																									
	Δ		(BR) *																									
	Δ		(BM) *																									
	Δ		(BN) *																									
	Δ		(BS) *																									
ADD	⊗		(BT) *																									

ACTION	ITEM NO.	HARDWARE REQUIREMENTS
EQUIP OUTSIDE AREA	Δ = 12A711PI	⊗ = SPICE AREA

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT

REVISIONS		DATE	BY	REASON
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				

**ENGINEERING ORDER
MANUFACTURING CHANGE ORDER**

2.74 (PART A)

[illegible]

QAC 1000
1072 (PART B)

GRUMMAN AEROSPACE CORPORATION										DASH NO		REV	
EQUIP INSIDE AREA } 3 = J6045										E0		L4	
PRIORITY										SEQ NO		CODE IDENT	
26512												12BEL6047	
MFG PART NO										SER NO			
EO CONT NO										12BEL4116		21	
REFERENCE DESIGNATOR/ROUTE LETTERS										G (GROUND)		S (SPLICE)	
CABLE ASSEMBLY AND ROUTING CODE ALL CABLES ARE PREPARED BY: 128AV										SEE NOTE		STOCK DISPOSITION	
ELECTROMAGNETIC COMPATIBILITY										A		X	
REFERENCE DESIGNATION										3		F	
ACTION										ADD		A	
HARDWARE REQUIREMENTS										Δ = 12A705-R1			
ITEM NO										EQUIP OUTSIDE AREA			

ENGINEERING ORDER /
MANUFACTURING CHANGE ORDER
SUPPLEMENT

DATE **TIME**

[illegible]

CAC 1000

GRUMMAN AEROSPACE CORPORATION										E0		128 EL 66013		REV L4	
PRIORITY		SEC NO		CABLE IDENT		26512		E0		128 EL 66013		REV L4			
ACTION		ITEM NO.		HARDWARE REQUIREMENTS		CABLE ASSEMBLY AND ROUTING CODE BY: 128AV		66014 (B)*		REFERENCE DESIGNATOR/ROUTE LETTERS		EFFECTIVITY			
ACTION		ITEM NO.		HARDWARE REQUIREMENTS		CABLE ASSEMBLY AND ROUTING CODE BY: 128AV		66014 (B)*		REFERENCE DESIGNATOR/ROUTE LETTERS		EFFECTIVITY			
ADD										F X B X		G (GROUND)			
												S (SPLICE)			
												SEE NOTE			
												STOCK DISPOSITION			
												EFFECTIVITY			

ENGINEERING ORDER/
 MANUFACTURING CHANGE ORDER
 SUPPLEMENT

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT

[illegible]

DATE: 10/11/2011

[illegible]

AD-A100 730

GRUMMAN AEROSPACE CORP BETHPAGE NY
HYDRAULIC DIAGNOSTIC MONITORING SYSTEM.(U)
MAR 81 J J DUZICH

F/G 14/2

N62269-78-C-0041

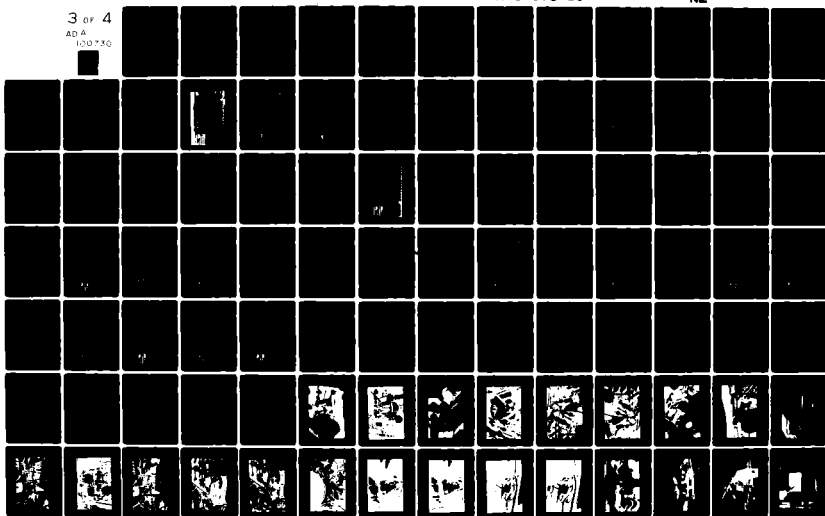
UNCLASSIFIED

NADC-TR-81073-60

NL

3 of 4

AD A
100 730



GRUMMAN AEROSPACE CORPORATION				SEQ NO	26512	CONTRACT NO	26512	NOTED	128 EL 66041	DRAWING NO	W5	REV	K5
WFG PART NO		ACD	ACD	PL/DEPT	ECF	OPERATIONS	OPERATIONS	DESIGN	128 EL 66041	TO CONT NO	128 EL 9222		
PL/DEPT		OPERATIONS	INS	PL/DEPT	ECF	OPERATIONS	OPERATIONS	DESIGN	128 EL 66041	TO CONT NO	128 EL 9222		
CONTRACT NO		N62269-78-C-0041											
DWG TITLE		SEE DWGS											
ACTION		QTY/MA	QTY/EL	PART NUMBER	NOTE	NEXT ASSEMBLY DWG	SD	EFF	UT	AUTHORITY	MODEL	END ITEM	CAC UNIT NO
										1 NAVAIR LTR	14E		11229
										2141-7K-79-49	19/79		

ENGINEERING ORDER				
DRAWING NUMBER	REV	SEQ NO	REV DWG	DOC
128 EL 66053	K5	52		1.3
128 EL 66019	M3	44		1.4
128 EL 66024	M3	46		1.5
128 EL 66039	TR	26		1.6.7
128 EL 66041	K5	28		1.2

THIS IS A RECORD E.O.

REASON FOR CHANGE		DESCRIPTION OF CHANGE	
INSTL OF HYDRAULIC CHECK-OUT SYSTEM (MYCOS)		DWGS NOTED ABOVE	
IN A/C FOR INSTRUMENTATION PURPOSES		ADDED WIRING RUNS	

APPROVED BY	GROUP FOR	SUPPORT	RELIABILITY	STRESS	PROD ENGRS	RELEASE	CUSTOMER
J. B. B...	1	PWD/MA	1	1	1	1	1
SIGNATURE	DATE	REV DWG	REV DWG	REV DWG	REV DWG	REV DWG	REV DWG
4-25-79	4-26-79	1	1	1	1	1	1
DATE	QTY PER ASST	QTY PER ASST	QTY PER ASST	QTY PER ASST	QTY PER ASST	QTY PER ASST	QTY PER ASST
4-19-79	4-19-79	4-19-79	4-19-79	4-19-79	4-19-79	4-19-79	4-19-79
DATE	DATE	DATE	DATE	DATE	DATE	DATE	DATE

ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

[illegible]

[illegible]

[illegible]

**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT**

GRUMMAN AEROSPACE CORPORATION				E0 NOTEL 128 EL 66058				DATE 12-5-1-4116			
PROJECT NAME				PROJECT NO				PROJECT NO			
OPERATIONS				OPERATIONS				OPERATIONS			
CITY				CITY				CITY			
STATE				STATE				STATE			
COUNTRY				COUNTRY				COUNTRY			
DRAWING NO				DRAWING NO				DRAWING NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE				TO TYPE				TO TYPE			
SO				SO				SO			
NO				NO				NO			
REV				REV				REV			
DATE				DATE				DATE			
BY				BY				BY			
CHECKED				CHECKED				CHECKED			
APPROVED				APPROVED				APPROVED			
SIGNATURE				SIGNATURE				SIGNATURE			
DATE				DATE				DATE			
TO TYPE											

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

[illegible]

100-443881

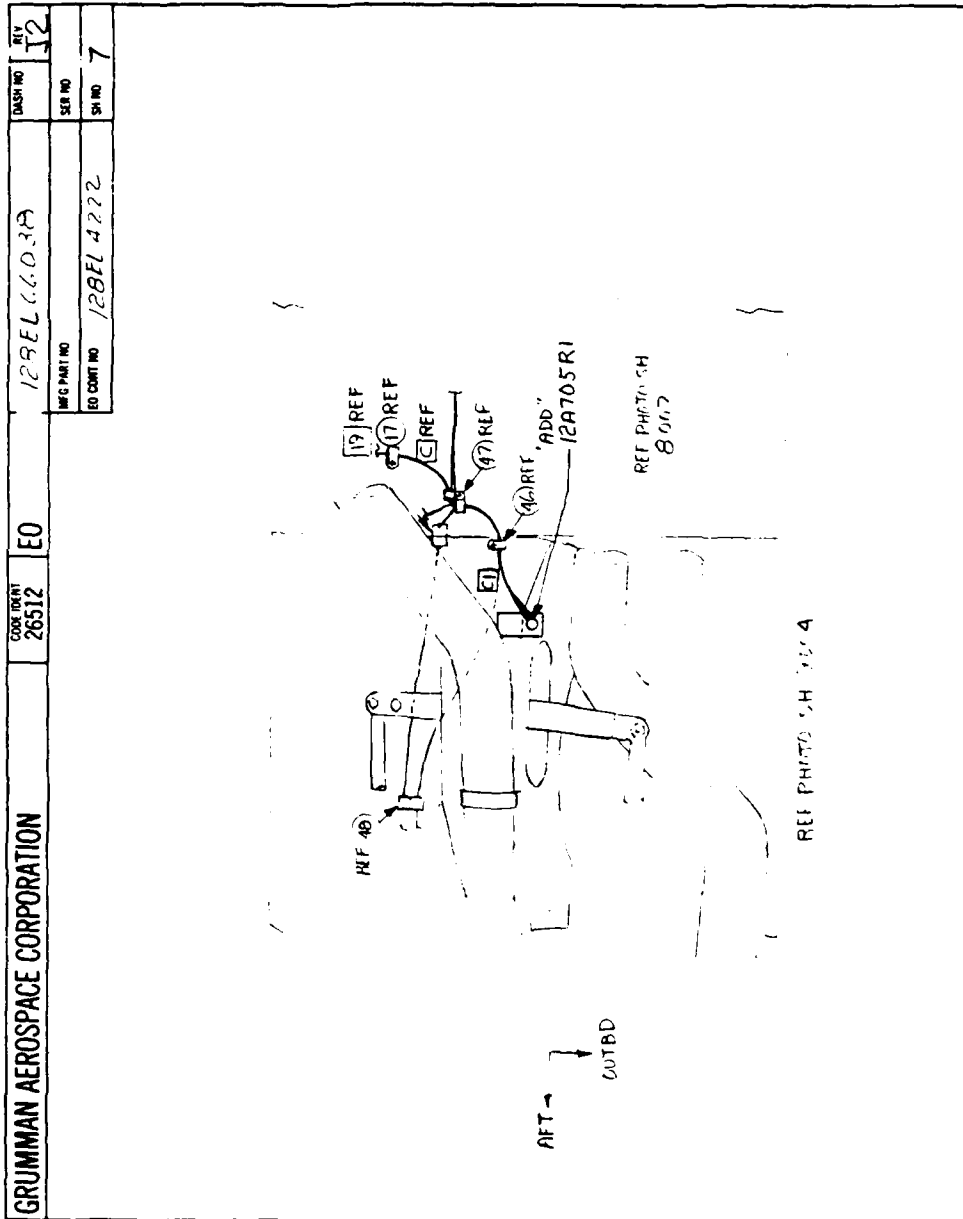
**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT**

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT

5-17-1968

**ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT**

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER
SUPPLEMENT



ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

[illegible]

GRUMMAN AEROSPACE CORPORATION				COO TITRY 26512	SEQ NO	EO NOTED	DASH NO	REV
INFO PART NO	MCO REV	ACD	ECR	PLT DEPT	INSR	DET SPEC	CHG CL	W/B
PLT/DEPT	OPERATIONS					128 EL 6001	1	128 EL 4116
CONTRACT NO N62269-78-C-0041				REPLACES PART NO				
DWG TITLE SEE DWGS				SH 1 0125				
ACTION	QTY IN	QTY EI	PART NUMBER	NOTE	NEXT ASSEMBLY DWG	SD	EFF	END ITEM
								M 229

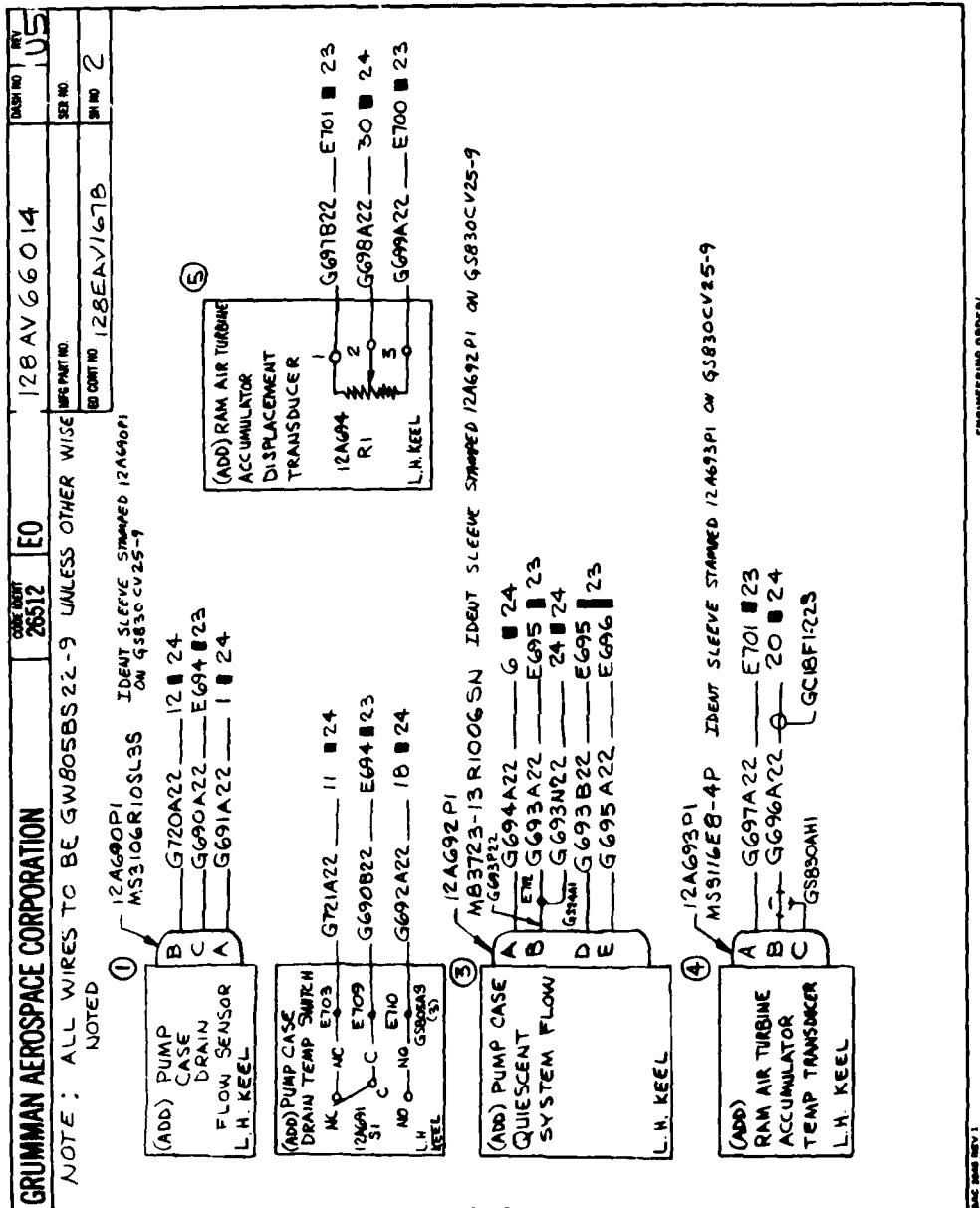
ENGINEERING ORDER										
DRAWING	NUMBER	REV	SEQ	NO	REV	DWG	DOC	REF	EO	SH
EO	128 EL 6001	K2	25						134567	
EO	128 EL 6003	K2	40						18910	
EO	128 EL 6003	M7	57						11112	
EO	128 EL 6001	L3	53						113	
EO	128 EL 6003	H9	36						114	
EO	128 EL 6003	H6	30						115	
EO	128 EL 6003	H4	33						116	
EO	128 EL 6003	K5	34						117	
EO	128 EL 6003	K2	27						210	
EO	128 EL 6003	F1	7						21920	
EO	128 EL 6003	L4	31						223	
EO	128 EL 6003	L1	44						222	
EO	128 EL 6003	L4	56						221	
EO	128 EL 6003	L1	38						2225	
EO	128 EL 6003	L1	38						221	
EO	128 EL 6003	L1	38						221	

REASON FOR CHANGE									
INSTL OF HYDRAULIC CHECK-OUT SYS (HYCOS)									
IN AK FOR INSTRUMENTATION PURPOSES									
APPROVED BY	UNAPPROVED BY	SUPPORT	RELIABILITY	STRESS	PROD ENGR	PROD ENGR	PROD ENGR	PROD ENGR	PROD ENGR
J. Bo Hun		2-22-79	2-22-79	2-22-79	2-22-79	2-22-79	2-22-79	2-22-79	2-22-79
DATE	EXT	2-20-79	2-20-79	2-20-79	2-20-79	2-20-79	2-20-79	2-20-79	2-20-79
GAC 3444 REV 1									

THIS IS A RECORD E.O.

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER



—EAC 2008 REV 1

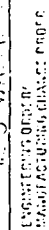
[illegible]

DAC 2048

ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

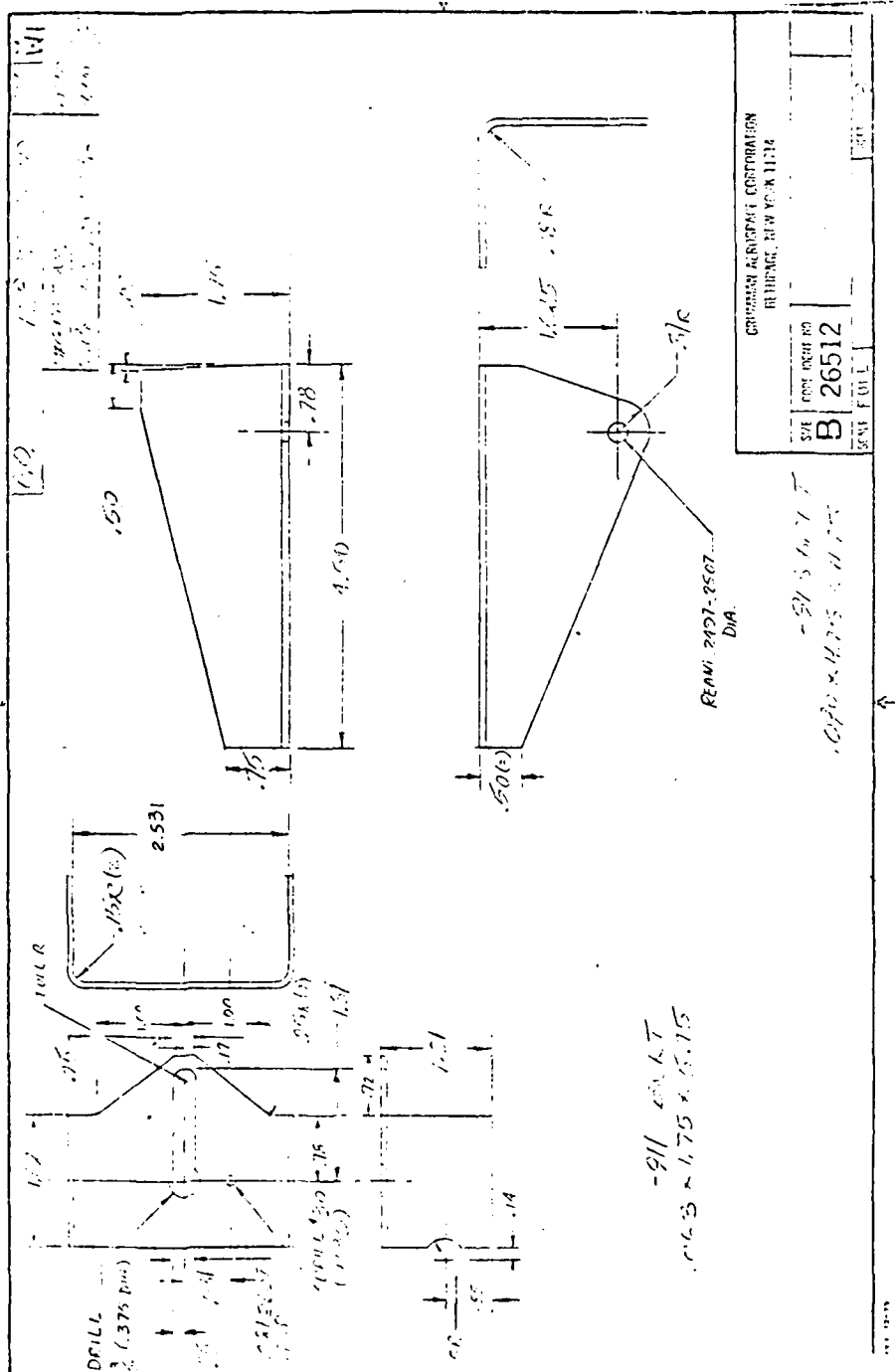
1. NAME OF THE PARTY
 2. NAME OF THE PARTY

[illegible]

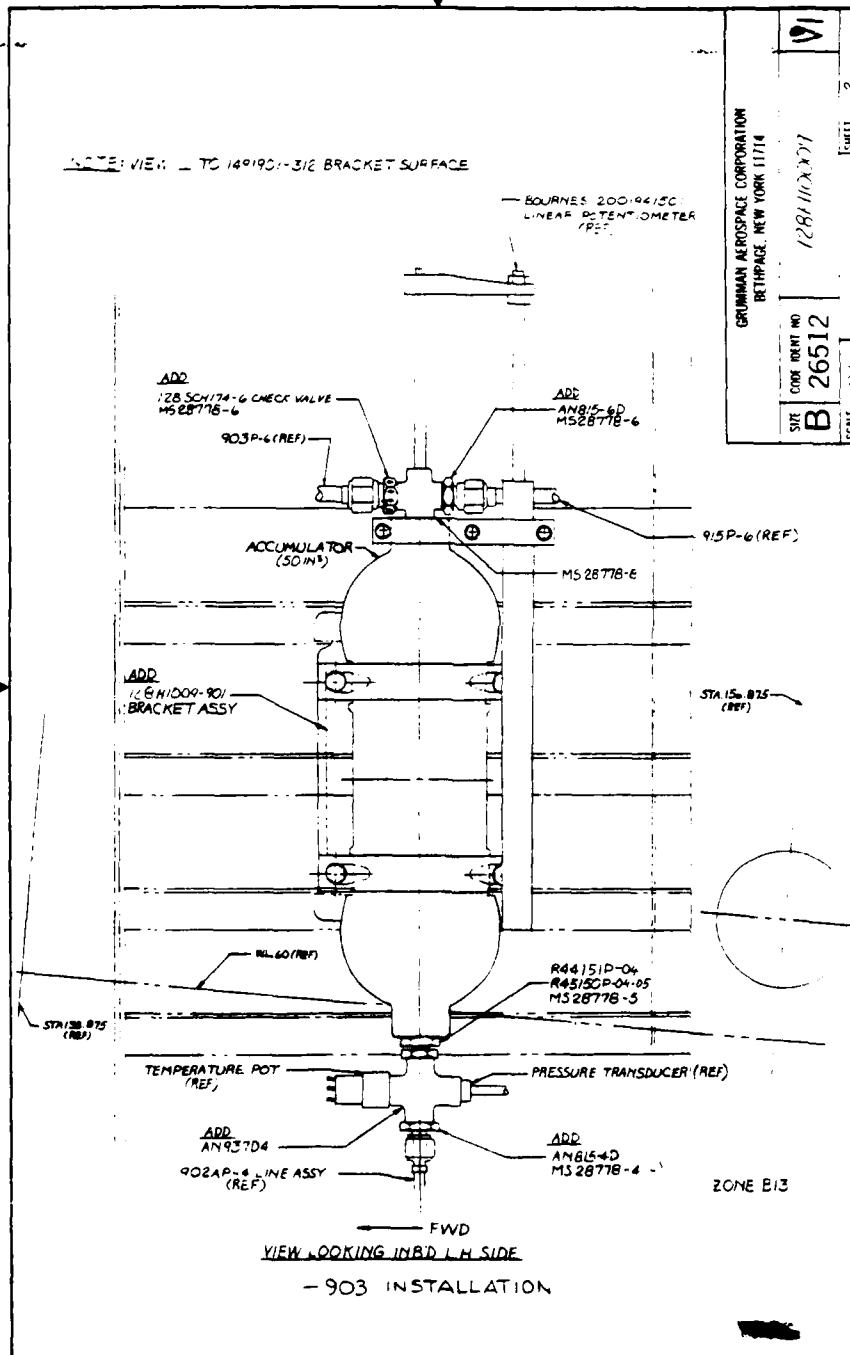


GRUMMAN AEROSPACE CORPORATION										DASH NO		W/F		M/F	
SPE PART NO										26512		E0		128CS10000	
PL/DEPT										OPERATIONS		PL/DEPT		128C637	
CONTRACT NO										N62269-76-C-0041		ECP		128C637	
SPE TITLE										POTENTIOMETER INSTL - LK SYS - RUDEL		ECP		128C637	
ACTION										QTY/AM		QTY/EL		PART NUMBER	
NOTE										NEXT ASSEMBLY TIME		SO		EEL	
EFFECT										AUTHORITY		MODEL		END ITEM	
EFFECT										1 UN2441 TL		146E		M222	
EFFECT										75-143, 31 JAN 77					
EFFECT										REPLACES PART NO		101		OF 1	
EFFECT										128CM13234-1		128CM13234-1		REF	
EFFECT										128CS10000-913 BLT (REF)		VIEW 8 &		(FROM E0128CS10000) M1	
EFFECT										NAS1104-7U REF					
EFFECT										AN260D46L REF					
EFFECT										GN10UG14SC2 REF					
EFFECT										AN320-4 REF					
EFFECT										M-24665-151 REF					
EFFECT										-201					
EFFECT										PART NUMBER		151		151	
EFFECT										QTY PER ASSY		1		1	
EFFECT										REASON FOR CHANGE		PROVIDE ALT. INSTALLATION TO PERMIT CHANGE		OF OPTIMUM LINK POSITION	
EFFECT										APPROVED BY		W. M. SAK		10-2-77	
EFFECT										DATE		10-2-77		10-2-77	
EFFECT										SIGNATURE		W. M. SAK		10-2-77	
EFFECT										DATE		10-2-77		10-2-77	
EFFECT										REASON FOR CHANGE		PROVIDE ALT. INSTALLATION TO PERMIT CHANGE		OF OPTIMUM LINK POSITION	
EFFECT										APPROVED BY		W. M. SAK		10-2-77	
EFFECT										DATE		10-2-77		10-2-77	
EFFECT										SIGNATURE		W. M. SAK		10-2-77	
EFFECT										DATE		10-2-77		10-2-77	

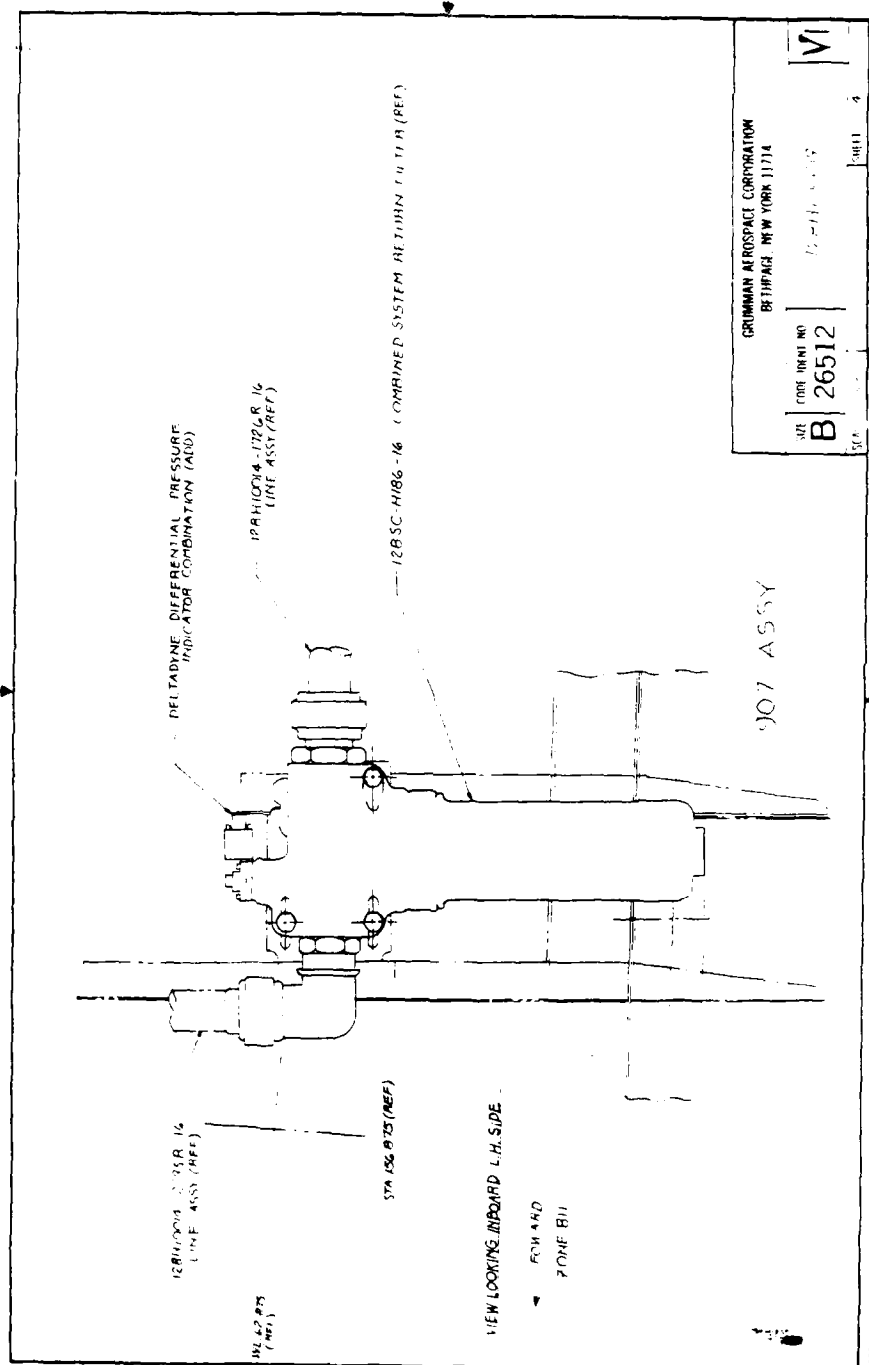
MATERIALS CHECK SHEET				12.6 CS 10000				10				26532				10			
ITEM				QUANTITY				UNIT				REMARKS				DATE			
A) 67200-0-0-004																			
1) 67200-0-0-004																			
2) 67200-0-0-004																			
3) 67200-0-0-004																			
4) 67200-0-0-004																			
5) 67200-0-0-004																			
6) 67200-0-0-004																			
7) 67200-0-0-004																			
8) 67200-0-0-004																			
9) 67200-0-0-004																			
10) 67200-0-0-004																			
11) 67200-0-0-004																			
12) 67200-0-0-004																			
13) 67200-0-0-004																			
14) 67200-0-0-004																			
15) 67200-0-0-004																			
16) 67200-0-0-004																			
17) 67200-0-0-004																			
18) 67200-0-0-004																			
19) 67200-0-0-004																			
20) 67200-0-0-004																			
21) 67200-0-0-004																			
22) 67200-0-0-004																			
23) 67200-0-0-004																			
24) 67200-0-0-004																			
25) 67200-0-0-004																			
26) 67200-0-0-004																			
27) 67200-0-0-004																			
28) 67200-0-0-004																			
29) 67200-0-0-004																			
30) 67200-0-0-004																			
31) 67200-0-0-004																			
32) 67200-0-0-004																			
33) 67200-0-0-004																			
34) 67200-0-0-004																			
35) 67200-0-0-004																			
36) 67200-0-0-004																			
37) 67200-0-0-004																			
38) 67200-0-0-004																			
39) 67200-0-0-004																			
40) 67200-0-0-004																			
41) 67200-0-0-004																			
42) 67200-0-0-004																			
43) 67200-0-0-004																			
44) 67200-0-0-004																			
45) 67200-0-0-004																			
46) 67200-0-0-004																			
47) 67200-0-0-004																			
48) 67200-0-0-004																			
49) 67200-0-0-004																			
50) 67200-0-0-004																			
51) 67200-0-0-004																			
52) 67200-0-0-004																			
53) 67200-0-0-004																			
54) 67200-0-0-004																			
55) 67200-0-0-004																			
56) 67200-0-0-004																			
57) 67200-0-0-004																			
58) 67200-0-0-004																			
59) 67200-0-0-004																			
60) 67200-0-0-004																			
61) 67200-0-0-004																			
62) 67200-0-0-004																			
63) 67200-0-0-004																			
64) 67200-0-0-004																			
65) 67200-0-0-004																			
66) 67200-0-0-004																			
67) 67200-0-0-004																			
68) 67200-0-0-004																			
69) 67200-0-0-004																			
70) 67200-0-0-004																			
71) 67200-0-0-004																			
72) 67200-0-0-004																			
73) 67200-0-0-004																			
74) 67200-0-0-004																			
75) 67200-0-0-004																			
76) 67200-0-0-004																			
77) 67200-0-0-004																			
78) 67200-0-0-004																			
79) 67200-0-0-004																			
80) 67200-0-0-004																			
81) 67200-0-0-004																			
82) 67200-0-0-004																			
83) 67200-0-0-004																			
84) 67200-0-0-004																			
85) 67200-0-0-004																			
86) 67200-0-0-004																			
87) 67200-0-0-004																			
88) 67200-0-0-004																			
89) 67200-0-0-004																			
90) 67200-0-0-004																			
91) 67200-0-0-004																			
92) 67200-0-0-004																			
93) 67200-0-0-004																			
94) 67200-0-0-004																			
95) 67200-0-0-004																			
96) 67200-0-0-004																			
97) 67200-0-0-004																			
98) 67200-0-0-004																			
99) 67200-0-0-004																			
100) 67200-0-0-004																			

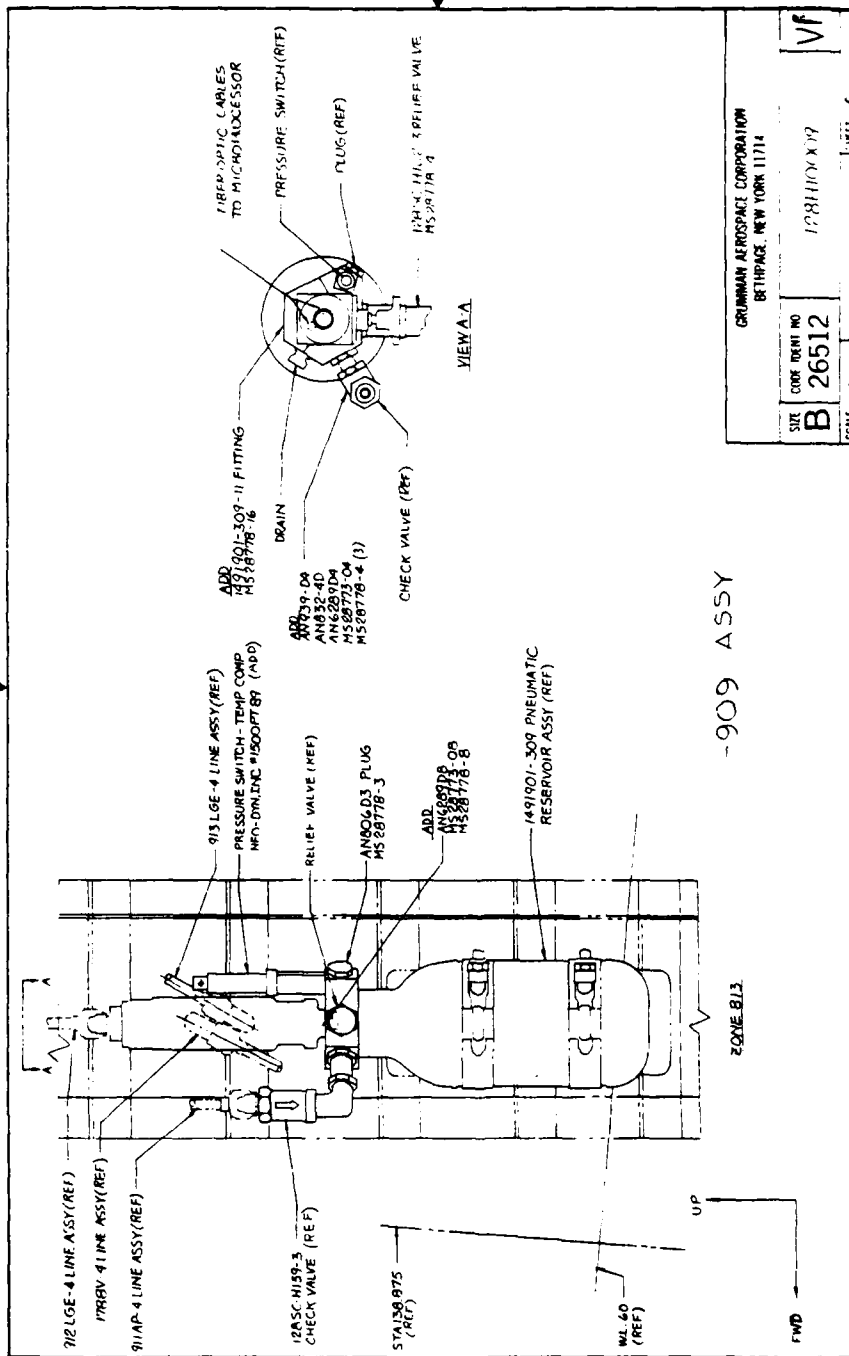


[illegible]



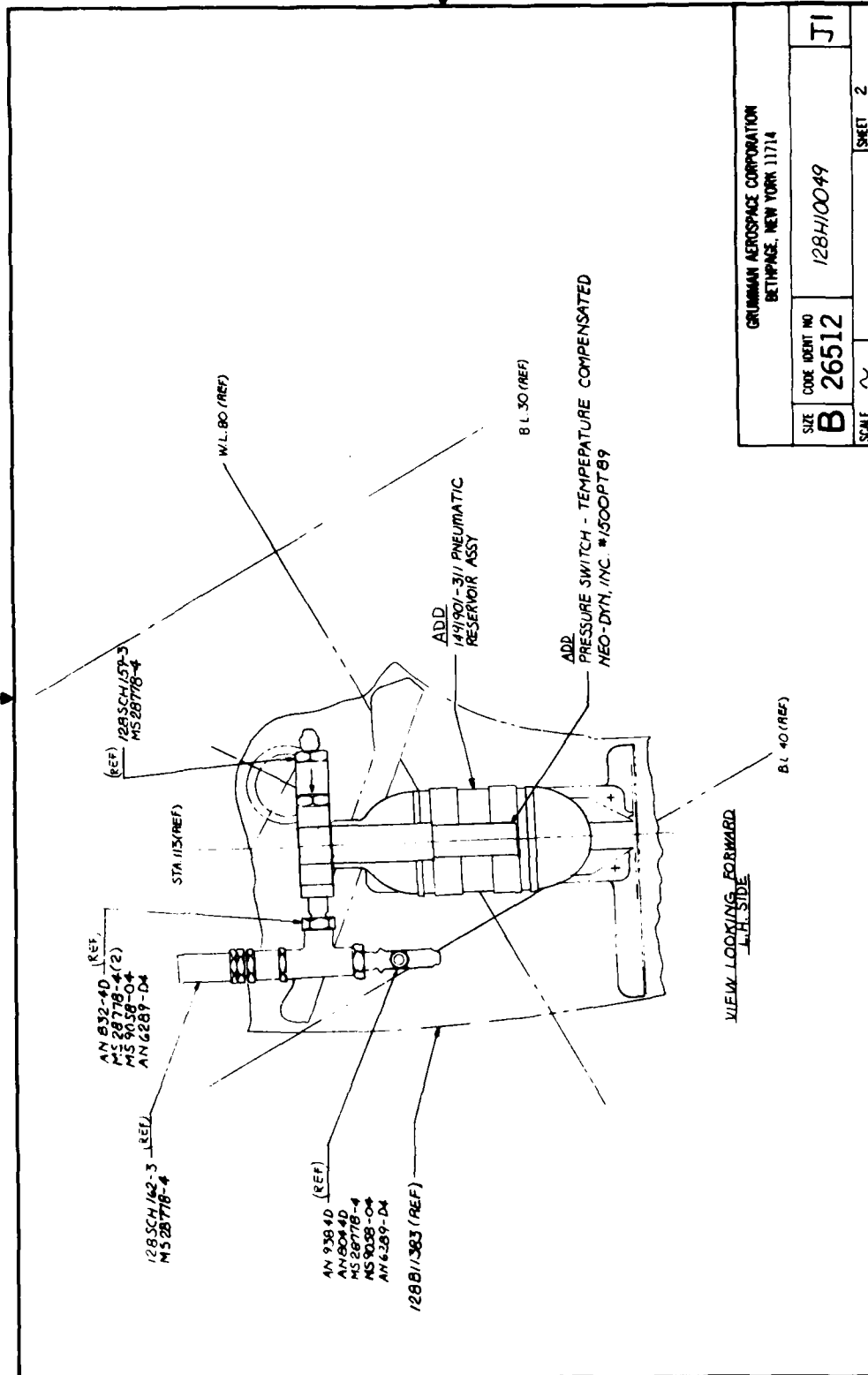




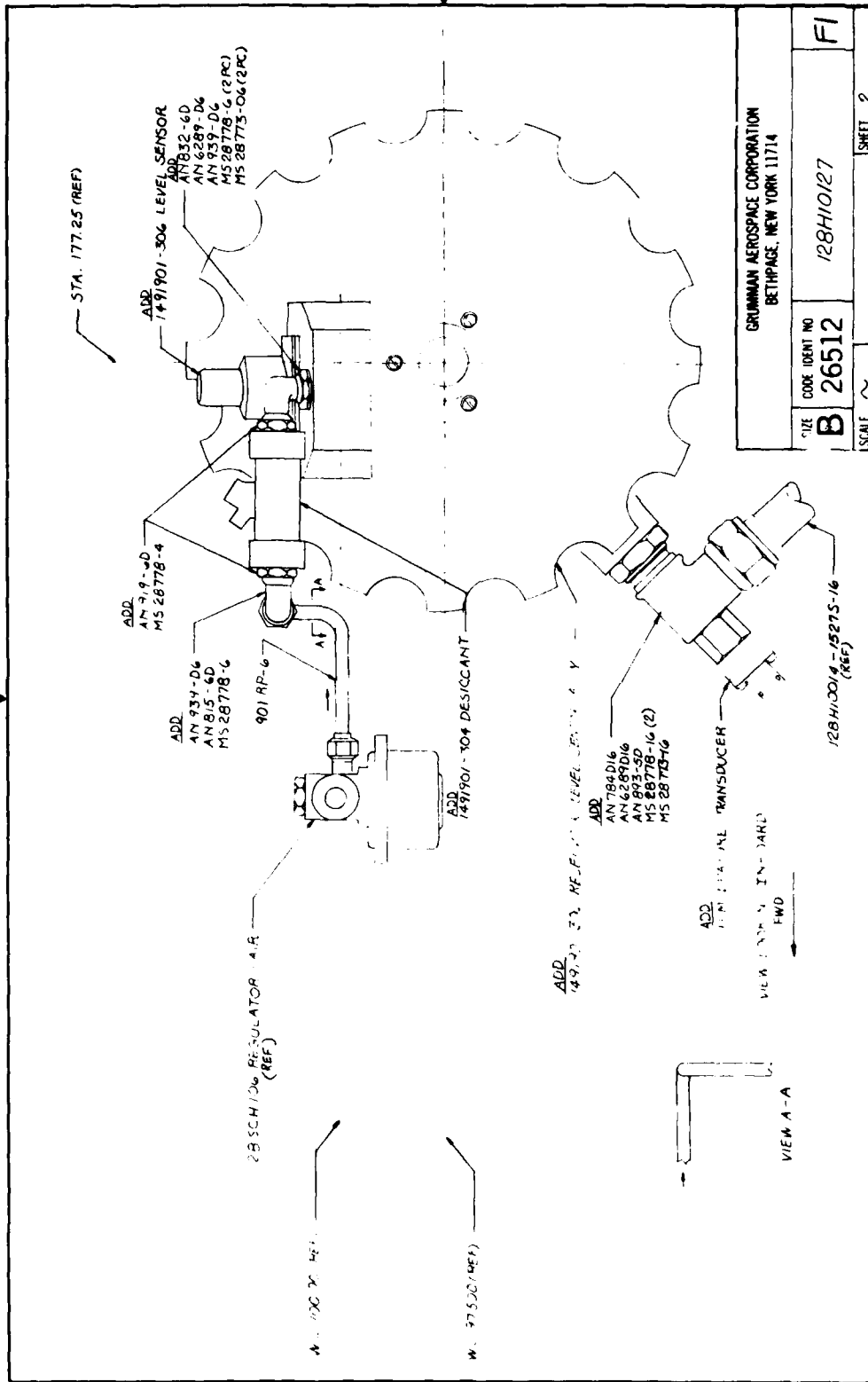


NO ACTION & ACCEPT 181
ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

[illegible]



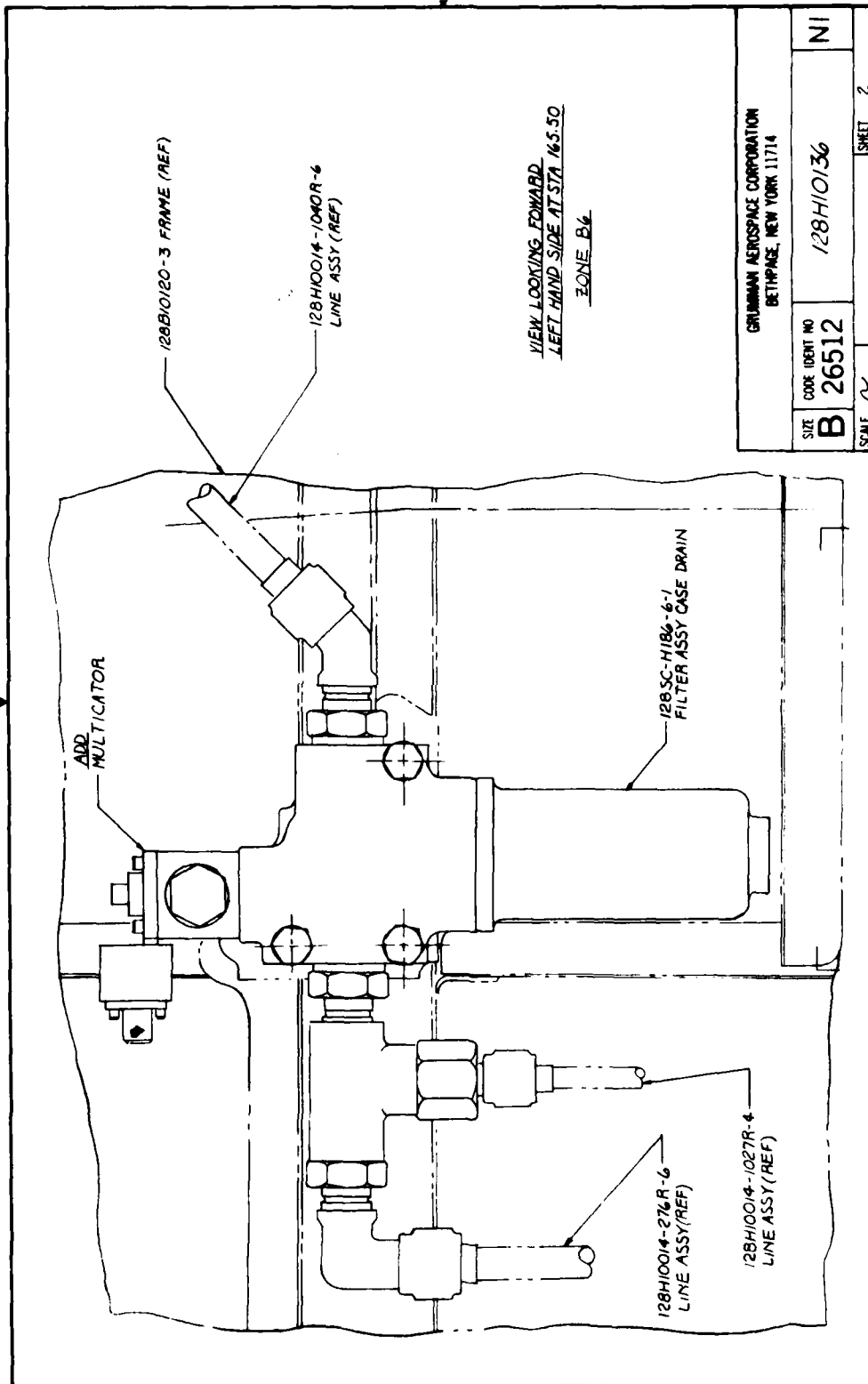
GRUBMAN AEROSPACE CORPORATION BETHPAGE, NEW YORK 11714		J1	
SIZE B	CODE IDENT NO 26512	128H10049	
SCALE ~		SHEET 2	



GRUMMAN AEROSPACE CORPORATION										SEC NO 7		CORP IDENT 26512		EO		128H10127		DASH NO		REV F2					
WFG PART NO										MFG REV 1		ECP		PROJ C		CHG CL 1		EO CONT NO 128H 775							
PLT/DEPT										OPERATIONS		INSPECTION		DESIGN SPEC		END ITEM NO		DTY I							
CONTRACT NO N62269-78C-0041										PLT/DEPT		OPERATIONS		INSPECTION		DESIGN SPEC		END ITEM NO		DTY I					
CONTRACT TITLE RESERVOIR INSTL HYDRAULIC - COMBINED SYSTEM										PLT/DEPT		OPERATIONS		INSPECTION		DESIGN SPEC		END ITEM NO		DTY I					
ACTION QTY IN QTY EI PART NUMBER										NOTE		SD		EFT		EFT		EFT		EFT					
1 21411-TK79-143 AGE										1 21411-TK79-143 AGE		1 21411-TK79-143 AGE		1 21411-TK79-143 AGE		1 21411-TK79-143 AGE		1 21411-TK79-143 AGE		1 21411-TK79-143 AGE					
REMOVE B										AN939-D6		AN815-6D		MS28-78-6											
THIS IS A RECORD E.O.																									
VIEW LOOKING INBOARD																									
90° PNEUMATIC LINE BEND REPLACED 90° ELBOW																									
REMOVED FITTINGS FROM 90IRP-6 LINE																									
APPROVED BY W. MOORE										GROUP FOR		SUPPORT		RELIABILITY		STRESS		PROD ENG		RELEASE 67		CUSTOMER			
SECTION FLUID POWER										SIGNATURE		DATE													
PLANT GROUP 04010357										EO TYPE		DIRECT ENG CHG (DOCI)		REV ENG		PROD ENG		RECORD E.O.		LAD 1		INST A			
DATE EXT 3-22-79 618Y										SD		RECM STK DISPN		DISPOSE 2		REWORK 3		INCREASE 4		CREATE 5		USE 6		HOLD 7	
NO ACTION 8										ACCEPT 9		IDENT 10		TRACEABILITY 11											

ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

CONFIGURATION VERIFICATION AND TRACEABILITY RECORD									
PART NO. 128H 775									
DATE 3-22-79									
BY W. MOORE									
CHECKED BY									
APPROVED BY									
DATE									
REVISIONS									
REV 1									
REV 2									
REV 3									
REV 4									
REV 5									
REV 6									
REV 7									
REV 8									
REV 9									
REV 10									
REV 11									
REV 12									
REV 13									
REV 14									
REV 15									
REV 16									
REV 17									
REV 18									
REV 19									
REV 20									
REV 21									
REV 22									
REV 23									
REV 24									
REV 25									
REV 26									
REV 27									
REV 28									
REV 29									
REV 30									
REV 31									
REV 32									
REV 33									
REV 34									
REV 35									
REV 36									
REV 37									
REV 38									
REV 39									
REV 40									
REV 41									
REV 42									
REV 43									
REV 44									
REV 45									
REV 46									
REV 47									
REV 48									
REV 49									
REV 50									
REV 51									
REV 52									
REV 53									
REV 54									
REV 55									
REV 56									
REV 57									
REV 58									
REV 59									
REV 60									
REV 61									
REV 62									
REV 63									
REV 64									
REV 65									
REV 66									
REV 67									
REV 68									
REV 69									
REV 70									
REV 71									
REV 72									
REV 73									
REV 74									
REV 75									
REV 76									
REV 77									
REV 78									
REV 79									
REV 80									
REV 81									
REV 82									
REV 83									
REV 84									
REV 85									
REV 86									
REV 87									
REV 88									
REV 89									
REV 90									
REV 91									
REV 92									
REV 93									
REV 94									
REV 95									
REV 96									
REV 97									
REV 98									
REV 99									
REV 100									



GRUMMAN AEROSPACE CORPORATION BETHPAGE, NEW YORK 11714			
SIZE B	CODE IDENT NO 26512	128H10136	NI
SCALE ~	SHEET 2		

TOP 15 1 12-72

GRUMMAN AEROSPACE CORPORATION										CODE IDENT 26512	E0 NOTED	DASH NO W2
										MFG PART NO	SER NO	
										EO CONT NO 265H811	SH NO	

ACTION	QTY	NA	QTY	ET	PART NUMBER	NOTE	NEXT ASSEMBLY DWS	SD	EFF	AUTHORITY	MODEL	END ITEM	GAC UNIT NO
3	100	ASSY				COMBINED SYSTEM RETURN FILTER (285C-H-1116)							
						REMOVE 100 PC LINE DIFFERENTIAL PRESSURE INDICATOR COMBINATION							
						WITH 100 PC LINE DIFFERENTIAL PRESSURE INDICATOR COMBINATION							
4	300	ASSY				REMOVE DIFFERENTIAL PRESSURE INDICATOR (149120-309)							
						INSTALL FMC DOOR EMERGENCY AIR BOTTLE (285C-H111) / (128N40026-1) PER (28H100) 3 INSTL							

ACTION	QTY PER ASSY	PART NUMBER	NOMENCLATURE	NOTE	COMMERCIAL SPECIFICATION CODE IDENT - COMB PART NO	MATERIAL SPECIFICATION	PROC	FIN	ZONE	A	S	D	E

ENGINEERING ORDER
MANUFACTURING CHANGE ORDER

ENGINEERING ORDER/
MANUFACTURING CHANGE ORDER

GRUMMAN AEROSPACE CORPORATION										CONTRACT NO. 26512		EONOTED 128H10127		DASH NO. 128H10127		REV. 51	
MFG PART NO.		REC REV		ACD		ECP		OPERATIONS		CHG CL		ED CONT NO.		128H10127		QTY/EI	
PLT/DEPT		OPERATIONS		INSPE		PLT/DEPT		OPERATIONS		INSPE		ED ITEM NO.		ACFT NO.		CONFIG RECD/CONFIG NOT RECD	
CONTRACT NO.		OPERATIONS		INSPE		PLT/DEPT		OPERATIONS		INSPE		ED ITEM NO.		ACFT NO.		CONFIG RECD/CONFIG NOT RECD	
LONG TITLE RESERVOIR INSTL - HYDRAULIC - COMBINED SYSTEM ACTION QTY/INQ QTY/EB PART NUMBER NOTE NEXT ASSEMBLY DNG SD EFT AUTHORITY MODEL EMD ITEM QAC UNIT NO.																	
(HYCOS) REMOVE RESERVOIR ASSY, 128H10125-1, RESERVOIR LEVEL SENSOR ASSY, AN9130-306, TEMPERATURE TRANSDUCER, DESICCANT, AN9130-304 & ALL ASSOCIATED HARDWARES AN919-6D, AN832-6D, AN6289-D6, AN939-D6, MS28773-06 (2), MS28778-4 MS28778-6 (2), MS28776-16 (2), MS28773-16, AN784D16, AN6289D16, AN893-50 RE-INSTALL RESERVOIR ASSY, 128H10125-1, PER 128H10127-1 INSTL																	
REASON FOR CHANGE		QTY PER ASSY		PART NUMBER		RESERVOIR INSTL		NOTE		COMMERCIAL SPECIFICATION CODE IDENT - COM PART NO		MATERIAL SPECIFICATION		PROC		FIN	
APPROVED BY		SIGNATURE		DATE		RELIABILITY		STRESS		PROJ ENGNG		PROJ ENGNG		RELEASE		CUSTOMER	
SECTION		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	
PLANT/ GROUP		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	
DATE - EXT		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	

 QAC 3044 REV 1
 8-11 PART 1

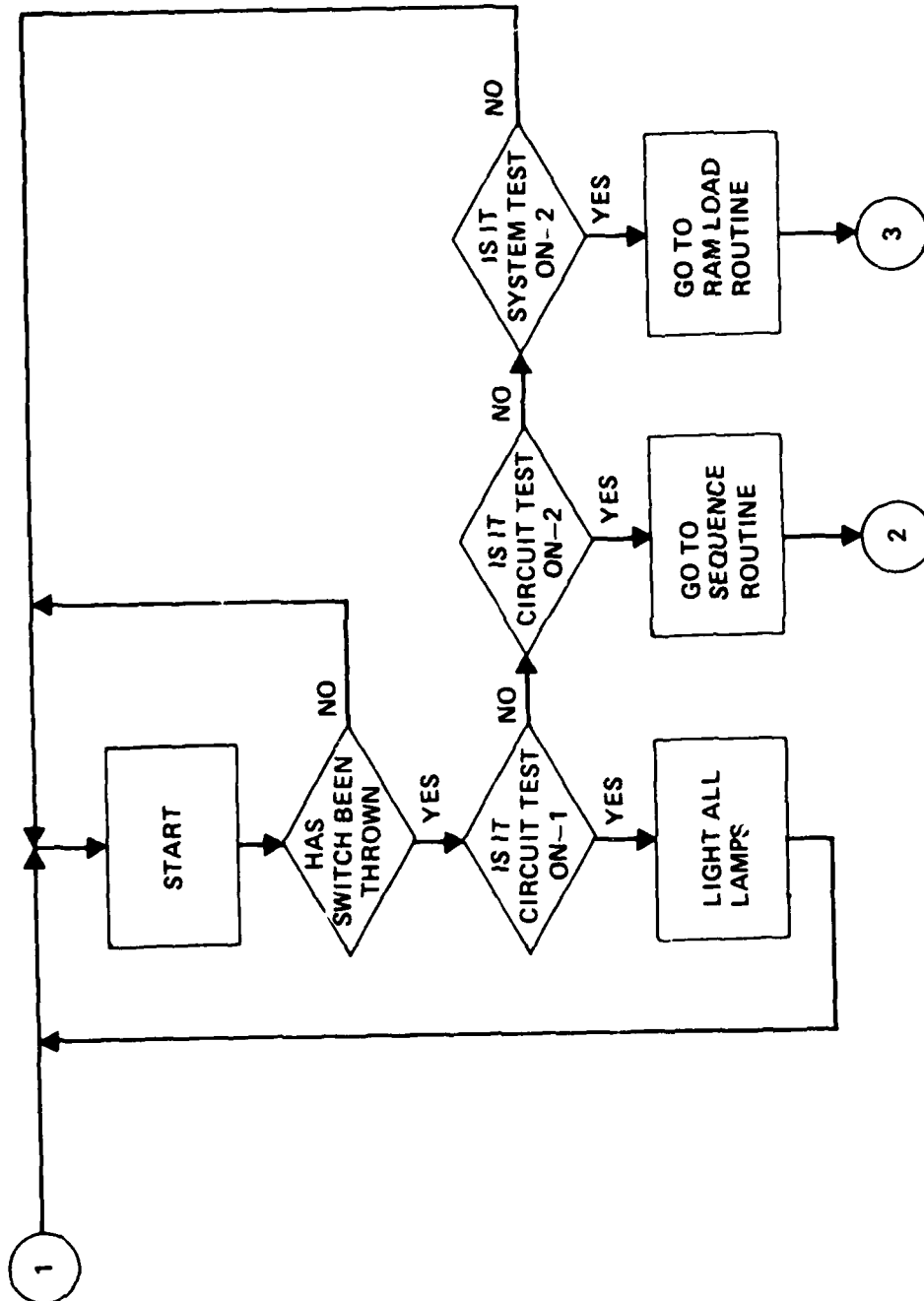
GRUMMAN AEROSPACE CORPORATION										CONTRACT NO. 26512		EONOTED 128H10127		DASH NO. 128H10127		REV. 51	
MFG PART NO.		REC REV		ACD		ECP		OPERATIONS		CHG CL		ED CONT NO.		128H10127		QTY/EI	
PLT/DEPT		OPERATIONS		INSPE		PLT/DEPT		OPERATIONS		INSPE		ED ITEM NO.		ACFT NO.		CONFIG RECD/CONFIG NOT RECD	
CONTRACT NO.		OPERATIONS		INSPE		PLT/DEPT		OPERATIONS		INSPE		ED ITEM NO.		ACFT NO.		CONFIG RECD/CONFIG NOT RECD	
LONG TITLE RESERVOIR INSTL - HYDRAULIC - COMBINED SYSTEM ACTION QTY/INQ QTY/EB PART NUMBER NOTE NEXT ASSEMBLY DNG SD EFT AUTHORITY MODEL EMD ITEM QAC UNIT NO.																	
(HYCOS) REMOVE RESERVOIR ASSY, 128H10125-1, RESERVOIR LEVEL SENSOR ASSY, AN9130-306, TEMPERATURE TRANSDUCER, DESICCANT, AN9130-304 & ALL ASSOCIATED HARDWARES AN919-6D, AN832-6D, AN6289-D6, AN939-D6, MS28773-06 (2), MS28778-4 MS28778-6 (2), MS28776-16 (2), MS28773-16, AN784D16, AN6289D16, AN893-50 RE-INSTALL RESERVOIR ASSY, 128H10125-1, PER 128H10127-1 INSTL																	
REASON FOR CHANGE		QTY PER ASSY		PART NUMBER		RESERVOIR INSTL		NOTE		COMMERCIAL SPECIFICATION CODE IDENT - COM PART NO		MATERIAL SPECIFICATION		PROC		FIN	
APPROVED BY		SIGNATURE		DATE		RELIABILITY		STRESS		PROJ ENGNG		PROJ ENGNG		RELEASE		CUSTOMER	
SECTION		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	
PLANT/ GROUP		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	
DATE - EXT		DATE		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS		REMARKS	

 QAC 3044 REV 1
 8-11 PART 1

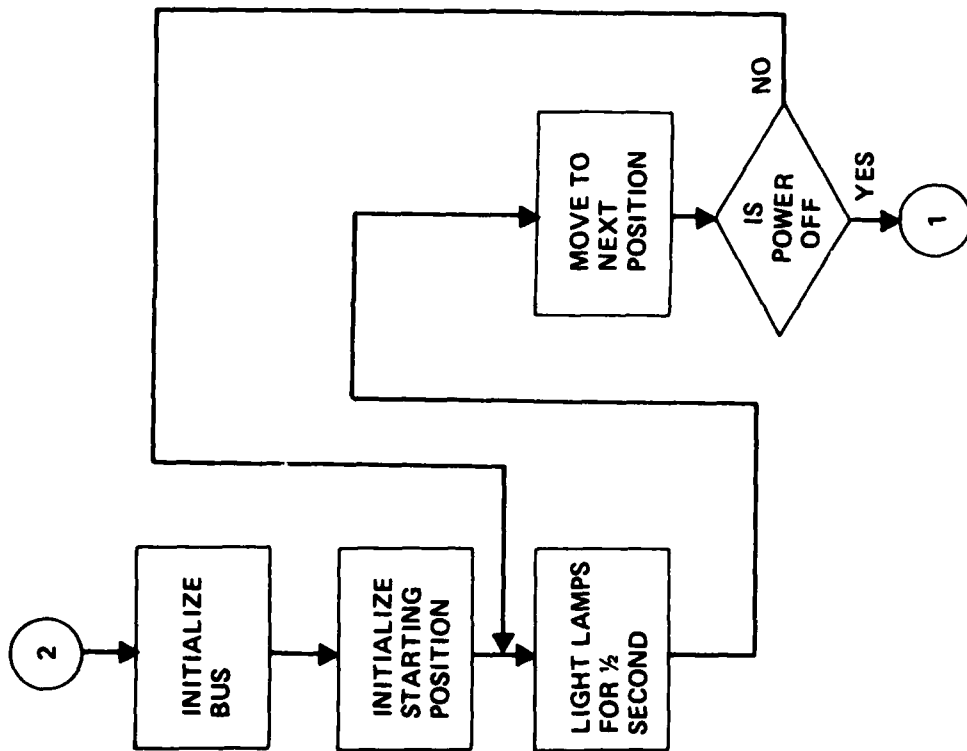
NADC 81073-60

APPENDIX H
HYCOS PROGRAM FLOW DIAGRAM

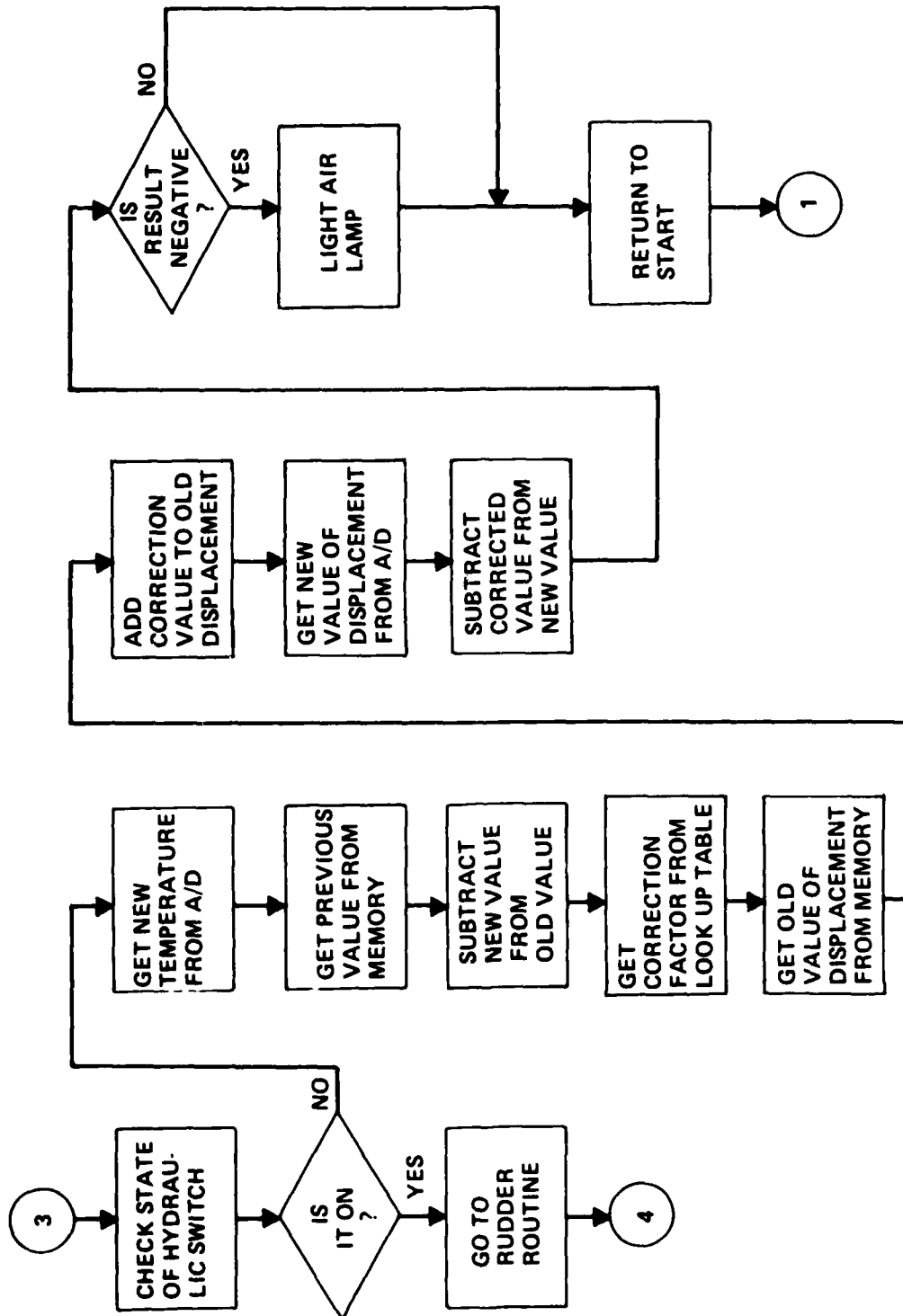
EXECUTIVE ROUTINE



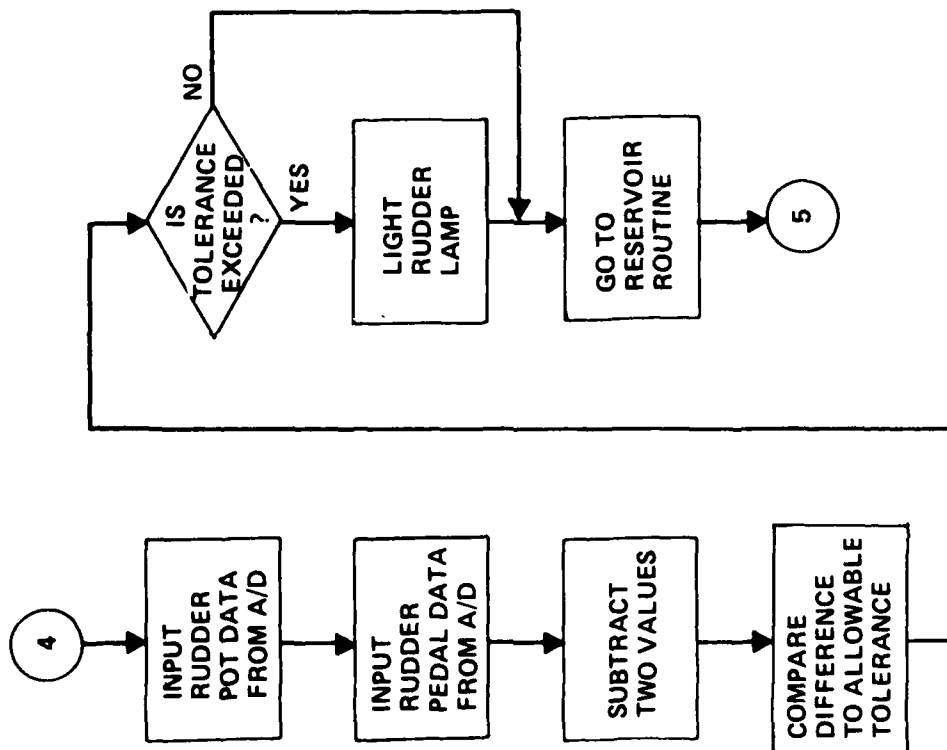
SEQUENCE ROUTINE



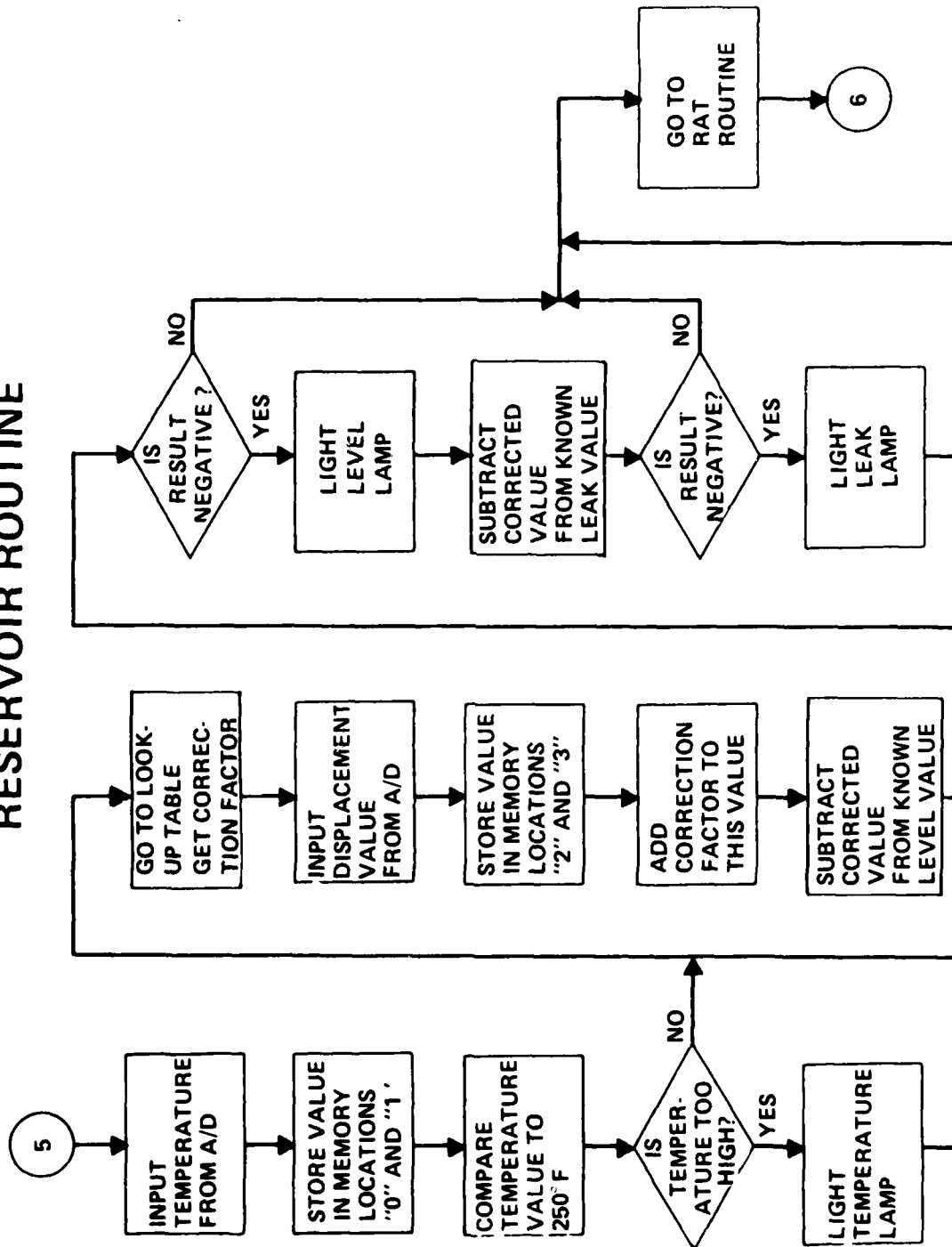
RAM LOAD ROUTINE



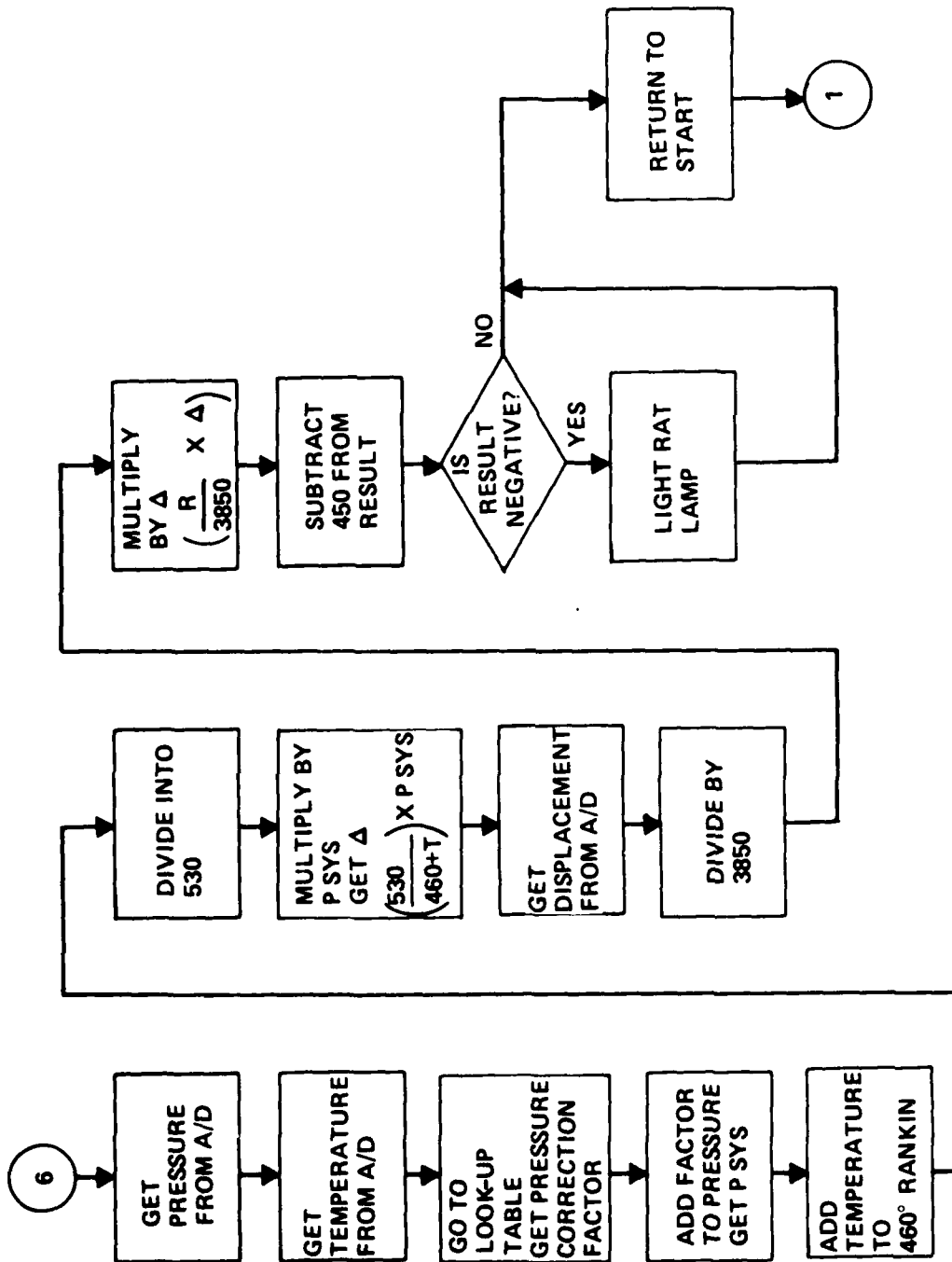
RUDDER ROUTINE



RESERVOIR ROUTINE



RAT ROUTINE



APPENDIX I

HYCOS BATTERY ANALYSIS AND CHARGER WIRING DIAGRAM

The Hydraulic Checkout/Diagnostic Monitoring System (HYCOS) includes the following nickel-cadmium batteries:

- +5V Battery; 4 Series-connected, 1 A-H, G.E. cells (Gold Top type X GCR 1.0ST)
- +3.6V Battery; 3 Series-connected, 100 mA Hr GE cells (Gold Top type X GCR 100ST)
- -6V/-4.8V Battery; 5 Series-connected (-6.0V) cells with a 4-cell tap for -4.8V. Cells are the same as the +3.6V battery cells.

These batteries are located within the HYCOS panel (box) and are not readily accessible.

I.1 GENERAL HYCOS POWER UTILIZATION

When installed in an aircraft, HYCOS uses 115 VAC, 400 Hz ship's power (when "on") to support HYCOS functional requirements and to recharge the batteries. When ship's power is "off" or otherwise not available, HYCOS power is supplied by the batteries.

A typical checkout test will last about 1/2 to 1 minute. It is estimated that up to six of these tests could be performed over a period of up to 6 weeks where no battery charging takes place.

I.2 BATTERY DISCHARGE

I.2.1 +5V Battery

This battery (now) only supplies power during the actual test period. Loads on this battery include:

- All power to logic circuits which, based on H. Dreksler's analysis, is approximately 500 mA

- Power for a maximum of five 'grain-of-wheat' lamps/test at approximately 50 mA each, or 250 mA total
- Power for two fiber optic light source lamps at approximately 750 mA each, or 1500 mA total.

The total current drain on the +5 battery during the test period is approximately 2.25 A. Assuming a realistic maximum test period of one (1) minute, the energy output per test is approximately 3.75% of the nameplate capacity of the battery.

1.2.2 +3.6V Battery

This battery is used to sustain the CMOS RAM (M5101). It supplies current of between 2-200 μ A essentially all the time. Assuming a nominal current of 100 μ A, the battery energy output would be approximately 2.4 mA-hr per day. At this rate the 100 mA-hr battery, if initially fully charged, could operate up to about 6 weeks without charging.

1.2.3 -6V/-4.8V Battery

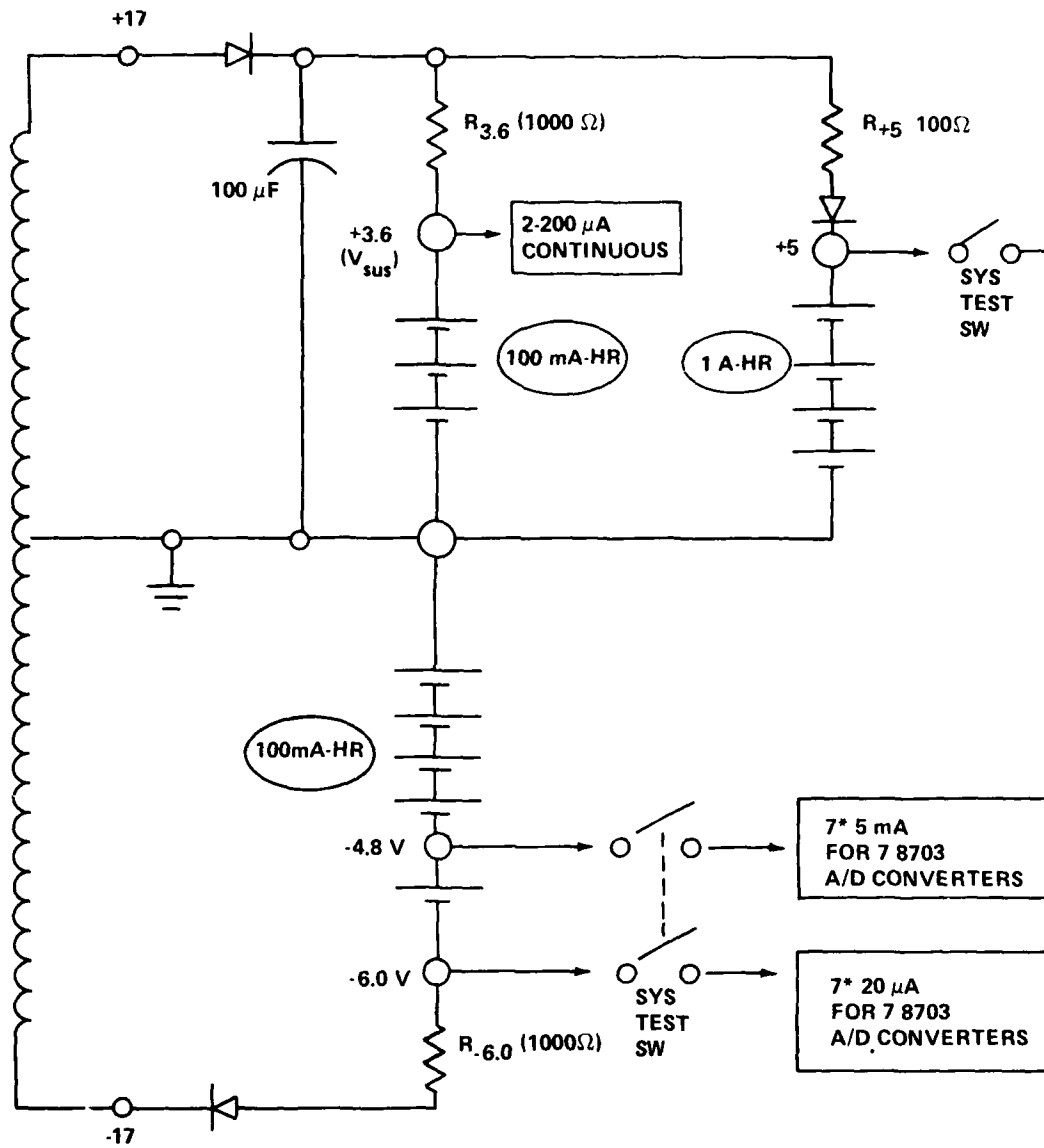
This battery supplies power only during the actual test period to seven (7) 8703 A/D converters. The -6V output supplies approximately 7 x 20 μ A or 140 μ A, while the -4.8V output, obtained by tapping into the -6V battery, supplies 7 x 5 mA or 35 mA. Thus, the cells that form the -4.8V battery have a total current drain of 35 mA + 140 μ A, or essentially 35 mA. On the basis of a one-minute test period, this -4.8V battery supplies about 0.6% of the nameplate capacity per test, while the additional cell used to obtain the -6V output supplies negligible energy/test (0.0023%/test).

On the basis of energy output requirements, each HYCOS battery would appear to be adequately sized. Even accounting for self-discharge of the batteries, which could range up to a loss of perhaps 50% capacity over a 6-week period (at normal storage temperatures of about 20°C), the batteries should have adequate capacity.

Note: The +3.6V battery, which is supplying memory-sustaining power while the other batteries are idle, should be marginally acceptable for a 6-week storage.

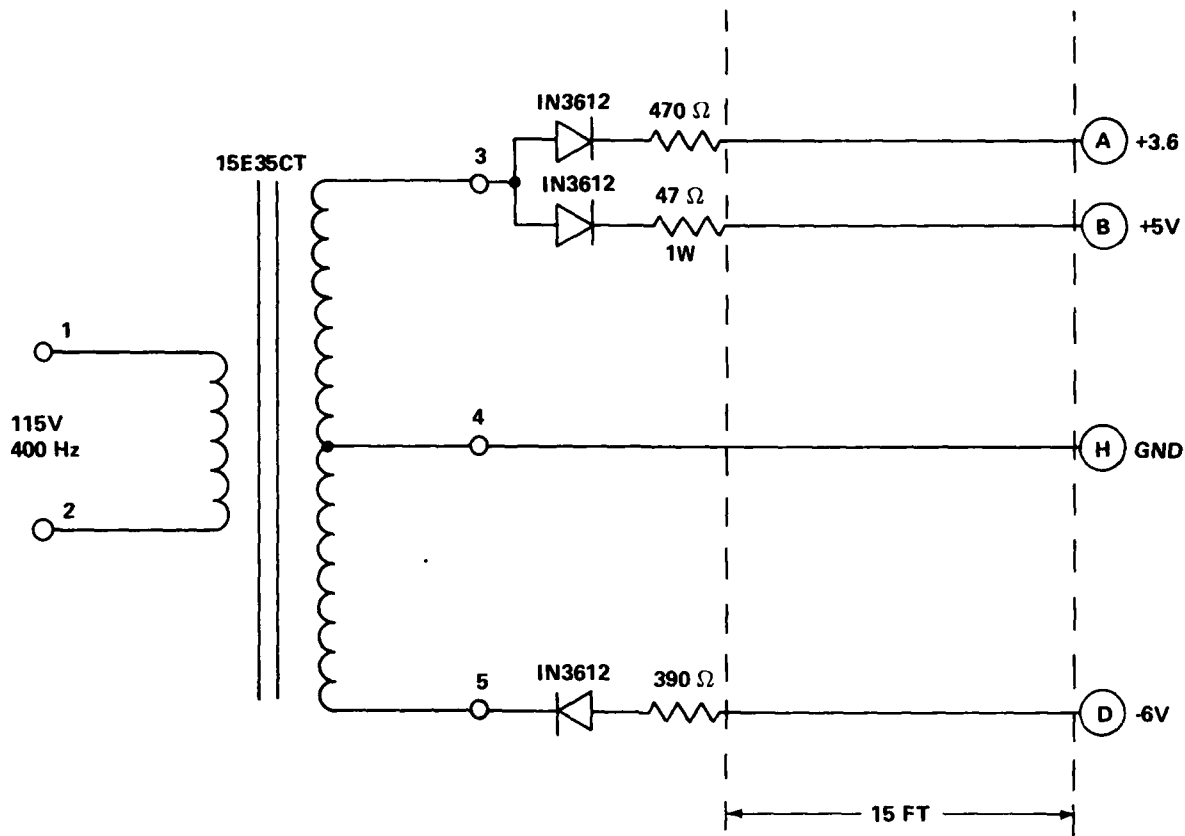
1.3 BATTERY CHARGING

The circuit used for battery charging is shown in Fig. I-1. Figure I-2 depicts the HYCOS Battery Charger. The recommended (by G.E.) constant current charge rate for the Gold Top batteries is between C/10 and C/20. These batteries can supposedly safely handle continuous overcharge at these rates.



R80-2038-103(T)

Figure I-1. Battery charging circuit.



R80-2038-104(T)

Figure I-2. HYCOS battery charger.

A fully depleted battery, in order to be fully charged at C/10, will require 14-18 hr of charge time and 30-35 hr of charge time at C/20. It is unlikely that HYCOS batteries will be provided this much time if charging is to be accomplished during aircraft flight.

Based on the questionable time available for recharge, it is recommended that the HYCOS panel be equipped with an externally accessible connector (Fig. I-3) that provides direct connection to battery + and - terminals, or connections to the input of the HYCOS battery charging circuit (i.e., 115 VAC, 400 Hz to transformer primary). The preferred approach is direct connection to the battery terminals. This connector would then allow :

- Monitoring or a status check on battery voltages
- Battery charging using a dedicated ground support charger.

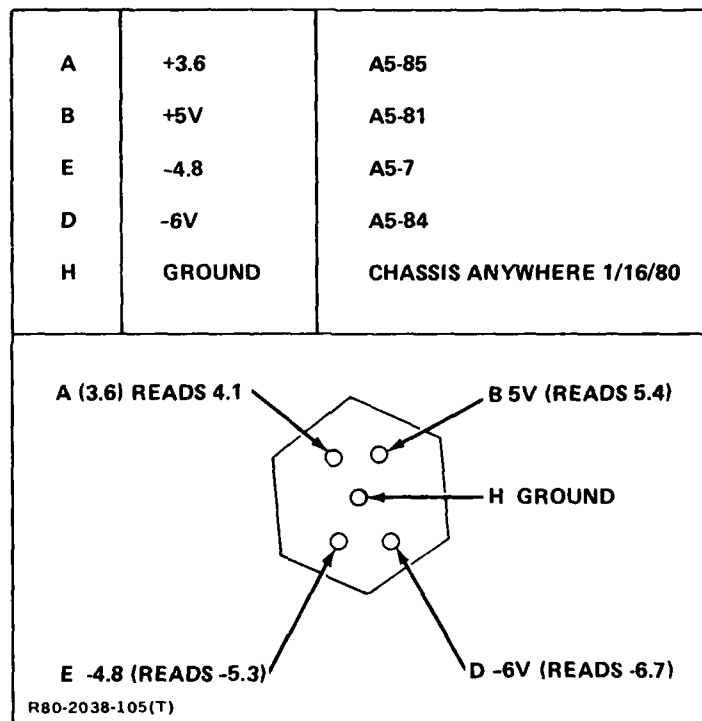


Figure I-3. Battery Test Panel Connector Interface.

APPENDIX J

SYSTEM INSTALLATION AND VEHICLE PHOTOS

PHOTO NO.	DESCRIPTION
J- 1	View showing temperature-compensated pressure switch mounted to 15 cubic inch pneumatic bottle.
J- 2	Port keel area showing quiescent flow sensor, system pressure switch, and pressure filter remote reading Delta P indicator.
J- 3	View showing temperature transducer in return line to reservoir.
J- 4	Combined system reservoir showing remote reading potentiometer and desiccant saturation detection unit.
J- 5	Port keel area showing probe-type temperature switch in pump case drain line. Also shown is system pressure switch.
J- 6	Port keel area showing probe-type temperature switch in pump case drain line. Also shown is system pressure switch. (Same as J-5.)
J- 7	Case drain filter showing APM multicator installation (provisions for fluid sampling case drain line).
J- 8	View looking forward at 30-cubic inch gear door dump bottle with temperature-compensated pressure switch on pedestal.
J- 9	View showing duct access area where HYCOS panel is to be mounted. Wire bundles are shown in area.
J-10	View showing bottom of Ram Air Turbine Accumulator with temperature and pressure transducer.
J-11	Forward port keel area showing Ram Air Turbine Accumulator with linear displacement transducer.
J-12	View showing bottom of Ram Air Turbine Accumulator with temperature and pressure transducer. (Same as J-10.)
J-13	Closeup of displacement rod on Ram Air Turbine Accumulator.
J-14	Closeup of displacement rod on Ram Air Turbine Accumulator (Same as J-13.)

PHOTO NO.	DESCRIPTION
J-15	View looking forward at RAT accumulator mounting.
J-16	Surface temperature switch mounted on flight control backup module.
J-17	Surface temperature switch mounted on flight control backup module (Same as J-16.)
J-18	Rudder actuator flow sensor on pressure line.
J-19	Rudder actuator flow sensor on pressure line. (Same as J-18.)
J-20	Pump case drain flow sensor installation.
J-21	A-6E Mod 229 flight test vehicle.
J-22	Plane Captain interrogating HYCOS system.
J-23	Closeup on HYCOS Display panel in flight test vehicle.

NADC 81073-60



Photo J-1

NADC 81073-60

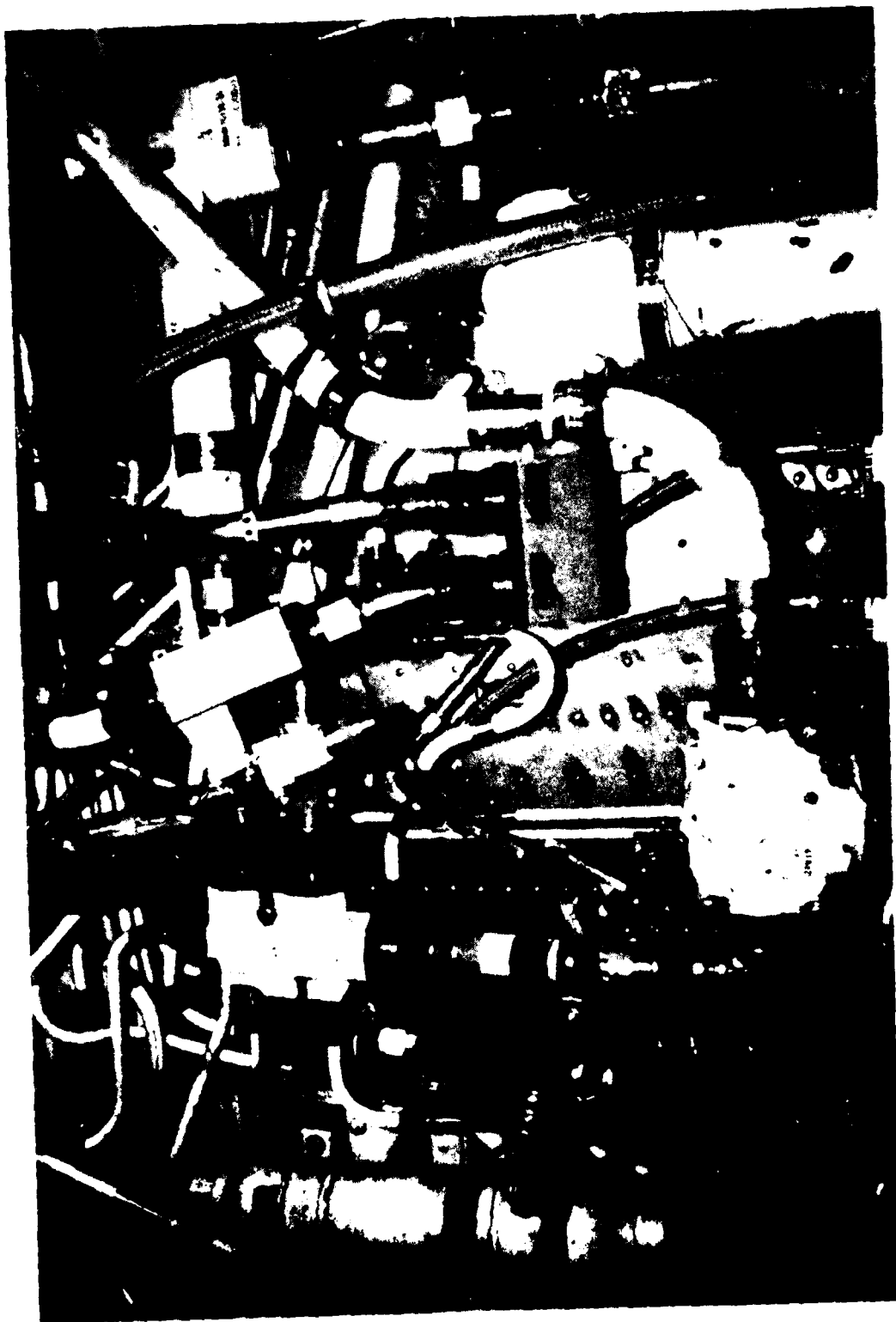


Photo J-2

NADC 81073-60



Photo J-3

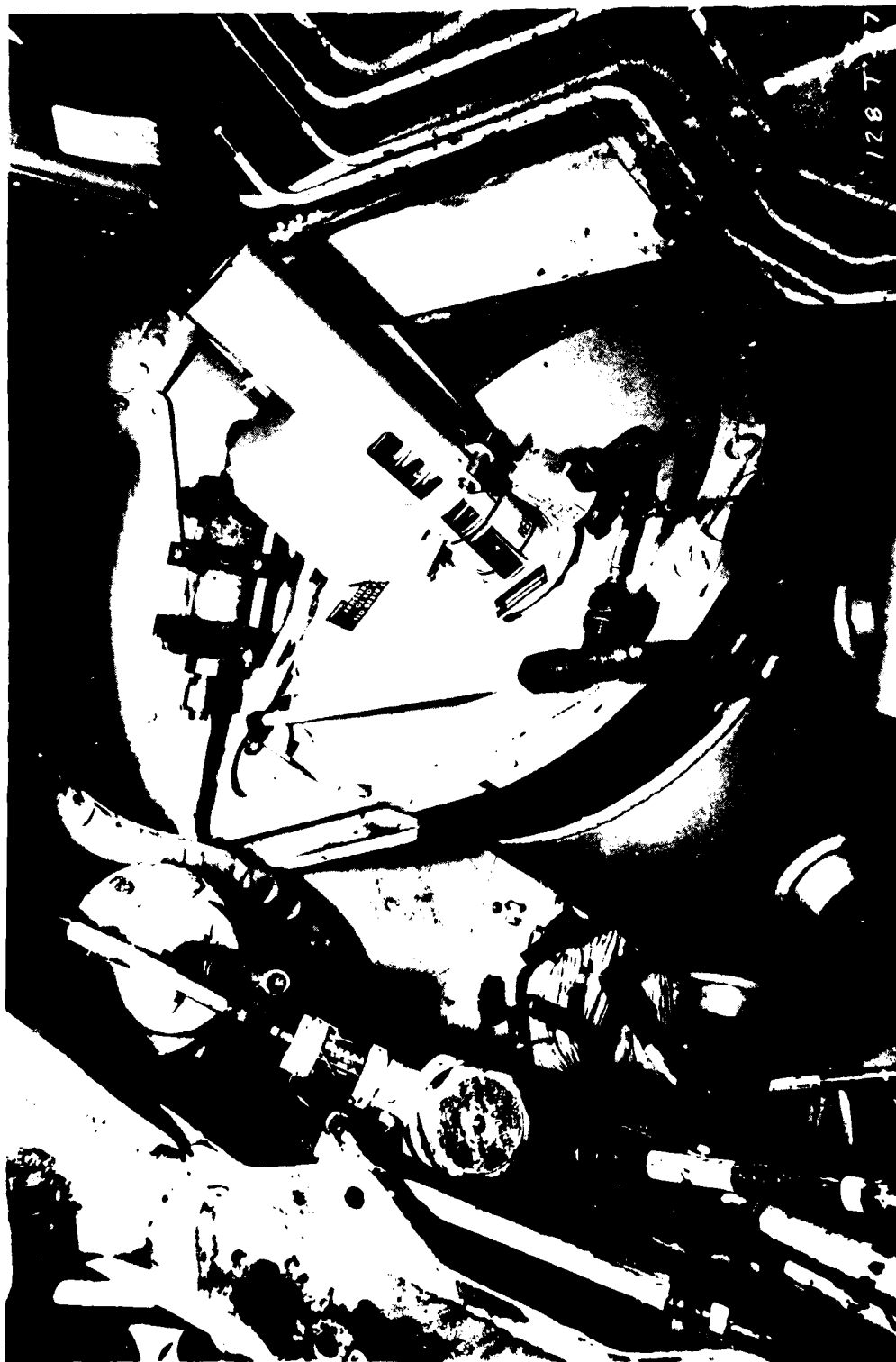


Photo J-4

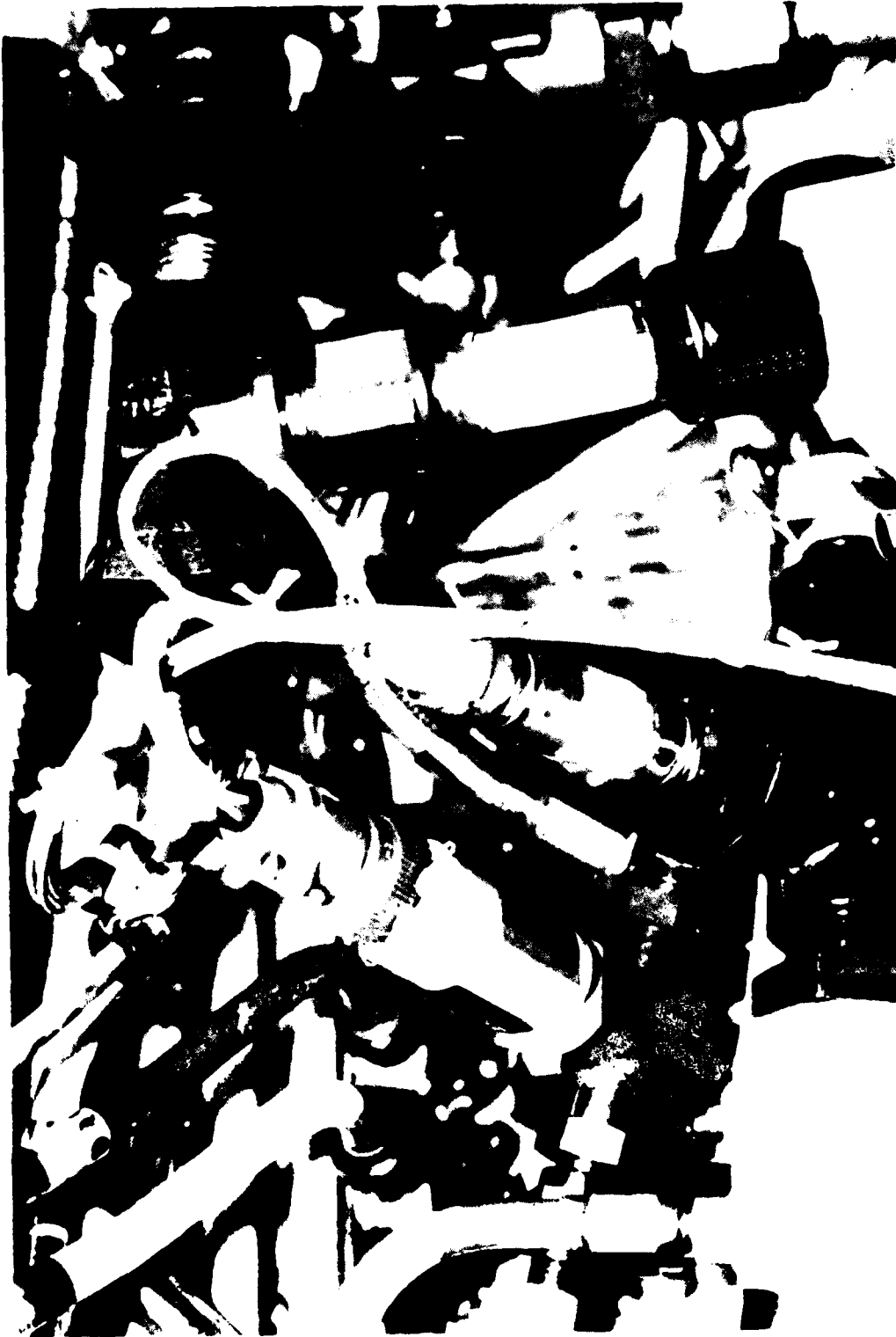


Photo J-5

NACC 81073-60



Photo J-6



Photo J-7

NADC 81073-60

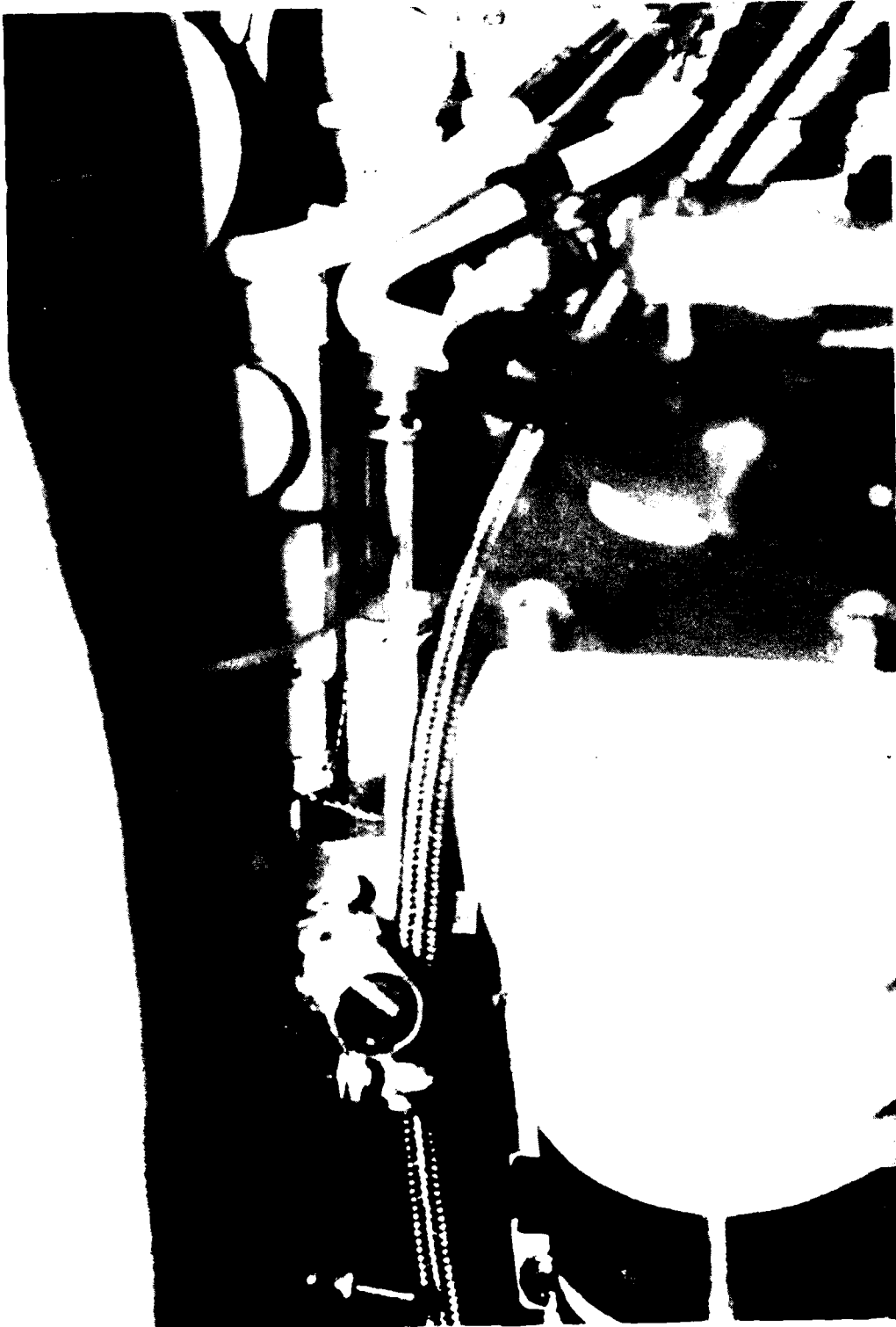


Photo J-8

NADC 81073-60



Photo J-9

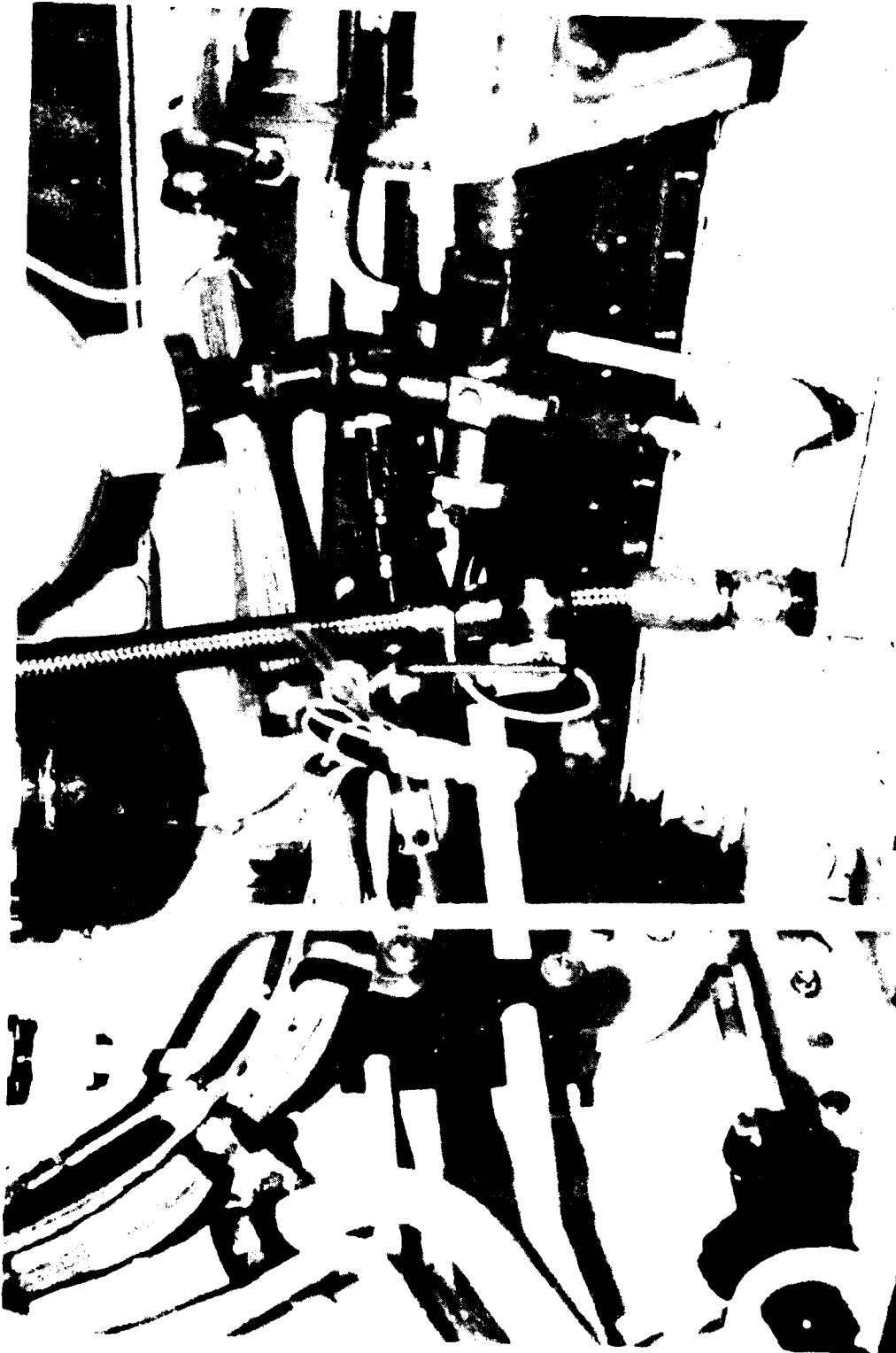


Photo J-10

NADC 81073-60

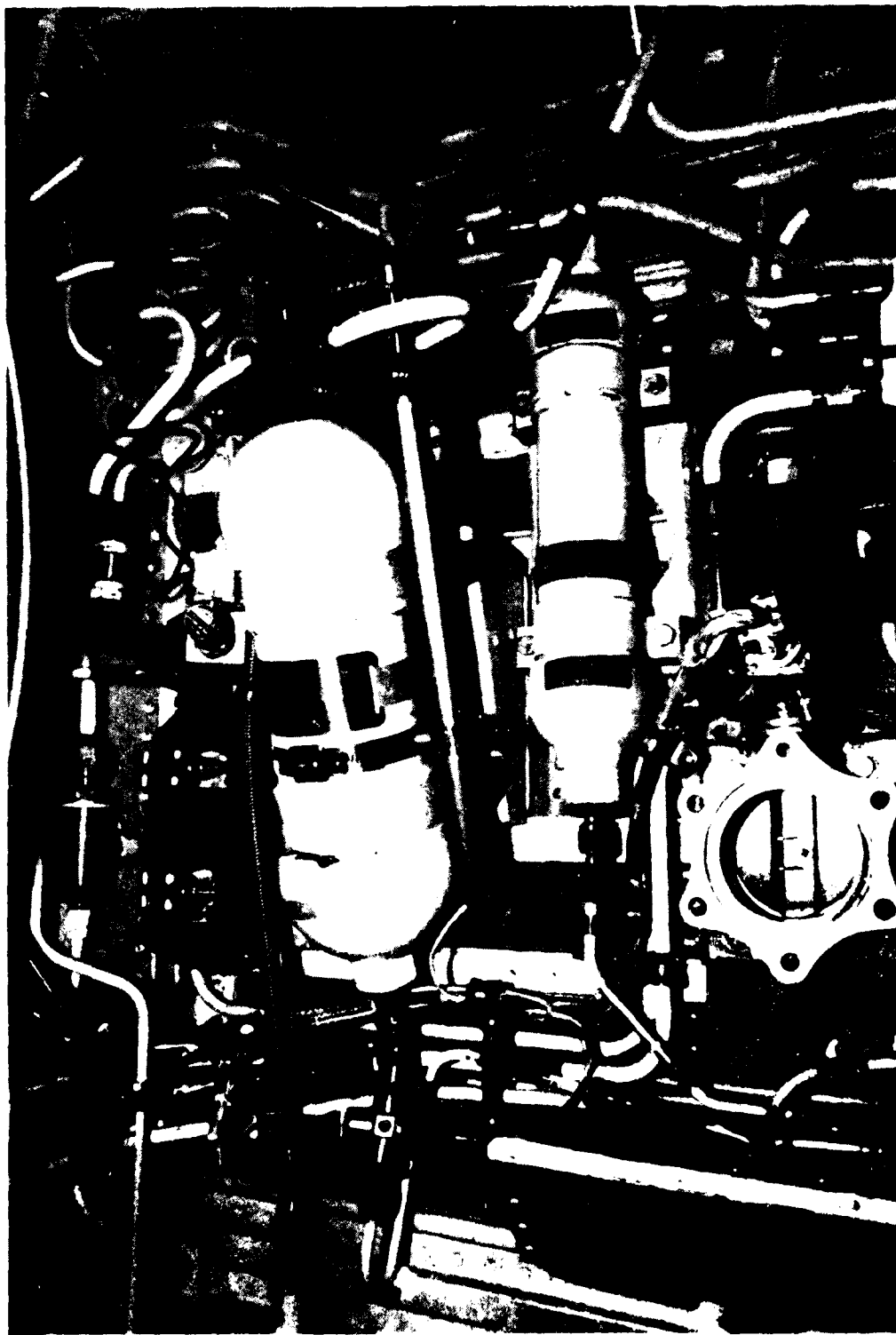


Photo J 11

NADC 81073-60

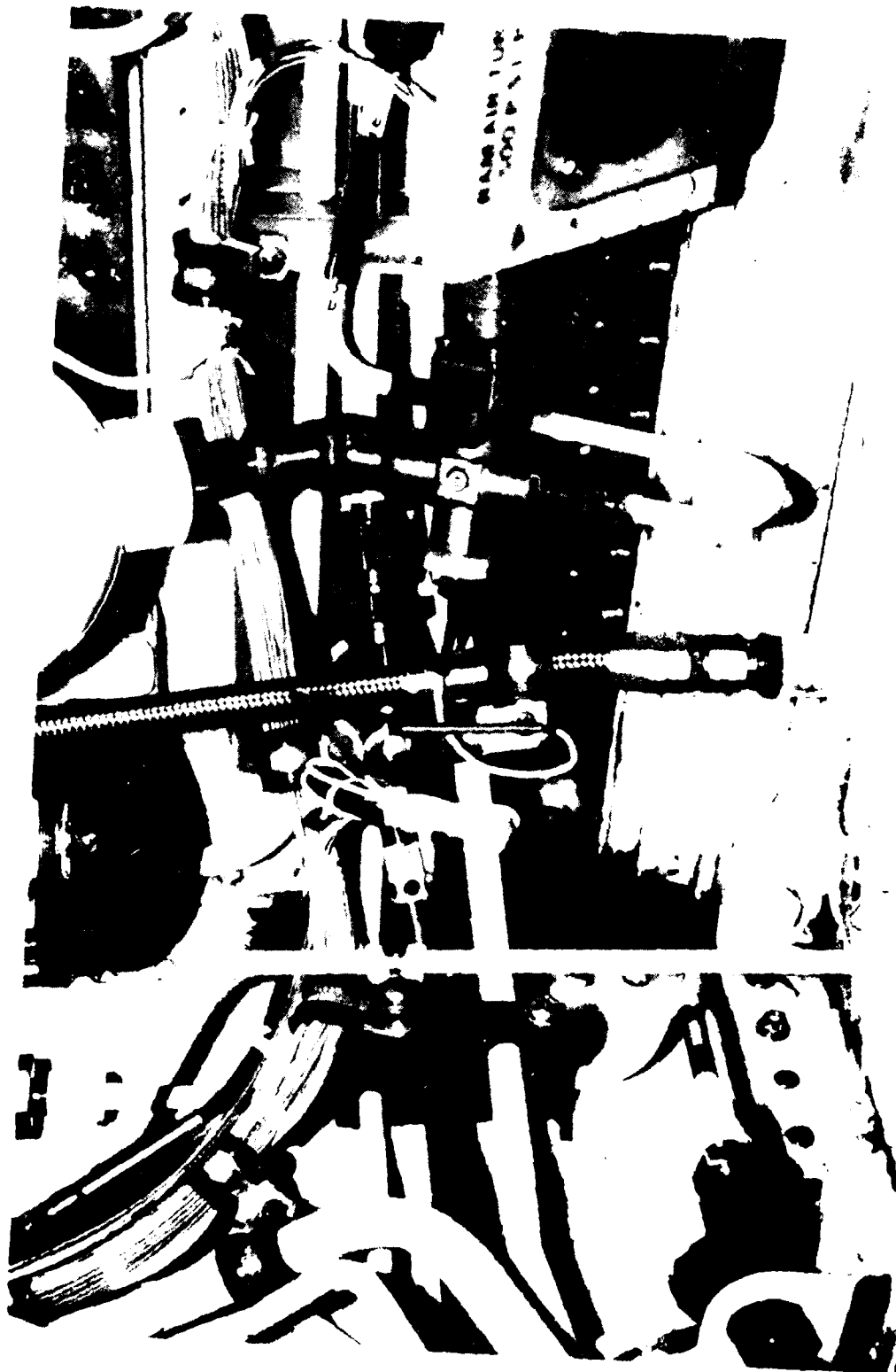


Photo J.12



Photo J-13

NADC 81073-60



Photo J-14

NADC 81073-60

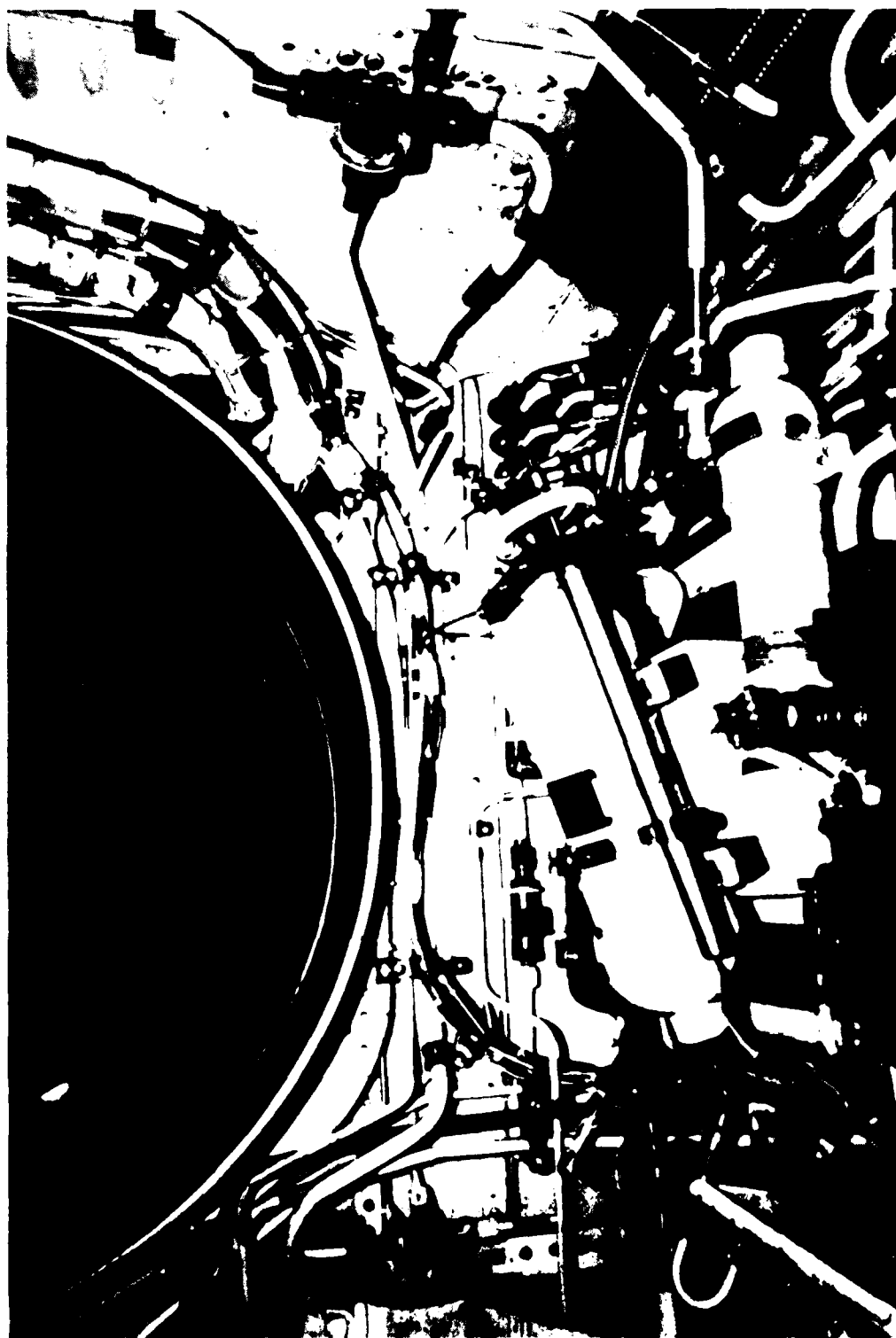


Photo J 15

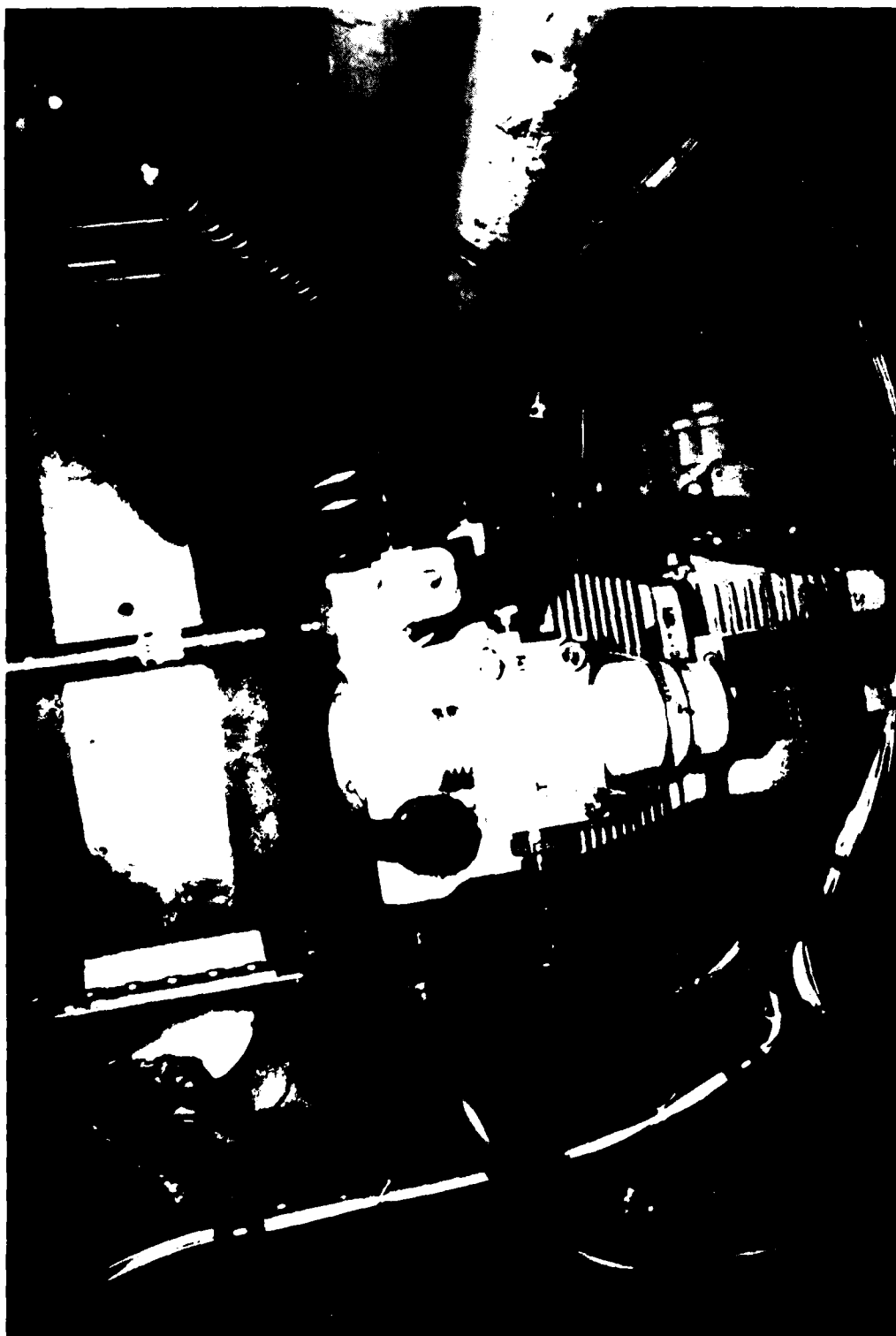


Photo J-16

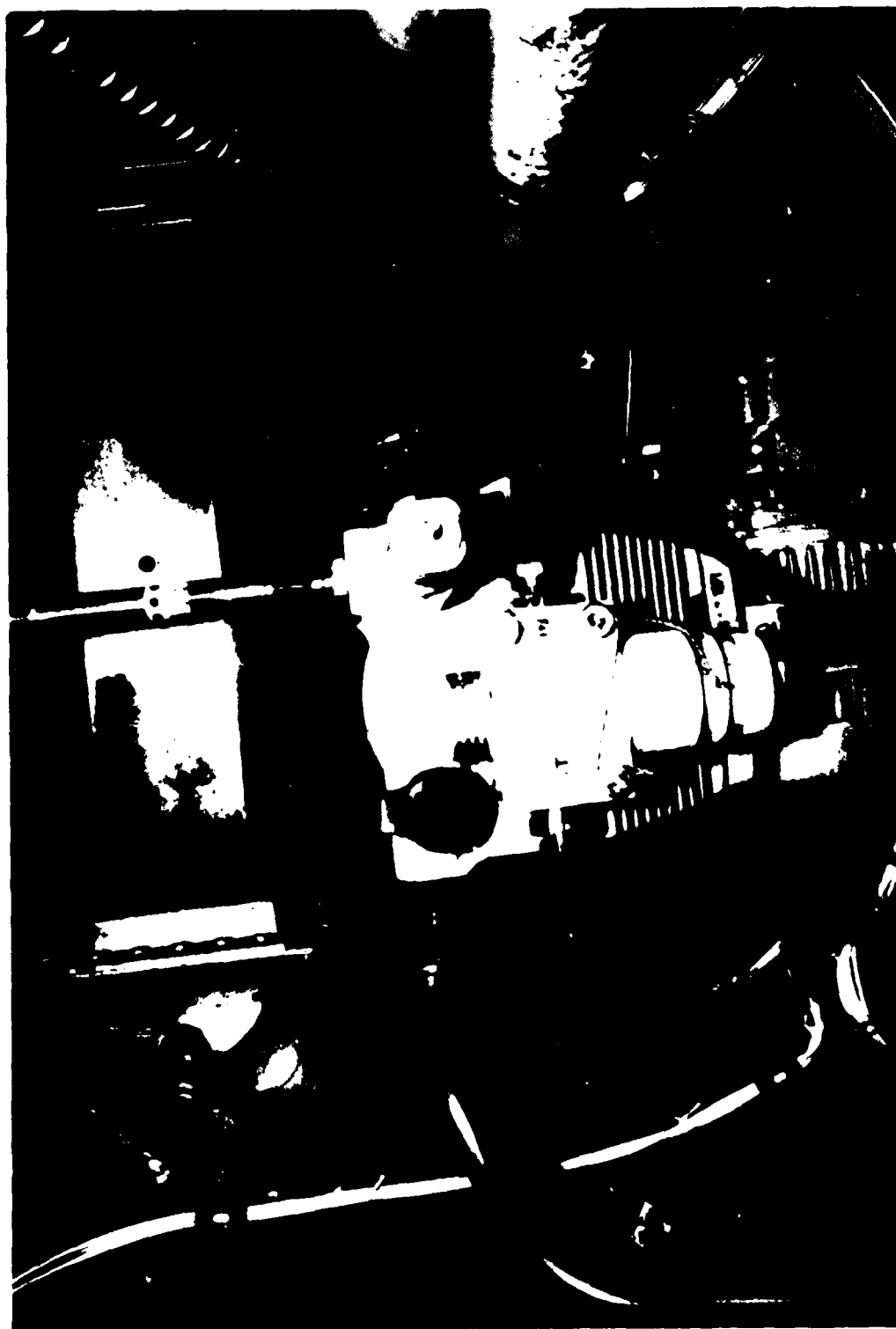


Photo J-17

NADC 81073-60

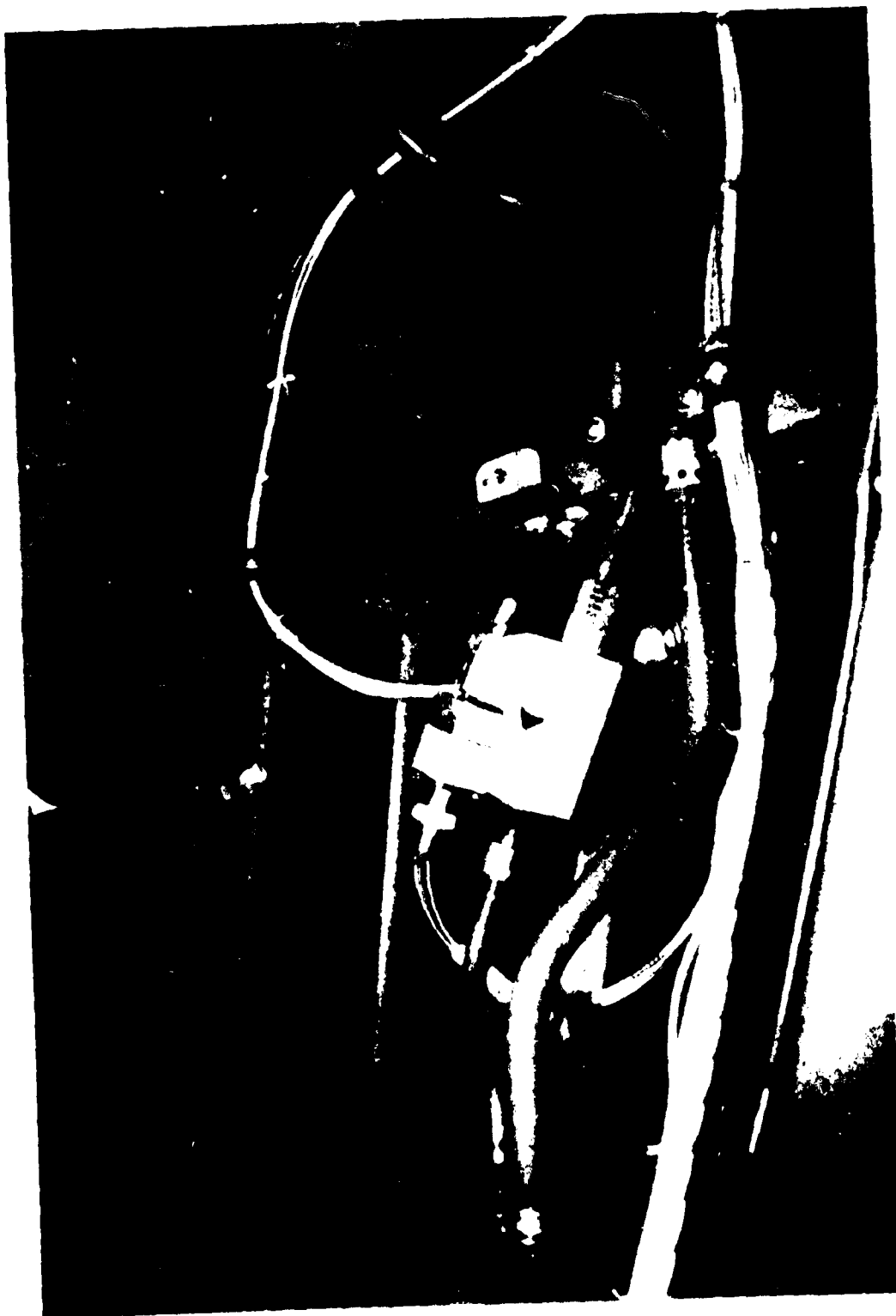


Photo J-18

NADC 81073-60

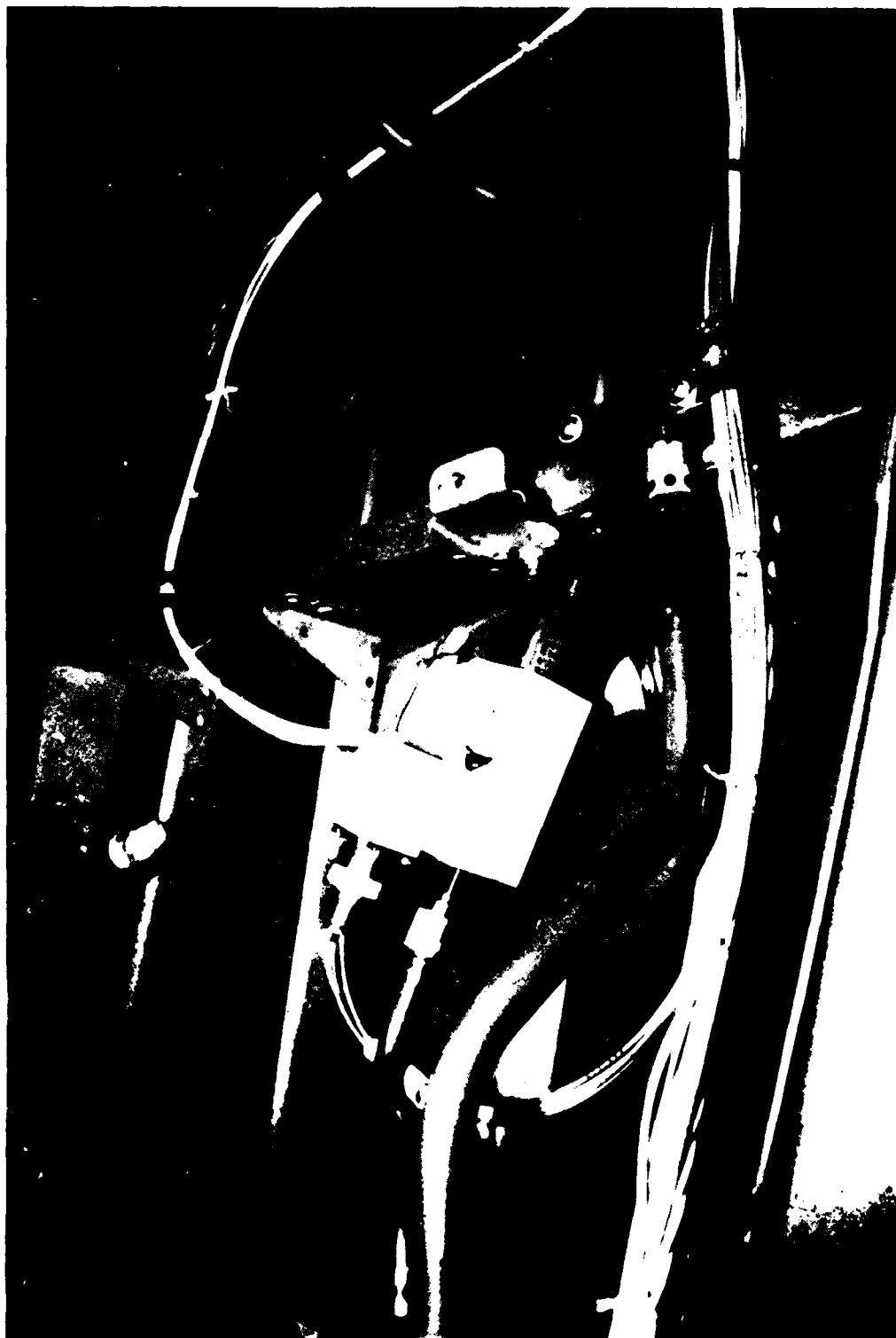


Photo J-19

NADC 81073-60



Photo J-20



Photo J-21

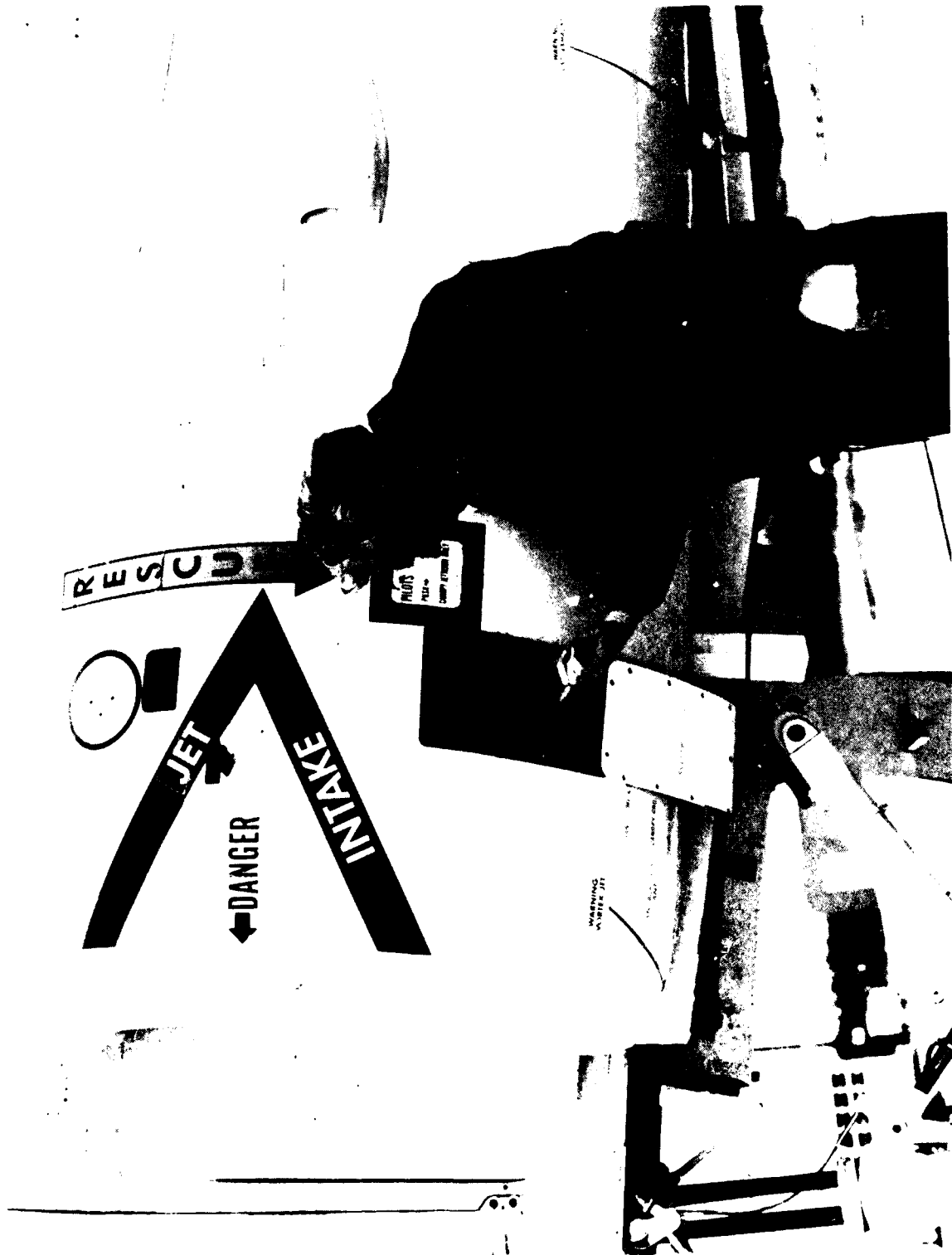
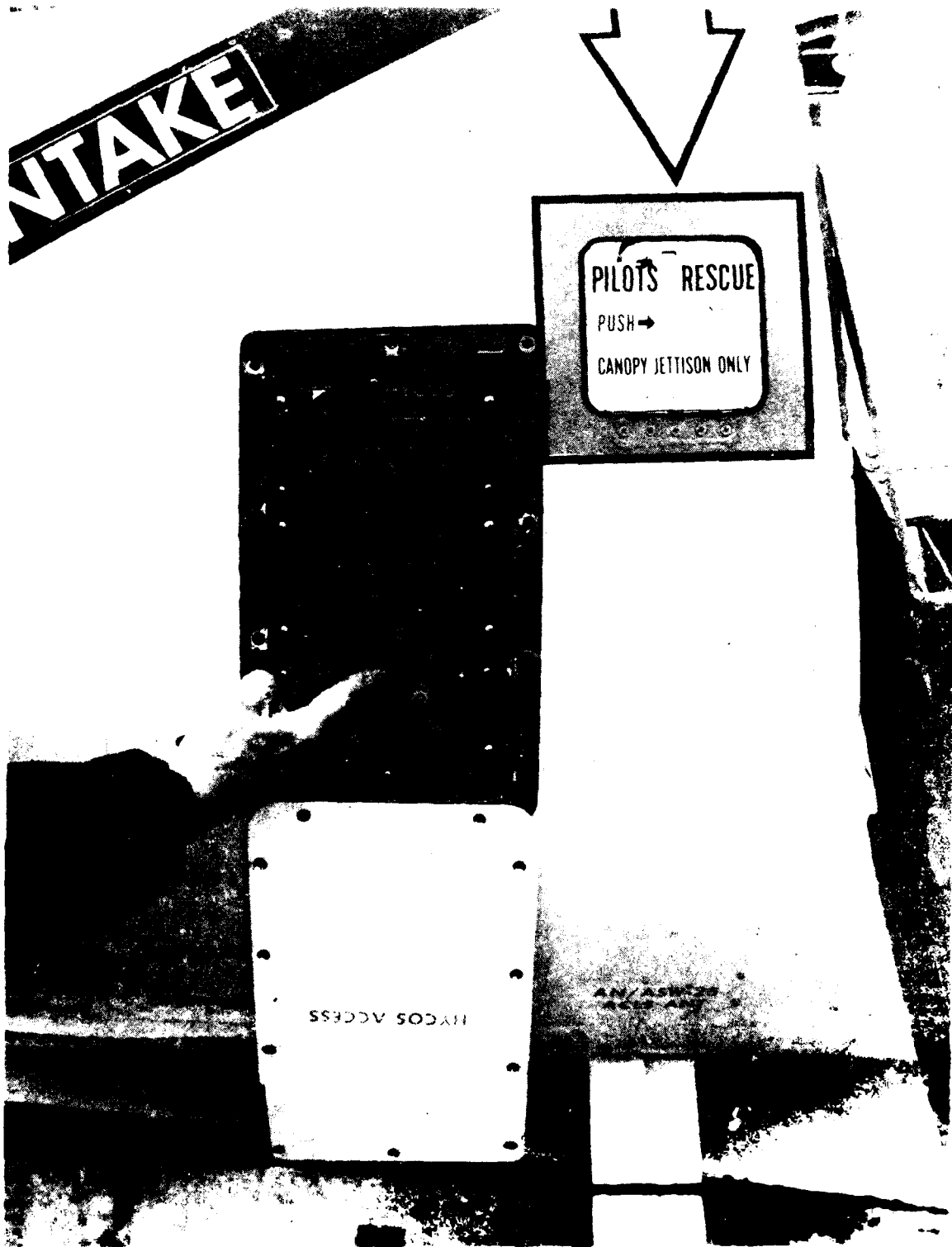


Photo J-22



AD-A100 730

GRUMMAN AEROSPACE CORP BETHPAGE NY
HYDRAULIC DIAGNOSTIC MONITORING SYSTEM.(U)
MAR 81 J J DUZICH

F/G 14/2

N62269-78-C-0041

UNCLASSIFIED

NADC-TR-81073-60

NL

4 OF 4

ADA
F/D-30



END
DATE
FILMED
7-81
DTIC

NADC 81073-60

APPENDIX K
MICROPROCESSOR PROGRAM

NADC 81073-60

ASM48 HVCOS SRC TITLE (HVCOS - A6 REV 18 1/19/80) PRINT (LP)

1515-II MCS-48/UPI-41 MACRO ASSEMBLER V2.0
HVCOS - A6 REV 18 1/19/80

PAGE 1

LOC	OBJ	SEQ	SOURCE STATEMENT
0000		1	ORG 0H
0000 E5		2	SEL MB0 ; INITIAL CONDITION
0001 C5		3	SEL RB0 ; MEMORY AND REGISTER BANK 0
		4	; EXECUTIVE ROUTINE
		5	; ROUTINE TO BE FOLLOWED EVERY TIME POWER IS
		6	; APPLIED WE CHECK TO SEE IF CIRCUIT TEST
		7	; SWITCH IS IN THE DOWN POSITION WHICH GENERATES
		8	; (T0). THIS SENDS THE PROCESSOR TO THE SEQUENCE
		9	; LOOP AND CHECKS TO SEE IF ALL THE RED LAMPS ARE
		10	; WORKING AND IF THE MICROPROCESSOR IS FUNCTIONAL
		11	; IF SYSTEM TEST SWITCH IS IN THE DOWN POSITION WE DO
		12	; A SYSTEM TEST. IF THE PRESSURE SWITCH IS ON WE DO A
		13	; RUDDER CHECK FOLLOWED BY AN OVER TEMPERATURE TEST.
		14	; A RESERVOIR LEVEL AND LEAK TEST, AND FINALLY A RAT
		15	; TEST. IF THE PRESSURE SWITCH IS OFF WE DO A RESERVOIR
		16	; AIR TEST.
		17	
0002 80		18 START	MOVX A, 000H ; DISABLE BUS
0003 2310		19	MOV A, #10H ; DISABLE MEMORY
0005 3A		20	OUTL P2, A ; DISABLE MEMORY
0006 27		21	CLR A ; SET INITIAL CONDITIONS
0007 39		22	OUTL P1, A ; INITIAL CONDITIONS
0008 17		23	INC A ; RESET FF
0009 39		24	OUTL P1, A ; " "
000A 39		25	OUTL P1, A ; EXTRA SHOT
000B 3616		26	JT0 S0NCE ; IF T0 DO SEQUENCE ROUTINE
000D 5625		27	JT1 RMLD ; IF T1 DO AIR ROUTINE
000F 17		28	INC A ; CHECK STATE
0010 39		29	OUTL P1, A ; OF SYSTEM
0011 00		30	INS A, BUS ; TEST SWITCH
0012 3225		31	JB1 RMLD ; IF SWITCH IS ON1 DO RAM LOAD
0014 0402		32	JMP START
		33	
		34	; SEQUENCE SUBROUTINE
		35	; THIS SUBROUTINE WILL LIGHT ALL THE LAMPS BY BLOCKS,
		36	; FIRST THE PUMPS (5 LAMPS), THEN RESERVOIR (4 LAMPS),
		37	; ETC LAMPS WILL STAY ON FOR 1/2 SECOND THEN SEQUENCE
		38	; TO NEXT BLOCK
		39	
		40	
0016 2300		41 S0NCE	MOV A, #000H ; OUTPUT TO GET P27 AND TO
0018 3A		42	OUTL P2, A ; DISABLE MEMORY FROM BUS
0019 2301		43	MOV A, #01H ; START BUS AT BEGINNING
001B 02		44 TSTUT	OUTL BUS, A ; OUTPUT TO BUS TO LIGHT LAMPS
001C 0A32		45	MOV R2, #32H ; PRELOAD R2 FOR 1/2 SECOND TIMING
001E 0B		46	MOV R3, A ; SAVE POSITION OF LAMPS IN R3
001F 3438		47	CALL MS10 ; GET 1/2 SECOND TIMING SUBROUTINE
0021 0B		48	MOV A, R3 ; RESTORE ACCUMULATOR
0022 E7		49	RL A ; MOVE BIT IN ACCUM TO LEFT
0023 041B		50	JMP TSTUT ; REPEAT TEST
		51	
		52	; RAM LOAD SUBROUTINE

NADC 81073-60

ISIS-II MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 2

LOC	OBJ	SEQ	SOURCE STATEMENT
		53	; IF HYDRAULIC SWITCH IS AT A "0" WE GO TO THE AIR ROUTINE
		54	; IF AT A "1" WE DO RESERVOIR ROUTINE
		55	; (FOLLOWING THE RUDDER ROUTINE)
		56	
0025	2302	57	RHLD: MOV A, #02 ; ENABLE STATE OF HYDRAULIC SWITCH
0027	39	58	OUTL P1, A ; TO BUS
0028	08	59	INS A, BUS ; AND INPUT TO ACCUMULATOR
0029	1250	60	JBB RUDDER ; IF A "1" DO RUDDER ROUTINE
		61	; AIR ROUTINE:
		62	; THE SYSTEM IS UNPRESSURIZED, THE SYSTEM TEST SWITCH IS
		63	; UP OR DOWN. TEMPERATURE T1 AND DISPLACEMENT R1 ARE IN
		64	; MEMORY LOCATIONS 0 & 1 AND 2 & 3 RESPECTIVELY. THE PRESENT
		65	; TEMPERATURE T2 IS INPUTTED FROM THE TRANSDUCER THRU ITS A/D
		66	; CONVERTER AND CHECKED FOR OVERTEMP. THEN T1 IS SUBTRACTED FROM
		67	; T2 TO GIVE DELTA T (ΔT). ΔT = T2 - T1. ΔT IS MULTIPLIED BY
		68	; CONSTANT 3.78 TO GET TEMPERATURE CORRECTION FACTOR. THE RESULT
		69	; IS ADDED TO OR SUBTRACTED FROM R1 DEPENDING ON THE SIGN OF ΔT
		70	; NEXT ADD 400 TO R1 TO ALLOW FOR A 1 INCH DISPLACEMENT AND GET
		71	; R1'. DISPLACEMENT R2 IS INPUTTED FROM THE RESERVOIR POT AND ITS
		72	; A/D. R1' IS SUBTRACTED FROM R2. IF RESULT IS POSITIVE DISPLACE-
		73	; MENT WAS MORE THAN 1 INCH AND WE LIGHT THE AIR LAMP.
		74	
		75	; EXAMPLE
		76	
		77	; ASSUME T1=135 C T2=21 C
		78	; R1=5500 R2=5600
		79	
		80	; AIR=R2 - (R1 + 400 + (T2 - T1) X 3.78)
		81	
		82	; R1 + 400 + (T2 - T1) X 3.78 = R1'
		83	
		84	; T2 - T1 = 21 - 135 = -114
		85	
		86	; -114 X 3.78 = -430
		87	
		88	; AIR = 5600 - (5500 + 400 - 430)
		89	; = 5600 - 5470
		90	; = + 130
		91	
		92	; ANSWER IS POSITIVE SO AIR LAMP LIGHTS
		93	
		94	; START WITH EQUATION (T2-T1) X 3.78
002B	249A	95	CALL TMPOK ; GET T2 FROM TEMP A/D CONVERTER
		96	; INPUT TO ACCUM AND R2
		97	; CHECK FOR OVERTEMP
002D	27	98	CLR A ; INITIAL CONDITION
002E	AD	99	MOV R5, A ; " "
		100	; R5 SETS UP MEMORY ADDRESS
002F	BE30	101	MOV R6, #30H ; " "
		102	; R6 OUTPUT USED FOR READ
0031	39	103	OUTL P1, A ; CLEAR PORT 1 FROM BUS
0032	345C	104	CALL LSD ; GET T1 FROM MEMORY
0034	34B2	105	CALL SBTCT ; ΔT = T2 - T1
0036	B901	106	MOV R1, #01H ; SETTING UP SIGN OF SUBTRACTION
0038	B63B	107	JF0 NEG1 ; IF NEGATIVE PEG 1 = 1

NADC 81073-60

1515-II MCS-48/UP1-41 MACRO ASSEMBLER V2.0
 MYCOS - A6 REV 18 1/19/80

PAGE 3

LOC	OBJ	SEQ	SOURCE STATEMENT
003A C9	108	DEC R1	; ELSE REG 1 = 0
003B 543A	109	CALL LKUP1	; GET BINARY VALUE FOR %T X 3.78
	110		; BINARY RESULT STORED IN REGISTER 4 RESISTOR R1 IS IN MEMORY
	111		; AND WE WILL ADD IT TO 400 (= 00H) AND %T VALUE
003D 345C	112	CALL LSD	; GET R1 FROM MEMORY
003F 0308	113	ADD A, #00H	; R1 + 424 (COULD NOT GET 400 EXACT)
0041 29	114	XCH A, R1	; EXCHANGE SUM WITH SIGN OF %T
0042 53FF	115	ANL A, #0FFH	; AND TO SEE IF 0
0044 C64C	116	JZ POS1	; IF 0 IT WAS POSITIVE
	117		; ELSE NEGATIVE
0046 FC	118	MOV A, R4	; GET %T
0047 37	119	CPL A	; ONES COMPLEMENT
0048 17	120	INC A	; 2'S COMPLEMENT
0049 69	121	ADD A, R1	; SUM - %T
004A 044E	122	JMP SUM1	; SUBTRACTION COMPLETE
004C FC	123	MOV A, R4	; GET %T
004D 69	124	ADD A, R1	; SUM + %T
004E AA	125	MOV R2, A	; R1 INTO REG 2
004F 2320	126	MOV A, #20H	; R2 A/D
0051 34A9	127	CALL GONOGO	; INTO ACCUM
0053 2A	128	XCH A, R2	; SWAP R2 AND R1
0054 34B3	129	CALL SBTCT	; R2 - R1
0056 8682	130	JF0 START	; IF NEGATIVE NO ERROR
	131		; REPEAT WHOLE OPERATION
0058 2307	132	MOV A, #07H	; ELSE LIGHT
005A 39	133	OUTL P1, A	; AIR LAMP
005B 0402	134	JMP START	; REPEAT WHOLE OPERATION
	135		
	136		
	137		; RUDDER CIRCUITRY
	138		; TAKE ANALOG OUTPUTS OF 2 POTS A/D CONVERT.
	139		; SUBTRACT FROM EACH OTHER THEN SUBTRACT DIFFERENCE
	140		; FROM A GIVEN TOLERANCE IF DIFFERENCE IS
	141		; TOO HIGH LIGHT RUDDER LAMP
	142		
005D 2318	143	MOV A, #18H	; RUDDER POT DATA
005F 34A9	144	CALL GONOGO	; FROM A/D
0061 AA	145	MOV R2, A	; PUT INTO R2
0062 2338	146	MOV A, #38H	; RUDDER PEDAL DATA
0064 34A9	147	CALL GONOGO	; FROM A/D
0066 34B3	148	CALL SBTCT	; R2-A=DELTA
0068 23F4	149	MOV A, #0F4H	; 2'S COMPLEMENT OF 12
006A 6A	150	ADD A, R2	; SUBTRACT 12 FROM DELTA
006B E670	151	JNC RSRVR	; IF NO CARRY RUDDERS OK
006D 2305	152	MOV A, #05H	; CALL RUDDER LAMP
006F 39	153	OUTL P1, A	; AND LITE IT
	154		
	155		
	156		
	157		
	158		; RESERVOIR ROUTINE
	159		; DUE TO SETTING OF POT THE FOLLOWING CONSTANTS ARE USED
	160		; EACH BIT IS 53 OHMS 6700/127
	161		; SLOPE FOR NORMAL DISPLACEMENT IS 1.85 OHMS / DEGREE F =
	162		; 12.77 OHMS / DEGREE C = 16 DEG C / BIT

NADC 81073-60

ISIS-II MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 4

LOC	OBJ	SEQ	SOURCE STATEMENT
		163	; 5420 OHMS AT -54 C =LEVEL MINIMUM
		164	; 5070 OHMS AT -54 C =LEAK MINIMUM
		165	; TEMPERATURE TRANSDUCER READS IN DEG C AND IS SET SO THAT
		166	; -54C IS EQUAL TO 0. EQUATIONS ARE
		167	;
		168	; LEVEL = 5420 + 3.33 X ZT - R (IF POSITIVE WE LIGHT LAMP)
		169	; LEAK = 5070 + 3.33 X ZT - R (IF POSITIVE WE LIGHT LAMP)
		170	
		171	RSVR:
0070	B000	172	MOV R5, 00H ; INITIAL ADDRESS OF MEMORY
0072	BE10	173	MOV R6, 010H ; INITIAL CONDITION
0074	340A	174	CALL TMPCX ; GET TEMPERATURE. CHECK FOR
		175	; OVERTEMPERATURE. STORE IN R2 & R4
0076	3447	176	CALL BYTST ; PUT IN MEMORY LOCATIONS '0' & '1'
0078	F8	177	MOV R, R0 ; TEMP BACK TO ACCUM
0079	5450	178	CALL LKUP2 ; GET BINARY EQUIVALENT OF TEMP
		179	; AND STORE IN R4
007B	2320	180	MOV R, 0020H ; DISPLACEMENT VALUE
007D	3409	181	CALL GONOGO ; INTO ACCUM
007F	B002	182	MOV R5, 002H ; INITIAL CONDITIONS
0081	AA	183	MOV R2, R ; STORE DISPLACEMENT IN R2
0082	3447	184	CALL BYTST ; PUT DISPLACEMENT IN MEMORY
		185	; LOCATIONS "2" & "3"
0084	FC	186	MOV R, R4 ; GET % T
0085	34B3	187	CALL SBTCT ; DISPLACEMENT - ZT = ZR
0087	AC	188	MOV R4, R ; STORE % R IN R4
0088	B066	189	MOV R2, 066H ; 5420 OHMS
008A	34B3	190	CALL SBTCT ; 5420 - % R
008C	B69B	191	JF0 RAT ; IF F0 ZR > 5420
008E	2303	192	MOV R, 003H ; ELSE LIGHT RESERVOIR
0090	39	193	OUTL P1, R ; LEVEL LAMP
0091	B060	194	MOV R2, 0060H ; 5070 OHMS
0093	FC	195	MOV R, R4 ; GET % R
0094	34B3	196	CALL SBTCT ; 5070 - ZR
0096	B69B	197	JF0 RAT ; IF F0 ZR > 5070
0098	2300	198	MOV R, 0000H ; ELSE LIGHT RESERVOIR
009A	39	199	OUTL P1, R ; LEAK LAMP
		200	
		201	; RAT ROUTINE
		202	; THIS ROUTINE SOLVES THE EQUATION
		203	;
		204	; PPR = (R/3850) X (530/(T + 460)) X PSYS
		205	;
		206	; PSYS = PRESSURE READING + TEMPERATURE CORRECTION FACTOR
		207	; R = RESISTANCE IN OHMS
		208	; 3850 = RESISTANCE AT STP
		209	; 530 = 70 DEGREES F + 460 TO MAKE DEGREES RANKIN
		210	; T = MEASURED TEMPERATURE IN DEGREES F
		211	;
		212	; FIRST WE SOLVE FOR PSYS, AND STORE RESULT IN MEMORY. THEN WE
		213	; PERFORM 2 DIVISIONS, THEN 2 MULTIPLICATIONS. WE THEN SUBTRACT
		214	; 450 PSI FROM THE RESULT TO TEST IF OUR PRECHARGE PRESSURE IS ADEQUATE
		215	; FOR THE SYSTEM. IF NOT WE LIGHT THE RAT LAMP.
		216	
		217	

NADC 81073-60

1515-11 MCS-48/UPI-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 5

LOC	OBJ	SEQ	SOURCE STATEMENT
		218	
		219	
0098	3400	220	RAT: CALL PRSCLC ; SOLVE FOR PSYS
009D	2385	221	MOV A, #85H ; PUT 400 INTO ACCUM
009F	6E	222	ADD A, R6 ; ADD TO GET RANKIN
00A0	E6A4	223	JNC NOCA ; IF NO CARRY NO OVERFLOW
00A2	23FF	224	MOV A, #0FFH ; ELSE PUT FF INTO CARRY
00A4	BAB1	225	NOCA: MOV R2, #0B1H ; PUT 530 R IN R2
00A6	B821	226	MOV R0, #21H ; INITIALIZE TO ADDRESS 33
00A8	5400	227	CALL DIVIDE ; PERFORM 530/(T+460)
		228	; STORE T IN 34 & 35
00AA	2328	229	MOV A, #28H ; GET DISPLACEMENT FROM
00AC	34A9	230	CALL GONOGO ; A/D CONVERTER
00AE	AA	231	MOV R2, A ; AND PUT IN R2
00AF	2378	232	MOV A, #78H ; PUT 3850 INTO ACCUM
00B1	5400	233	CALL DIVIDE ; PERFORM R/3850
		234	; STORE IN 36 & 37
00B3	27	235	CLR A ; WANT 0 IN
00B4	AC	236	MOV R4, A ; R4 AND
00B5	AD	237	MOV R5, A ; R5
00B6	B820	238	MOV R0, #20H ; ADDRESS 32
00B8	F0	239	MOV A, #00
00B9	AE	240	MOV R6, A ; MSBYTE OF PRESSURE
00BA	18	241	INC R0 ; ADDRESS 33
00BB	F0	242	MOV A, #00
00BC	AF	243	MOV R7, A ; MSBYTE OF PRESSURE
00BD	18	244	INC R0 ; ADDRESS 34
00BE	F0	245	MOV A, #00
00BF	C6C5	246	JZ NMULT ; IF 0 NO MULTIPLY
00C1	FE	247	MOV A, R6 ; MSBYTE OF PRESS
00C2	AC	248	MOV R4, A ; TO R4
00C3	FF	249	MOV A, R7 ; MSBYTE OF PRESSURE
00C4	AD	250	MOV R5, A ; TO R5
00C5	18	251	NMULT: INC R0 ; ADDRESS 35
00C6	F0	252	MOV A, #00
00C7	5466	253	CALL QUADM ; MULTIPLY TEMP & PRES
00C9	18	254	INC R0 ; ADDRESS 36
00CA	F0	255	MOV A, #00
00CB	C6D0	256	JZ NMULT1 ; IF 0 CONTINUE
00CD	FE	257	MOV A, R6 ; MSBYTE TO A
00CE	04D4	258	JMP NMULT2 ; NO MULTIPLY
00D0	18	259	NMULT1: INC R0 ; ADDRESS 37
00D1	F0	260	MOV A, #00
00D2	5466	261	CALL QUADM ; MULT PREV RESULT
00D4	53FF	262	NMULT2: ANL A, #0FFH ; WANT TO CHECK Z FLAG
00D6	96E4	263	JNZ END2 ; GREATER THAN 512
00D8	FF	264	MOV A, R7 ; MSBYTE OF PPR
00D9	AA	265	MOV R2, A ; PUT IN R2
00DA	23B6	266	MOV A, #006H ; PUT 400 INTO A
00DC	34B2	267	CALL SBTCT ; REMAINDER - 400
00DE	95	268	CPL F0
00DF	B6E4	269	JF0 END2 ; IF CARRY REM:400
00E1	2304	270	END3: MOV A, #04H ; ADDRESS RAT LAMP
00E3	39	271	OUTL P1, A ; TURN IT ON
00E4	0402	272	END2: JMP START ; REPEAT

NADC 81073-60

ISIS-II MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
MVCOS - A6 REV 18 1/19/80

PAGE 6

LOC	OBJ	SEQ	SOURCE STATEMENT
		273	
0100		274	ORG 0100H
		275	;PRESSURE CALCULATION
		276	;THIS CALCULATION TAKES THE PRESSURE READING IN MV, TAKES
		277	;A TEMPERATURE READING, ADDS OR SUBTRACTS A TEMPERATURE
		278	;CORRECTION TO AN INITIAL SLOPE READING, MULTIPLIES THE NEW
		279	;SLOPE BY THE MV READING AND ADDS AN INITIAL OFFSET, THE MSBYTE
		280	;IS STORED IN R5, AND THE LS BYTE IN R3
		281	;POSITIVE TEMPERATURE
		282	;PRESSURE = (21 + (3T')X0.011) X MV + 23
		283	;NEGATIVE TEMPERATURE
		284	;PRESSURE = (21 - (3T')X0.017) X MV + 23
		285	
0100	2330	286	PRSCLC: MOV A, #30H ;GET PRESSURE DATA FROM
0102	34A9	287	CALL GONOGO ; A/D CONVERTER
0104	A8	288	MOV R0, A ;SAVE VALUE
0105	8A0A	289	MOV R2, #0A0H ;429 PSI
0107	34B3	290	CALL SBTCT ;429 - P
0109	B60D	291	JF0 END4 ;IF CARRY P < 429
010B	04E1	292	JMP END3 ;LIGHT LAMP
010D	F8	293	END4: MOV A, R0 ;GET VALUE BACK
010E	AF	294	MOV R7, A ;STORE
010F	2310	295	MOV A, #10H ;GET TEMPERATURE DATA FROM
0111	34A9	296	CALL GONOGO ; A/D CONVERTER
0113	AE	297	MOV R6, A ;STORE
0114	AA	298	MOV R2, A ; " ALSO IN R2
0115	232B	299	MOV A, #2BH ;GET 70 F IN ACCUM
0117	34B3	300	CALL SBTCT ;T-70 = T'
0119	77	301	RR A ;
011A	77	302	RR A ;
011B	77	303	RR A ;
011C	77	304	RR A ;DIVIDE BY 16
011D	530F	305	ANL A, #0FH ;4 SHIFTS SHOULD BE 0
011F	B629	306	JF0 NTMPTR ;IF NEGATIVE TEMPERATURE
0121	77	307	RR A ;ELSE DIVIDE BY 32
0122	5307	308	ANL A, #07H ;5 SHIFTS SHOULD BE 0
0124	0316	309	ADD A, #16H ;ADD 22 TO DELTA
0126	AD	310	MOV R5, A ;SAVE IN R5
0127	242E	311	JMP MVMPLY ;GO TO MULTIPLY
0129	BA16	312	NTMPTR: MOV R2, #16H ;GET 22
012B	34B3	313	CALL SBTCT ;22 MINUS DELTA
012D	AD	314	MOV R5, A ;SAVE IN R5
012E	FF	315	MVMPLY: MOV A, R7 ;GET MILLI VOLTS
012F	AA	316	MOV R2, A ;AND PUT IN R2
0130	FD	317	MOV A, R5 ;GET DELTA
0131	A9	318	MOV R1, A ;AND PUT IN R1
0132	34B2	319	CALL BMPV ;MULTIPLY
0134	B820	320	MOV R0, #20H ;ADDRESS #32
0136	A0	321	MOV @R0, A ;MSBYTE IN 32
0137	18	322	INC R0 ;ADDRESS #33
0138	F9	323	MOV A, R1 ;GET LS BYTE
0139	A0	324	MOV @R0, A ;STORE IN 33
013A	83	325	RET
		326	
		327	

NADC 81073-60

1515-11 MCS-48/UP1-41 MACRO ASSEMBLER V2.0
HYCOS - A6 REV 18 1/19/88

PAGE 7

LOC	OBJ	SEQ	SOURCE STATEMENT
		328	;10 MILLISECOND SUBROUTINE
		329	;THIS SUBROUTINE USES THE 8748 BUILT IN TIMER THE
		330	;T COUNTER IS LOADED TO 800H
		331	;THIS GIVES A 10 MILLISECOND COUNTDOWN EACH TIME WE
		332	;REACH COUNTDOWN WE DECREMENT A COUNT IN R2 SO THAT
		333	;WE CAN GET MULTIPLES OF 10 MILLISECONDS.
		334	
0138	2380	335 MS10:	MOV A, 800H
013D	62	336	MOV T, A ;LOAD MAX COUNT IN T, ALL 0'S
013E	55	337	STRT T ;START COUNTDOWN
013F	1643	338 CONT:	JTF DECR ;LOOP FOR 10 MILLISECONDS
0141	243F	339	JMP CONT ; " " " "
0143	65	340 DECR:	STOP TCNT ;STOP COUNTER
0144	EA38	341	DJNZ R2, MS10 ;LOOP TILL R2 = 0
0146	83	342	RET
		343	
		344	
		345	
		346	;BYTE STORE SUBROUTINE
		347	;BYTE STORE TRANSFERS THE FIRST 4 BITS INTO THE NEXT RAM
		348	;ADDRESS, THEN THE SECOND 4 BITS INTO THE NEXT RAM ADDRESS.
		349	
0147	A8	350 BYTST:	MOV R0, A ;STORE VALUE IN R0
0148	344F	351	CALL WRITE ;WRITE LSD INTO MEMORY
014A	F8	352	MOV A, R0 ;GET WORD BACK INTO ACCUMULATOR
014B	47	353	SWAP A ;PUT MSD INTO LSD POSITION
014C	344F	354	CALL WRITE ;WRITE MSD INTO MEMORY
014E	83	355	RET
		356	
		357	
		358	;WRITE SUBROUTINE
		359	;WRITE DATA INTO RAM. FIRST PUT DATA ON BUS WITH CE1, 00
		360	;AND RN ALL HIGH. THEN ADDRESS WITH ONLY 00 HIGH. THEN ADDRESS
		361	;WITH ALL HIGH TO TURN OFF MEMORY. P6 HAS 10H STORED AS AN
		362	;INITIAL CONDITION.
014F	B2	363 WRITE	OUTL BUS, A ;OUTPUT DATA ON BUS
0150	FD	364	MOV A, R5 ;PUT INTO ACCUM
0151	4E	365	ORL A, R6 ;PUT A 1 IN FRONT OF ADDRESS
0152	3A	366	OUTL P2, A ;OUTPUT TO MEMORY
0153	4350	367	ORL A, #50H ;TURN ON WRITE
0155	3A	368	OUTL P2, A ;AND OUTPUT TO MEMORY
0156	531F	369	ANL A, #1FH ;PUT 1 IN FRONT OF ADDRESS
0158	3A	370	OUTL P2, A ;OUTPUT TO MEMORY
0159	80	371	MOVX A, @R0 ;PUT BUS IN TRI STATE
015A	1D	372	INC R5 ;GET NEXT ADDRESS
015B	83	373	RET
		374	
		375	;LSD SUBROUTINE
		376	;THIS SUBROUTINE GOES TO MEMORY AND FETCHES A NIBBLE AND
		377	;STORES IT IT THEN GETS THE SECOND NIBBLE COMBINES THEM
		378	;AND WE GET THE WHOLE BYTE
		379	
015C	3464	380 LSD	CALL READ ;GET LSD
015E	47	381	SWAP A ;PUT LSD IN LSD POSITION
015F	A8	382	MOV R0, A ;STORE IN R0

NADC 81073-60

IS15-II MCS-48/UP1-41 MACRO ASSEMBLER. V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 8

LOC	OBJ	SEQ	SOURCE STATEMENT
0160	3464	383	CALL READ ; GET MS0
0162	48	384	ORL A,R0 ; PUT BYTE TOGETHER
0163	83	385	RET
		386	
		387	; READ SUBROUTINE
		388	; READ DATA OUT OF RAM. INITIAL CONDITIONS R5=00 ; R6=30
		389	
0164	00	390	READ: MOVX A,000 ; DISABLE BUS
0165	27	391	CLR A ; ZERO ACCUM
0166	39	392	OUTL P1,A ; CLEAR BUS
0167	FD	393	MOV A,R5 ; PUT INTO ACCUM
0168	4E	394	ORL A,R6 ; PUT A 3 IN FRONT OF ADDRESS
0169	3A	395	OUTL P2,A ; AND OUTPUT TO RAM
016A	532F	396	ANL A,#2FH ; ENABLE READ
016C	4340	397	ORL A,#40H ; 60 IN FRONT OF ADDRESS
016E	3A	398	OUTL P2,A ; " "
016F	00	399	INS A,BUS ; GET WORD FROM RAM
0170	00	400	INS A,BUS ; TWICE
0171	53F0	401	ANL A,#0F0H ; MASK OUT LSD
0173	AF	402	MOV R7,A ; STORE IN R7
0174	FD	403	MOV A,R5 ; GET ADDRESS BACK
0175	4E	404	ORL A,R6 ; PUT 7 IN FRONT OF ADDRESS
0176	533F	405	ANL A,#3FH ; 3 IN FRONT OF ADDRESS
0178	3A	406	OUTL P2,A ; TURN OFF MEMORY
0179	FF	407	MOV A,R7 ; PUT WORD BACK IN ACCUM
017A	1D	408	INC R5 ; GET NEXT ADDRESS
017B	83	409	RET
		410	
		411	; MULTIPLY SUBROUTINE
		412	; MULTIPLY SUBTRACTS T0 IN ACCUM FROM T1 IN R2 TAKES THE
		413	; DIFFERENCE AND MULTIPLIES IT BY CONSTANT (SLOPE) TO GET
		414	; DELTA RESISTANCE. CONSTANT = 3/8
		415	; FIRST DIVIDE BY 8 THEN MULTIPLY BY 2 AND ADD 1
		416	
		417	
017C	34B3	418	MULTPLY: CALL SBTCT ; T1-T0=T'
017E	B903	419	MOV R1,#03H ; NEED 3 SHIFTS
0180	97	420	MULT: CLR C ; SET CARRY = 0
0181	67	421	RRC A ; DIVIDE BY 2
0182	E900	422	DJNZ R1,MULT ; DIVIDE 3 TIMES
0184	A9	423	MOV R1,A ; STORE RESULT IN R1
0185	97	424	CLR C ; SET CARRY = 0
0186	F7	425	RLC A ; MULTIPLY BY 2
0187	69	426	ADD A,R1 ; AND ADD 1
0188	A9	427	MOV R1,A ; STORE IN R1
0189	83	428	RET
		429	
		430	; TMPCK SUBROUTINE
		431	; GETS TEMPERATURE DATA FROM A/D (FOR RESERVOIR AND AIR
		432	; CHECKS) TESTS TO SEE IF IT IS ABOVE 250F (= 121C). IF
		433	; IT IS TOO HIGH WE LIGHT THE TEMP LAMP
		434	
018A	2300	435	TMPCK: MOV A,#00H ; CALL T1 A/D CONVERTER
018C	34A9	436	CALL GONOGO ; GET T1 DATA
018E	AA	437	MOV R2,A ; WANT T1 IN R2

NADC 81073-60

1515-11 MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 9

LOC	OBJ	SEQ	SOURCE STATEMENT
018F	AB	438	MOV R3, A ;SAVE IN R3
0190	2368	439	MOV A, #68H ;68 = 121C = 250F INTO ACCUM
0192	34B3	440	CALL SBTCT ;121-T1
0194	B699	441	JF0 EXCH ;IF CARRY T1<250F
0196	2340	442	MOV A, #40H ;ELSE ENABLE TEMP LAMP
0198	39	443	OUTL P1, A ;LIGHT IT
0199	28	444 EXCH:	XCH R, R3 ;GET T1 FROM R3
019A	2A	445	XCH R, R2 ;PUT IT IN R2
019B	83	446	RET
		447	
		448	
		449	;RESISTOR SUBROUTINE
		450	;FINDS CALCULATED VALUE OF RESISTANCE AND SUBTRACTS IT FROM
		451	;ACTUAL VALUE
		452	
019C	B6A2	453 RSTR:	JF0 SBRTN ;IF F0 IS SET WE HAVE TO SUBTRACT
019E	6A	454	ADD A, R2 ;ELSE WE ADD
019F	AA	455	MOV R2, A ;STORE IN R2
01A0	24A4	456	JMP FINI ;ADDITION COMPLETE
01A2	34B3	457 SBRTN:	CALL SBTCT ;STEP 1 ABOVE
01A4	2320	458 FINI:	MOV A, #20H ;GET ACTUAL R FROM A/D
01A6	34A9	459	CALL GONOGO ;AND PUT IN ACCUM
01A8	83	460	RET
		461	
		462	
		463	
		464	
		465	;GONOGO SUBROUTINE
		466	;THIS SUBROUTINE ENABLES THE SELECTED A/D CONVERTER
		467	;TO PUT DATA ON THE BUS. THE DATA VALID OUTPUT OF THE A/D
		468	;IS CHECKED AND DATA IS ACCEPTED IF TRUE
		469	
01A9	39	470 GONOGO:	OUTL P1, A ;SELECT A/D CONVERTERS
01AA	08	471 NOK:	INS A, BUS ;INPUT DATA FROM BUS
01AB	08	472	INS A, BUS ;TWICE
01AC	F2B0	473	JB7 OK ;CHECK BIT 7 DATA VALID BIT
01AE	24AA	474	JMP NOK ;IF NOT VALID GET NEW DATA
01B0	537F	475 OK:	ANL A, #7FH ;IF OK MASK OUT MSB
01B2	83	476	RET
		477	
		478	;SUBTRACT SUBROUTINE
		479	;SUBTRACTS NUMBER IN ACCUMULATOR FROM NUMBER IN REGISTER R2
		480	;AND STORES THE RESULT IN R2. FLAG F0 IS "0" FOR POSITIVE
		481	;RESULTS AND "1" FOR NEGATIVE
		482	
01B3	85	483 SBTCT:	CLR F0 ;SET FLAG F0 TO 0
01B4	37	484	CPL A ;COMPLEMENT ACCUM
01B5	6A	485	ADD A, R2 ;AND ADD TO R2
01B6	F6B8	486	JC PLUS ;IF A CARRY RESULT IS PLUS
01B8	95	487	CPL F0 ;SET FLAG F0 TO "1"
01B9	37	488	CPL A ;COMPLEMENT ANSWER
01BA	07	489	DEC A ;SUBTRACT 1 AS WE ADD 1 NEXT STEP
01BB	17	490 PLUS:	INC A ;ADD 1 TO GET CORRECT ANSWER
01BC	AA	491	MOV R2, A ;STORE ANSWER IN R2
01BD	83	492	RET ;RETURN

NADC 81073-60

1515-11 MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 10

LOC	OBJ	SEQ	SOURCE STATEMENT
		493	
		494	
		495	; BINARY MULTIPLY SUBROUTINE
		496	; THIS ROUTINE ASSUMES A 1-BYTE MULTIPLIER AND A 1-BYTE
		497	; MULTIPLICAND. THE PRODUCT THEREFORE IS 2 BYTES LONG.
		498	; THE ALGORITHM FOLLOWS THESE STEPS:
		499	; (1) THE REGISTERS ARE ARRANGED AS FOLLOWS:
		500	; ACC = 0
		501	; R1 = MULTIPLIER
		502	; R2 = MULTIPLICAND
		503	; R3 = LOOP COUNTER (=8)
		504	; THE ACCUMULATOR AND REGISTER R1 ARE TREATED AS A REGISTER
		505	; PAIR WHEN THEY ARE SHIFTED RIGHT.
		506	; (2) THE ACCUMULATOR AND R1 ARE SHIFTED RIGHT 1 PLACE. THUS THE
		507	; LSB OF THE MULTIPLIER GOES INTO THE CARRY.
		508	; (3) THE MULTIPLICAND IS ADDED TO THE ACCUMULATOR IF THE CARRY
		509	; BIT IS A '1'. NO ACTION IF CARRY IS A '0'.
		510	; (4) DECREMENT THE LOOP COUNTER AND LOOP (RETURN TO STEP 2) UNTIL
		511	; IT REACHES ZERO.
		512	; (5) SHIFT THE RESULT RIGHT 1 LAST TIME JUST BEFORE EXITING
		513	; THE ROUTINE
		514	
		515	; THE RESULTS WILL BE FOUND: MSBYTE IN THE ACCUMULATOR AND
		516	; LSBYTE IN R1.
01BE	BB08	517 BNPV:	MOV R3, #08H ; SET LOOP COUNTER TO 8
01C0	27	518	CLR A ; CLEAR ACCUMULATOR
01C1	97	519	CLR C ; CLEAR CARRY BIT
01C2	340C	520 BNP1:	CALL DBLRT ; DOUBLE SHIFT RIGHT ACC
		521	; AND R1 INTO CARRY
01C4	E6C7	522	JNC BNP2 ; IF CARRY = 1 ADD ELSE DON'T
01C6	6A	523	ADD A, R2 ; ADD MULTIPLICAND TO ACCUMULATOR
01C7	EBC2	524 BNP2:	DJNZ R3, BNP1 ; DECREMENT LOOP COUNTER AND
		525	; LOOP IF NOT ZERO
01C9	340C	526	CALL DBLRT
01CB	83	527	RET
		528	
		529	
		530	
01CC	67	531 DBLRT:	RRC A ; ROTATE RIGHT THRU CARRY
01CD	29	532	XCH A, R1 ; GET R1 IN ACCUM
01CE	67	533	RRC A
01CF	29	534	XCH A, R1 ; PUT R1 BACK
01D0	83	535	RET
		536	
		537 MRK1:	
01D1	2320	538	MOV A, #20H ; GET R VALUE FROM A/D
01D3	34A9	539	CALL GONOGO ; PUT IN ACCUMULATOR
01D5	BA5C	540	MOV R2, #05CH ; IF R MUST BE LESS THAN
		541	; 11 5K OUT OF 15 7K A/D
		542	; VALUE MUST BE LESS THAN
		543	; 11 5/15 7 X 127 = 92=05CH
01D7	34B3	544	CALL SBTCT ; 05CH - R VALUE
01D9	95	545	CPL F0
01DA	B6DF	546	JF0 MRK2 ; IF A CARRY NO ERROR
01DC	2303	547	MOV A, #03H ; ELSE LIGHT RESEPO1P

NADC 81073-60

IS15-11 MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 11

LOC	OBJ	SEQ	SOURCE STATEMENT
01DE 39		548	OUTL P1,A ; LEVEL LAMP
01DF 049B		549	MRK2: JMP RAT
		550	
		551	
		552	; DIVIDE ROUTINE
		553	; WE DIVIDE A 16 BIT DIVIDEND BY AN 8 BIT DIVISOR
		554	; MSBYTE OF DIVIDEND IS IN R2
		555	; LSBYTE OF DIVIDEND IS IN R3
		556	; DIVISOR IS IN THE ACCUMULATOR
		557	; WE CHECK FOR THE FIRST '1' IN THE DIVISOR WHICH TELLS US HOW
		558	; MANY DIVISIONS. WE ADD THE 2'S COMPLEMENT OF THE DIVISOR TO
		559	; THE DIVIDEND. THE RESULTING CARRY IS SHIFTED INTO THE LSB
		560	; POSITION OF THE LSBYTE THAT RESULTING CARRY IS SHIFTED INTO
		561	; THE LSB POSITION OF THE MSBYTE THE FINAL ANSWER IS STORED
		562	; IN MEMORY
0200		563	ORG 0200H
0200 0000		564	DIVIDE: MOV R3, #0 ; CLEAR R3
0202 8000		565	MOV R5, #0 ; CLEAR R5
0204 05		566	CLR F0 ; CLEAR FLAG F0
0205 97		567	CLR C ; CLEAR CARRY
0206 B908		568	MOV R1, #08H ; INITIAL # OF DIVIDE STEPS
0208 53FF		569	ANL A, #0FFH ; TO SEE IF ACCUM = 0
020A C632		570	JZ X7 ; WANT TO AVOID DIVIDE BY 0
020C F7		571	X1: RLC A ; WANT FIRST '1' SO WE KNOW
020D 19		572	INC R1 ; HOW MANY DIVIDE STEPS
020E 1D		573	INC R5 ; SAME AS ABOVE
020F E60C		574	JNC X1 ; FIRST ONE
0211 67		575	RRC A ; RETURN '1' TO ACCUM
0212 37		576	CPL A ; 1'S COMPLEMENT
0213 17		577	INC A ; 2'S COMPLEMENT
0214 AC		578	MOV R4, A ; SAVE DIVISOR
0215 27		579	CLR A
0216 97		580	X6: CLR C
0217 A7		581	CPL C
0218 F7		582	RLC A
0219 ED16		583	DJNZ R5, X6
021B AE		584	MOV R6, A
021C FC		585	MOV A, R4
021D 6A		586	X2: ADD A, R2 ; SUBTRACT DIVISOR FROM DIVIDEND
021E F622		587	JC X5 ; IF FLAG SET WAS A CARRY
0220 E625		588	JNC X3 ; IF NO CARRY NO CHANGE
0222 97		589	X5: CLR C ; WANT TO SET CARRY TO 1
0223 A7		590	CPL C
0224 AA		591	MOV R2, A ; ELSE PUT NEW RESULT IN R2
0225 FB		592	X3: MOV A, R3 ; LSBYTE IN ACCUM
0226 F7		593	RLC A ; SHIFT CARRY INTO LSB
0227 AB		594	MOV R3, A ; PUT BACK
0228 85		595	CLR F0 ; CLEAR FLAG F0
0229 FA		596	MOV A, R2 ; MSBYTE IN ACCUM
022A F7		597	RLC A ; SHIFT CARRY INTO LSB
022B EE2E		598	JNC X4 ; NO CARRY DON'T SET F0
022D 95		599	CPL F0 ; IF CARRY SET F0
022E AA		600	X4: MOV R2, A ; PUT BACK
022F FC		601	MOV A, R4 ; GET DIVISOR BACK
0230 E91D		602	DJNZ R1, X2 ; CONTINUE DIVISION

NADC 81073-60

ISIS-II MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCOS - A6 REV 18 1/19/88

PAGE 12

LOC	OBJ	SEQ	SOURCE STATEMENT
0232	FE	603	MOV A, R6
0233	5A	604	ANL A, R2
0234	18	605	INC R0 ; GET NEXT MEMORY POSITION
0235	80	606	MOV @R0, A ; STORE IN MEMORY
0236	18	607	INC R0 ; NEXT MEMORY LOCATION
0237	FB	608	MOV A, R3 ; LSBYTE TO ACCUM
0238	80	609	MOV @R0, A ; AND STORE IN MEMORY
0239	83	610	RET
		611	
		612	;LKUP1
		613	;AIR LOOK UP TABLE TO GET (T2 - T1) X 3.78 INTO THE BINARY
		614	;EQUIVALENT OHMS EACH BIT IS 53 OHMS. THIS MAKES EVERY 14 DEGREES
		615	;C EQUAL TO 1 BIT ASSUMING A TEMPERATURE SWING MAX OF FROM -54
		616	;C TO + 135 C OR 189 DEGREES. 189/14 = 13.5 THIS PROGRAM WILL
		617	;LET T' = 13 FOR ZT > 182 AND WILL SUBTRACT 1 FOR EACH 14 DEGREE
		618	;LOWERING. ZT IS STORED IN REG 3. THE ANSWER IS IN REG 4
		619	; (182 - 14 N) WHERE N = NUMBER OF SUBTRACTIONS
		620	
		621	
023A	8B	622	LKUP1: MOV R3, A ; STORE ZT IN R3
023B	BC0E	623	MOV R4, #0EH ; START WITH 14 IN R4
023D	B086	624	MOV R5, #086H ; START WITH 182 IN R5
023F	FB	625	REPT1: MOV A, R3 ; ZT IN ACCUM
0240	AA	626	MOV R2, A ; AND PUT IN R2
0241	FD	627	MOV A, R5 ; 182 - 14N
0242	3483	628	CALL SBTCT ; ZT - (182 - 14N)
0244	FD	629	MOV A, R5 ; GET 182 - 14N
0245	03F2	630	ADD A, #0F2H ; SUBTRACT ANOTHER 14
0247	AD	631	MOV R5, A ; NEW VALUE BACK IN R5
0248	FC	632	MOV A, R4 ; PUT R4 INTO ACCUM
0249	07	633	DEC A ; A CONTAINS ANSWER
024A	C64F	634	JZ NONR1 ; IF R4 = 0 END ROUTINE
024C	AC	635	MOV R4, A ; ELSE PUT RESULT BACK IN R4
024D	B63F	636	JF0 REPT1 ; IF F0 ZT < (182 - 14N)
024F	83	637	NONR1: RET
		638	
		639	
		640	
		641	;LKUP2
		642	;NORMAL DISPLACEMENT LOOKUP TABLE. THIS ROUTINE WILL TAKE
		643	;ZT X 3.33 DIVIDE BY 53 AND GIVE THE BINARY EQUIVALENT OF THE
		644	;ANSWER JUST AS FOR LKUP1 ABOVE EACH TEMPERATURE DELTA IS 16
		645	;DEGREES AS ABOVE ZT MAX = 189. 189/16 = 11.8 WE LET THE
		646	;MAX BINARY # = 11 FOR ZT > 176 AND WE SUBTRACT 1 FOR EVERY
		647	;16 DEGREE LOWERING.
		648	;ZT IS STORED IN R3.
		649	;FINAL ANSWER STORED IN R4
		650	
		651	
		652	
0250	8B	653	LKUP2: MOV R3, A ; STORE ZT IN REG 3
0251	BC0C	654	MOV R4, #0CH ; START WITH 12 IN R4
0253	B080	655	MOV R5, #080H ; START WITH 176 IN R5
0255	FB	656	REPT2: MOV A, R3 ; ZT IN ACCUM
0256	AA	657	MOV R2, A ; AND INTO R2

NADC 81073-60

ISIS-II MCS-48/UPI-41 MACRO ASSEMBLER V2.0
HYCOS - A6 REV 18 1/19/80

PAGE 13

LOC	OBJ	SEQ	SOURCE STATEMENT
0257	FD	658	MOV R, R5 ;176 - 16N INTO ACCUM
0258	34B3	659	CALL SBTCT ;ZT - (176 - 16N)
025A	FD	660	MOV R, R5 ;GET 176 -16N
025B	03F0	661	ADD R, #0F0H ;SUBTRACT ANOTHER 16
025D	AD	662	MOV R5, A ;AND STORE RESULT IN R5
025E	FC	663	MOV R, R4 ;R4 INTO ACCUM
025F	07	664	DEC A ;A HAS ANSWER
0260	C665	665	JZ NOMR2 ;IF R4 IS 0 END ROUTINE
0262	AC	666	MOV R4, A ;ELSE PUT RESULT BACK IN R4
0263	B655	667	JF0 REPT2 ;IF F0 ZT < (176 - 16N)
0265	83	668	NOMR2: RET
		669	
		670	
		671	
		672	
		673	
		674	;QUAD MULTIPLY
		675	;FIRST MULTIPLY 0 AND R7 (LSBYTE) DROP LSBYTE OF RESULT
		676	;AND ADD MSBYTE OF RESULT TO R5.
		677	;THEN MULTIPLY 0 AND R6 (MSBYTE). ADD LSBYTE OF RESULT
		678	;TO R5 AND MSBYTE OF RESULT TO R4.
		679	
		680	
0266	AA	681	QUADM: MOV R2, A ;GET MULTIPLIER IN R2
0267	FF	682	MOV R, R7 ;LSBYTE
0268	AA	683	MOV R1, A ;TO R1
0269	34BE	684	CALL BMPY ;MULTIPLY
026B	6D	685	ADD R, R5 ;ADD MSBY OF CALC TO R5
026C	AD	686	MOV R5, A ;STORE IN R5
026D	E670	687	JNC Y1 ;IF CARRY
026F	1C	688	INC R4 ;ADD 1 TO R4
0270	FE	689	Y1: MOV R, R6 ;MSBYTE
0271	AA	690	MOV R1, A ;TO R1
0272	34BE	691	CALL BMPY ;MULTIPLY
0274	29	692	XCH R, R1 ;MSBY TO R1 LSBY TO A
0275	6D	693	ADD R, R5 ;ADD LSBYTES
0276	BD00	694	MOV R5, #0H ;CLEAR R5
0278	AF	695	MOV R7, A ;RESULT TO R7
0279	E67C	696	JNC Y2 ;IF CARRY
027B	1C	697	INC R4 ;ADD 1 TO MSBY
027C	F9	698	Y2: MOV R, R1 ;MSBYTE TO A
027D	6C	699	ADD R, R4 ;ADD MSBYTES
027E	BD00	700	MOV R4, #0H ;CLEAR R4
0280	AE	701	MOV R6, A ;RESULT TO R7
0281	83	702	RET
		703	
		704	
		705	
		706	
		707	
		708	END

USER SYMBOLS

BMP1	01C2	BMP2	01C7	BMPY	01BE	BYTST	0147	CONT	013F	DBLRT	01CC	DECR	0143	DIVIDE	0200
END2	00E4	END3	00E1	END4	0100	EXCH	0199	FINI	01A4	GONOGO	01A9	LKUP1	023A	LKUP2	0250

NADC 81073-60

1515-11 MCS-48/UP1-41 MACRO ASSEMBLER, V2.0
HYCDS - A6 REV 18 1/19/80

PAGE 14

LSD	015C	MULTPLY	017C	MRK1	01D1	MRK2	01DF	MS10	013B	MULT	0180	MMPLY	012E	NEG1	0038
NMLT1	00D0	NMLT2	00D4	NOCR	00A4	NOK	01AA	NOMLT	00C5	NOMR1	024F	NOMR2	0265	NTHPTR	0129
OK	01B0	PLUS	01BB	POS1	004C	PRCLC	0100	QUADM	0266	RAT	0098	READ	0164	REPT1	023F
REPT2	0255	RMLD	0025	RSRVR	0070	RSTR	019C	RUDDER	005D	SBRTN	01A2	SBTCT	01B3	SQNC	0016
START	0002	SUM1	004E	THPCX	010A	TSTUT	001B	WRITE	014F	X1	020C	X2	021D	X3	0225
X4	022E	X5	0222	X6	0216	X7	0232	Y1	0270	Y2	027C				

ASSEMBLY COMPLETE, NO ERRORS

**DAT
FILM**